

# **ASHRAE Standard 140-2020**

## **Test Results Comparison for**

### **Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF**

Results for TRNSYS 18.05.0001  
(TRNSYS18)

vs.

Example Results

Prepared By  
Thermal Energy System Specialists, LLC  
(TESS)

Results Developed  
22-Mar-2023

## ASHRAE Standard 140-2020

### Computer Programs, Program Authors, and Producers of Example Results for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF

The programs used to generate the example results for Sections 5.2.1, 5.2.2, and 5.2.3 are described in Table B11-1. Under the "Computer Program" column, the first entry in each cell is the proper program name and version number. The entries in parentheses are the abbreviations for the programs used in the tables and charts of this workbook.

The second column ("Authoring Organization") indicates the national research facility, university, or industry organization with expertise in building science that wrote the simulation software.

The third column ("Example Results Produced By") indicates the national research facility, university, or industry organization with expertise in building science that performed the simulations. Most of the organizations that performed simulations are members of the development team for the simulation model that they ran.

See Standard 140, Annex B11 for further details.

**TABLE B11-1**

#### Computer Programs, Program Authors, and Producers of Example Results

| Computer Program (Abbrev.)                                | Authoring Organization  | Example Results Produced by                               |
|---|---|---|
| BSIMAC 9, Version 9.0.74<br>(BSIMAC)                      | Alec Johannsen Consulting Engineers,<br>South Africa  | Alec Johannsen Consulting Engineers,<br>South Africa      |
| California Simulation Engine,<br>Version 0.861.1<br>(CSE) | J.R. Barnaby/C.S. Barnaby/Big Ladder<br>Software LLC/Wrightsoft Corp., United<br>States         | Big Ladder Software LLC, United States                    |
| DeST 2.0, Version 20190401<br>(DeST)                      | Tsinghua University, China  | Southeast University, China<br>Tsinghua University, China |
| EnergyPlus, Version 9.0.1<br>(EnergyPlus)                 | U.S. Department of Energy, Building<br>Technologies Office, United States                       | GARD Analytics, Inc., United States                       |
| ESP-r, Version 13.3<br>(ESP-r)                            | University of Strathclyde, United<br>Kingdom  | University of Strathclyde, United<br>Kingdom              |
| TRNSYS, Version 18.01.0001<br>(TRNSYS)                    | Transsolar Energietechnik GmbH,<br>Germany; Thermal Energy System<br>Specialists, United States | Transsolar Energietechnik GmbH,<br>Germany                |
| TRNSYS, Versions 17.02.0005 and<br>18.00.0017<br>(N/A)    | Transsolar Energietechnik GmbH,<br>Germany; Thermal Energy System<br>Specialists, United States | Ecole Polytechnique Montréal, Canada <sup>a,b</sup>       |

<sup>a</sup> Ecole Polytechnique and GARD also worked on simulations for developing alternative constant interior and exterior surface coefficients, applying TRNSYS and EnergyPlus, respectively.

<sup>b</sup> Also checking input files versus the Transsolar participant's files and vice versa.

Note: Results for "TestSpec-Alt" are shown in Table B8-16 and in Figures B8-6, B8-H10, and B8-H11; contents of tables and figures are further described in sheet tabs labeled "Table List" and "Figure List". "TestSpec-Alt" results are alternative values resulting from optional alternative inputs for sky temperature provided in the test specification (see Section 5.2.1.1.1.2 and Annex A1, Section A1.1.1.2).

**ASHRAE Standard 140-2010 Section 5.2 - Building Thermal Envelope and Fabric Load Tests  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

**List of Tables**

| <i>Table</i> | <i>Description</i>   | <i>Sheet Tab</i> | <i>Cell Range</i> |
|--------------|--|------------------|-------------------|
| B8-1         | Annual Heating Loads   | Tables 1         | B7 - N57          |
| B8-2         | Annual Sensible Cooling Loads  |                  | B59 - N109        |
| B8-3         | Annual Hourly Integrated Peak Heating Loads                                  | Tables 2         | B7 - A157         |
| B8-4         | Annual Hourly Integrated Peak Sensible Cooling Loads                         |                  | B59 - A1109       |
| B8-5         | Free-Float Temperature Output  |                  | B111 - A1145      |
| B8-6         | Low Mass Basic Sensitivity Tests   | Tables 3         | B7 - N58          |
| B8-7         | High Mass Basic Sensitivity Tests  |                  | B61 - N112        |
| B8-8         | Low Mass In-Depth (Cases 195 thru 320) Sensitivity Tests                     | Tables 4         | B7 - N76          |
| B8-9         | Low Mass In-Depth (Cases 395 thru 470) Sensitivity Tests                     | Tables 5         | B7 - N64          |
| B8-10        | High Mass Basic and In-Depth Sensitivity Tests                               |                  | B67 - N122        |
| B8-11        | Annual Transmissivity Coefficient of Windows                                 | Tables 6         | B7 - N16          |
| B8-12        | Annual Shading Coefficient of Window Shading Devices: Overhangs & Fins       |                  | B18 - N25         |
| B8-13        | Case 600 Annual Incident Solar Radiation (kWh/m <sup>2</sup> )               |                  | B27 - N36         |
| B8-14        | Case 600 Annual Transmitted Solar Radiation – Unshaded (kWh/m <sup>2</sup> ) |                  | B38 - N46         |
| B8-15        | Case 600 Annual Transmitted Solar Radiation –Shaded (kWh/m <sup>2</sup> )    |                  | B48 - N54         |
| B8-16        | Sky Temperature Output, Case 600   | Tables 7         | B7 - AM15         |
| B8-M1        | Monthly Heating Loads  | Tables M1        | B7 - N36          |
| B8-M2        | Monthly Sensible Cooling Loads   |                  | B38 - N67         |
| B8-M3        | Monthly Hourly Integrated Peak Heating Loads                                 | Tables M2        | B7 - AB36         |
| B8-M4        | Monthly Hourly Integrated Peak Sensible Cooling Loads                        |                  | B38 - AB67        |
| B8-M5        | Monthly Load 600-900 Sensitivity Tests                                       | Tables M3        | B7 - N68          |

**ASHRAE Standard 140-2010 Section 5.2 - Building Thermal Envelope and Fabric Load Tests  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

**List of Figures**

| <b>Figure</b> | <b>Title</b>  | <b>Sheet Tab</b>                 |
|---------------|---|----------------------------------|
| B8-1          | Annual Incident Solar Radiation   | Fig B8-1 Ann Incident Solar      |
| B8-2          | Annual Transmitted Solar Radiation Unshaded   | Fig B8-2 Ann SolRad Unshaded     |
| B8-3          | Annual Transmitted Solar Radiation Shaded   | Fig B8-3 Ann SolRad Shaded       |
| B8-4          | Annual Transmissivity Coefficient of Windows<br>(Unshaded Transmitted)/(Incident Solar Radiation)     | Fig B8-4 Trans Coeff             |
| B8-5          | Annual Overhang and Fin Shading Coefficients<br>(1-(Shaded)/(Unshaded)) Transmitted Solar Radiation   | Fig B8-5 OH&Fin Shade Coeff      |
| B8-6          | Average, Minimum and Maximum Sky Temperature, Case 600  | Fig B8-6 Sky Temp                |
| B8-7          | Basic: Low Mass Annual Heating  | Fig B8-7 Lomass Ann Heat         |
| B8-8          | Basic: Low Mass Annual Sensible Cooling   | Fig B8-8 Lomass Ann Cool         |
| B8-9          | Basic: Low Mass Peak Heating  | Fig B8-9 Lomass Peak Heat        |
| B8-10         | Basic: Low Mass Peak Sensible Cooling   | Fig B8-10 Lomass Peak Cool       |
| B8-11         | Basic: High Mass Annual Heating   | Fig B8-11 Himass Ann Heat        |
| B8-12         | Basic: High Mass Annual Sensible Cooling  | Fig B8-12 Himass Ann Cool        |
| B8-13         | Basic: High Mass Peak Heating   | Fig B8-13 Himass Peak Heat       |
| B8-14         | Basic: High Mass Peak Sensible Cooling  | Fig B8-14 Himass Peak Cool       |
| B8-15         | Basic and In-Depth: South Window (Delta),<br>Annual Heating and Sensible Cooling                      | Fig B8-15 Delta-S Win-Ann        |
| B8-16         | Basic and In-Depth: South Window (Delta),<br>Peak Heating and Sensible Cooling                        | Fig B8-16 Delta-S Win-Peak       |
| B8-17         | Basic: Window Shading and Orientation (Delta),<br>Annual Heating and Sensible Cooling                 | Fig B8-17 Delta-ShadeOrient-Load |
| B8-18         | Basic: Window Shading and Orientation (Delta),<br>Peak Heating and Sensible Cooling                   | Fig B8-18 Delta-ShadeOrient-Peak |
| B8-19         | Basic: Thermostat Setback, Vent Cooling, and Sunspace (Delta),<br>Annual Heating and Sensible Cooling | Fig B8-19 Delta-640650960-Load   |
| B8-20         | Basic: Thermostat Setback, Vent Cooling, and Sunspace (Delta),<br>Peak Heating and Sensible Cooling   | Fig B8-20 Delta-640650960-Peak   |
| B8-21         | Basic and In-Depth: Mass Effect (Delta),<br>Annual Heating and Sensible Cooling                       | Fig B8-21 Delta-Mass Effect-Ann  |
| B8-22         | Basic and In-Depth: Mass Effect (Delta),<br>Peak Heating and Sensible Cooling                         | Fig B8-22 Delta-Mass Effect-Pk   |
| B8-23         | Basic: Cases 660 to 695 and 980 to 995 Annual Heating   | Fig B8-23 660+ Ann Heat          |
| B8-24         | Basic: Cases 660 to 695 and 980 to 995 Annual Cooling   | Fig B8-24 660+ Ann Cool          |
| B8-25         | Basic: Cases 660 to 695 and 980 to 995 Peak Heating   | Fig B8-25 660+ Peak Heat         |
| B8-26         | Basic: Cases 660 to 695 and 980 to 995 Peak Cooling   | Fig B8-26 660+ Peak Cool         |
| B8-27         | Basic: Window Types (Delta), Annual Heating and Sensible Cooling                                      | Fig B8-27 Delta-Windows-Load     |
| B8-28         | Basic: Window Types (Delta), Peak Heating and Sensible Cooling  | Fig B8-28 Delta-Windows-Peak     |
| B8-29         | Basic: Insulation (Delta), Annual Heating and Sensible Cooling  | Fig B8-29 Delta-Insul-Load       |
| B8-30         | Basic: Insulation (Delta), Peak Heating and Sensible Cooling  | Fig B8-30 Delta-Insul-Peak       |
| B8-31         | Basic: Insulation, Mass Effect (Delta),<br>Annual Heating and Sensible Cooling                        | Fig B8-31 Del-Mass-Ins-Load      |
| B8-32         | Basic: Insulation, Mass Effect (Delta),<br>Peak Heating and Sensible Cooling                          | Fig B8-32 Del-Mass-Ins-Peak      |
| B8-33         | Basic: Average Hourly Annual Temperature Free-Float Cases   | Fig B8-33 FF Average Temp        |
| B8-34         | Basic: Maximum Hourly Annual Temperature Free-Float Cases   | Fig B8-34 FF Maximum Temp        |
| B8-35         | Basic: Minimum Hourly Annual Temperature Free-Float Cases   | Fig B8-35 FF Minimum Temp        |

**ASHRAE Standard 140-2010 Section 5.2 - Building Thermal Envelope and Fabric Load Tests  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

**List of Figures**

| <b>Figure</b> | <b>Title</b>  | <b>Sheet Tab</b>                 |
|---------------|---|----------------------------------|
| B8-36         | In-Depth: Low Mass Cases 195 to 250 Annual Heating  | Fig B8-36 195to250 Ann Heat      |
| B8-37         | In-Depth: Low Mass Cases 195 to 250 Annual Sensible Cooling                                     | Fig B8-37 195to250 Ann Cool      |
| B8-38         | In-Depth: Low Mass Cases 195 to 250 Peak Heating  | Fig B8-38 195to250 Peak Heat     |
| B8-39         | In-Depth: Low Mass Cases 195 to 250 Peak Sensible Cooling                                       | Fig B8-39 195to250 Peak Cool     |
| B8-40         | In-Depth: Low Mass Cases 270 to 320 Annual Heating  | Fig B8-40 270to320 Ann Heat      |
| B8-41         | In-Depth: Low Mass Cases 270 to 320 Annual Sensible Cooling                                     | Fig B8-41 270to320 Ann Cool      |
| B8-42         | In-Depth: Low Mass Cases 270 to 320 Peak Heating  | Fig B8-42 270to320 Peak Heat     |
| B8-43         | In-Depth: Low Mass Cases 270 to 320 Peak Sensible Cooling                                       | Fig B8-43 270to320 Peak Cool     |
| B8-44         | In-Depth: Cases 195 to 220 (Delta)<br>Annual Heating and Sensible Cooling                       | Fig B8-44 Delta 195to220 Load    |
| B8-45         | In-Depth: Cases 195 to 220 (Delta)<br>Peak Heating and Sensible Cooling                         | Fig B8-45 Delta 195to220 Peak    |
| B8-46         | In-Depth: Cases 220 to 270 (Delta)<br>Annual Heating and Sensible Cooling                       | Fig B8-46 Delta 220to270 Load    |
| B8-47         | In-Depth: Cases 220 to 270 (Delta)<br>Peak Heating and Sensible Cooling                         | Fig B8-47 Delta 220to270 Peak    |
| B8-48         | In-Depth: Cases 270 to 320 (Delta)<br>Annual Heating and Sensible Cooling                       | Fig B8-48 Delta 270to320 Load    |
| B8-49         | In-Depth: Cases 270 to 320 (Delta)<br>Peak Sensible Cooling                                     | Fig B8-49 Delta 270to320 Peak    |
| B8-50         | In-Depth: Cases 395 to 440, 800, 810 Annual Heating   | Fig B8-50 395to440,8n0 Ann Heat  |
| B8-51         | In-Depth: Cases 395 to 440, 800, 810 Annual Sensible Cooling                                    | Fig B8-51 395to440,8n0 Ann Cool  |
| B8-52         | In-Depth: Cases 395 to 440, 800, 810 Peak Heating   | Fig B8-52 395to440,8n0 Pk Heat   |
| B8-53         | In-Depth: Cases 395 to 440, 800, 810 Peak Sensible Cooling                                      | Fig B8-53 395to440,8n0 Pk Cool   |
| B8-54         | In-Depth: Cases 395 to 600, 810 to 900 (Delta)<br>Annual Heating and Sensible Cooling           | Fig B8-54 Del 395-600,810,900 Ld |
| B8-55         | In-Depth: Cases 395 to 600, 810 to 900 (Delta)<br>Peak Heating and Sensible Cooling             | Fig B8-55 Del 395-600,810,900 Pk |
| B8-56         | In-Depth: Surface Heat Transfer Cases 600, 450, 460, 470<br>Annual Heating and Sensible Cooling | Fig B8-56 SurfCoefs-Load         |
| B8-57         | In-Depth: Surface Heat Transfer Cases 600, 450, 460, 470<br>Peak Heating and Sensible Cooling   | Fig B8-57 SurfCoefs-Peak         |
| B8-58         | In-Depth: Surface Heat Transfer Cases 450 to 600 (Delta)<br>Annual Heating and Sensible Cooling | Fig B8-58 SurfHT Delta-Load      |
| B8-59         | In-Depth: Surface Heat Transfer Cases 450 to 600 (Delta)<br>Peak Heating and Sensible Cooling   | Fig B8-59 SurfHT Delta-Peak      |

**ASHRAE Standard 140-2010 Section 5.2 - Building Thermal Envelope and Fabric Load Tests  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

**List of Figures**

| <b>Figure</b> | <b>Title</b>   | <b>Sheet Tab</b>                |
|---------------|--|---------------------------------|
| B8-M1         | Monthly Heating, Case 600  | Fig B8-M1 MthlyHtg-600          |
| B8-M2         | Monthly Sensible Cooling, Case 600   | Fig B8-M2 MthlyCtg-600          |
| B8-M3         | Monthly Peak Heating, Case 600   | Fig B8-M3 MthlyPkHtg-600        |
| B8-M4         | Monthly Peak Sensible Cooling, Case 600  | Fig B8-M4 MthlyPkClg-600        |
| B8-M5         | Monthly Heating, Case 900  | Fig B8-M5 MthlyHtg-900          |
| B8-M6         | Monthly Sensible Cooling, Case 900   | Fig B8-M6 MthlyCtg-900          |
| B8-M7         | Monthly Peak Heating, Case 900   | Fig B8-M7 MthlyPkHtg-900        |
| B8-M8         | Monthly Peak Sensible Cooling, Case 900  | Fig B8-M8 MthlyPkClg-900        |
| B8-M9         | Monthly Heating Sensitivity (Delta), Case 600-900  | Fig B8-M9 Del-MthlyHtg 600-900  |
| B8-M10        | Monthly Cooling Sensitivity (Delta), Case 600-900  | Fig B8-M10 Del-MthlyCtg 600-900 |
| B8-M11        | Monthly Peak Heating Sensitivity (Delta), Case 600-900   | Fig B8-M11 Del-MthlyPkH 600-900 |
| B8-M12        | Monthly Peak Cooling Sensitivity (Delta), Case 600-900   | Fig B8-M12 Del-MthlyPkC 600-900 |
| B8-H1         | Case 900FF Annual Hourly Temperature Frequency   | Fig B8-H1 Hrly-Temp Freq        |
| B8-H2         | Case 600 Cloudy & Clear Day Hourly Incident Solar Horizontal (Upward) Facing Surface                         | Fig B8-H2 Hrly-IncSol-Horz      |
| B8-H3         | Case 600 Cloudy & Clear Day Hourly Incident Solar South Facing Surface                                       | Fig B8-H3 Hrly-IncidentSol-S    |
| B8-H4         | Case 600 Cloudy & Clear Day Hourly Incident Solar West Facing Surface  | Fig B8-H4 Hrly-IncidentSol-W    |
| B8-H5         | Cases 600, 660, 670 Hourly Transmitted Solar, Clear/Cold Day (Feb 1) Double-Pane, Low-E, Single-Pane Windows | Fig B8-H5 Hrly-TransSol-Feb1    |
| B8-H6         | Case 600 Hourly Transmitted Solar, Cloudy Day (May 4) Double-Pane Windows                                    | Fig B8-H6 Hrly-Trans-May4-600   |
| B8-H7         | Cases 660,670 Hourly Transmitted Solar, Cloudy Day (May 4) Low-E and Single-Pane Windows                     | Fig B8-H7 Hrly-Trans-May4-6670  |
| B8-H8         | Case 600 Hourly Transmitted Solar, Clear/Hot Day (Jul 14) Double-Pane Windows                                | Fig B8-H8 Hrly-Trans-Jul14-600  |
| B8-H9         | Cases 660, 670 Hourly Transmitted Solar, Clear/Hot Day (Jul 14) Low-E and Single-Pane Windows                | Fig B8-H9 Hrl-Trans-Jul14-6670  |
| B8-H10        | Hourly Sky Temperatures, Case 600: Clear/Cold, Cloudy Days   | Fig B8-H10 Hrly-Tsky-ClearCloud |
| B8-H11        | Hourly Sky Temperatures, Case 600: Clear/Cold, Clear/Hot Days  | Fig B8-H11 Hrly-Tsky-ColdHot    |
| B8-H12        | Hourly Free-Float Temperatures, Clear Cold Day (Feb 1), Cases 600FF and 900FF                                | Fig B8-H12 Hrly-FF Temp-ColdDay |
| B8-H13        | Hourly Free-Float Temperatures, Clear Hot Day (Jul 14), Cases 650FF and 950FF                                | Fig B8-H13 Hrly-FF Temp-HotDay  |
| B8-H14        | Hourly Free-Float Temperatures, Clear Cold Day (Feb 1), Cases 680FF and 980FF                                | Fig B8-H14 Hr-6980FF T-ColdDay  |

**ASHRAE Standard 140-2010 Section 5.2 - Building Thermal Envelope and Fabric Load Tests  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

**List of Figures**

| <b>Figure</b> | <b>Title</b>  | <b>Sheet Tab</b>              |
|---------------|---|-------------------------------|
| B8-H15        | Hourly Loads: Clear Cold Day, Case 600 (Low Mass, Double-Clear Window)<br>Heating (+), Sensible Cooling (-) | Fig B8-H15 Hrly-600Loads-Cold |
| B8-H16        | Hourly Loads: Clear Hot Day, Case 600 (Low Mass, Double-Clear Window)<br>Heating (+), Sensible Cooling (-)  | Fig B8-H16 Hrly-600Loads-Hot  |
| B8-H17        | Hourly Loads: Clear Cold Day, Case 640 (Low Mass, Night Setback)<br>Heating (+), Sensible Cooling (-)       | Fig B8-H17 Hrly-640Loads-Cold |
| B8-H18        | Hourly Conditioned Zone Temperatures, Clear Cold Day, Case 640<br>Heating (+), Sensible Cooling (-)         | Fig B8-H18 Hrly-640Tzone-Cold |
| B8-H19        | Hourly Loads: Clear Cold Day, Case 940 (High Mass, Night Setback)<br>Heating (+), Sensible Cooling (-)      | Fig B8-H19 Hrly-940Loads-Cold |
| B8-H20        | Hourly Conditioned Zone Temperatures, Clear Cold Day, Case 940<br>Heating (+), Sensible Cooling (-)         | Fig B8-H20 Hrly-940Tzone-Cold |
| B8-H21        | Hourly Loads: Clear Cold Day, Case 660 (Low-E Window)<br>Heating (+), Sensible Cooling (-)                  | Fig B8-H21 Hrly-660Loads-Cold |
| B8-H22        | Hourly Loads: Clear Hot Day, Case 660 (Low-E Window)<br>Heating (+), Sensible Cooling (-)                   | Fig B8-H22 Hrly-660Loads-Hot  |
| B8-H23        | Hourly Loads: Clear Cold Day, Case 670 (Single-Pane Window)<br>Heating (+), Sensible Cooling (-)            | Fig B8-H23 Hrly-670Loads-Cold |
| B8-H24        | Hourly Loads: Clear Hot Day, Case 670 (Single-Pane Window)<br>Heating (+), Sensible Cooling (-)             | Fig B8-H24 Hrly-670Loads-Hot  |
| B8-H25        | Hourly Loads: Clear Cold Day, Case 680 (Insulation)<br>Heating (+), Sensible Cooling (-)                    | Fig B8-H25 Hrly-680Loads-Cold |
| B8-H26        | Hourly Loads: Clear Hot Day, Case 680 (Insulation)<br>Heating (+), Sensible Cooling (-)                     | Fig B8-H26 Hrly-680Loads-Hot  |
| B8-H27        | Hourly Loads: Clear Cold Day, Case 685 (20/20 Tstat)<br>Heating (+), Sensible Cooling (-)                   | Fig B8-H27 Hrly-685Loads-Cold |
| B8-H28        | Hourly Loads: Clear Hot Day, Case 685 (20/20 Tstat)<br>Heating (+), Sensible Cooling (-)                    | Fig B8-H28 Hrly-685Loads-Hot  |
| B8-H29        | Hourly Loads: Clear Cold Day, Case 695 (20/20, Insulation)<br>Heating (+), Sensible Cooling (-)             | Fig B8-H29 Hrly-695Loads-Cold |
| B8-H30        | Hourly Loads: Clear Hot Day, Case 695 (20/20, Insulation)<br>Heating (+), Sensible Cooling (-)              | Fig B8-H30 Hrly-695Loads-Hot  |
| B8-H31        | Hourly Loads: Clear Cold Day, Case 900 (High Mass)<br>Heating (+), Sensible Cooling (-)                     | Fig B8-H31 Hrly-900Loads-Cold |
| B8-H32        | Hourly Loads: Clear Hot Day, Case 900 (High Mass)<br>Heating (+), Sensible Cooling (-)                      | Fig B8-H32 Hrly-900Loads-Hot  |
| B8-H33        | Hourly Loads: Clear Cold Day, Case 980 (High Mass, Insulation)<br>Heating (+), Sensible Cooling (-)         | Fig B8-H33 Hrly-980Loads-Cold |
| B8-H34        | Hourly Loads: Clear Hot Day, Case 900 (High Mass, Insulation)<br>Heating (+), Sensible Cooling (-)          | Fig B8-H34 Hrly-980Loads-Hot  |
| B8-H35        | Hourly Loads: Clear Cold Day, Case 985 (High Mass, 20/20 Tstat)<br>Heating (+), Sensible Cooling (-)        | Fig B8-H35 Hrly-985Loads-Cold |
| B8-H36        | Hourly Loads: Clear Hot Day, Case 985 (High Mass, 20/20 Tstat)<br>Heating (+), Sensible Cooling (-)         | Fig B8-H36 Hrly-985Loads-Hot  |
| B8-H37        | Hourly Loads: Clear Cold Day, Case 995 (High Mass, 20/20, Insulation)<br>Heating (+), Sensible Cooling (-)  | Fig B8-H37 Hrly-995Loads-Cold |
| B8-H38        | Hourly Loads: Clear Hot Day, Case 995 (High Mass, 20/20, Insulation)<br>Heating (+), Sensible Cooling (-)   | Fig B8-H38 Hrly-995Loads-Hot  |

**ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results**

**By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-1. Annual Heating Loads (MWh)**

| Simulation Model:<br>Case                          | BSIMAC | CSE   | DeST   | EnergyPlus | ESP-r | TRNSYS | Statistics for Example Results |        |        |                          | TRNSYS18 |
|--|--------|-------|--------|------------|-------|--------|--------------------------------|--------|--------|--------------------------|----------|
|  |        |       |        |            |       |        | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 600 Base Case, South Windows                       | 4.050  | 3.993 | 4.047  | 4.324      | 4.362 | 4.504  | 3.993                          | 4.504  | 4.213  | 12.1%                    | 4.500    |
| 610 S. Windows + Overhang                          | 4.163  | 4.066 | 4.144  | 4.375      | 4.527 | 4.592  | 4.066                          | 4.592  | 4.311  | 12.2%                    | 4.589    |
| 620 East & West Windows                            | 4.370  | 4.094 | 4.297  | 4.485      | 4.514 | 4.719  | 4.094                          | 4.719  | 4.413  | 14.2%                    | 4.715    |
| 630 E&W Windows + Overhang & Fins                  | 4.923  | 4.356 | 4.677  | 4.784      | 5.051 | 5.139  | 4.356                          | 5.139  | 4.821  | 16.2%                    | 5.137    |
| 640 Case 600 with Htg Temp. Setback                | 2.682  | 2.403 | 2.619  | 2.662      | 2.654 | 2.653  | 2.403                          | 2.682  | 2.612  | 10.7%                    | 2.648    |
| 650 Case 600 with Night Ventilation                | 0.000  | 0.000 | 0.000  | 0.000      | 0.000 | 0.000  | 0.000                          | 0.000  | 0.000  | ---                      | 0.000    |
| 660 Low-E Windows                                  | 3.574  | 3.602 | 3.821  | 3.707      | 3.787 | 3.790  | 3.574                          | 3.821  | 3.713  | 6.7%                     | 3.786    |
| 670 Single-Pane Windows                            | 5.484  | 5.300 | 5.573  | 5.616      | 5.975 | 6.140  | 5.300                          | 6.140  | 5.681  | 14.8%                    | 6.136    |
| 680 Case 600 with Increased Insulation             | 2.219  | 1.786 | 1.732  | 2.180      | 2.132 | 2.286  | 1.732                          | 2.286  | 2.056  | 27.0%                    | 2.284    |
| 685 Case 600 with "20/20" Thermostat               | 4.532  | 4.574 | 4.646  | 4.877      | 4.904 | 5.042  | 4.532                          | 5.042  | 4.763  | 10.7%                    | 5.038    |
| 695 Case 685 with Increased Insulation             | 2.709  | 2.415 | 2.385  | 2.802      | 2.732 | 2.892  | 2.385                          | 2.892  | 2.656  | 19.1%                    | 2.889    |
| 900 South Windows                                  | 1.726  | 1.379 | 1.591  | 1.664      | 1.585 | 1.814  | 1.379                          | 1.814  | 1.626  | 26.8%                    | 1.803    |
| 910 S. Windows + Overhang                          | 2.163  | 1.648 | 1.860  | 1.956      | 2.067 | 2.132  | 1.648                          | 2.163  | 1.971  | 26.1%                    | 2.127    |
| 920 East & West Windows                            | 3.500  | 2.956 | 3.259  | 3.337      | 3.300 | 3.607  | 2.956                          | 3.607  | 3.326  | 19.6%                    | 3.589    |
| 930 E&W Windows + Overhang & Fins                  | 4.270  | 3.524 | 3.933  | 3.994      | 4.278 | 4.384  | 3.524                          | 4.384  | 4.064  | 21.2%                    | 4.369    |
| 940 Case 900 with Htg Temp. Setback                | 1.389  | 0.863 | 1.149  | 1.067      | 1.015 | 1.169  | 0.863                          | 1.389  | 1.109  | 47.4%                    | 1.157    |
| 950 Case 900 with Night Ventilation                | 0.000  | 0.000 | 0.000  | 0.000      | 0.000 | 0.000  | 0.000                          | 0.000  | 0.000  | ---                      | 0.000    |
| 960 Sunspace                                       |        | 2.522 | 2.771  | 2.689      | 2.624 | 2.860  | 2.522                          | 2.860  | 2.693  | 12.5%                    | 2.850    |
| 980 Case 900 with Increased Insulation             | 0.720  | 0.246 | 0.266  | 0.411      | 0.351 | 0.450  | 0.246                          | 0.720  | 0.407  | 116.4%                   | 0.450    |
| 985 Case 900 with "20/20" Thermostat               | 2.801  | 2.120 | 2.279  | 2.369      | 2.283 | 2.536  | 2.120                          | 2.801  | 2.398  | 28.4%                    | 2.526    |
| 995 Case 985 with Increased Insulation             | 1.330  | 0.755 | 0.770  | 1.006      | 0.905 | 1.077  | 0.755                          | 1.330  | 0.974  | 59.0%                    | 1.076    |
| 195 Solid Conduction                               | 4.217  | 3.990 | 4.157  | 4.070      | 3.951 | 4.094  | 3.951                          | 4.217  | 4.080  | 6.5%                     | 4.091    |
| 200 Surface Convection (Int & Ext IR="off")        | 5.041  | 4.813 | 5.226  | 5.105      | 4.920 | 5.143  | 4.813                          | 5.226  | 5.042  | 8.2%                     | 5.156    |
| 210 Infrared Radiation (Int IR="off", Ext IR="on") | 5.627  | 5.966 | 6.531  | 6.047      | 6.317 | 6.429  | 5.627                          | 6.531  | 6.153  | 14.7%                    | 6.449    |
| 215 Infrared Radiation (Int IR="on", Ext IR="off") | 5.652  | 5.307 | 5.697  | 5.405      | 5.181 | 5.443  | 5.181                          | 5.697  | 5.448  | 9.5%                     | 5.463    |
| 220 In-Depth Base Case                             | 6.377  | 6.666 | 7.178  | 6.455      | 6.726 | 6.868  | 6.377                          | 7.178  | 6.712  | 11.9%                    | 6.899    |
| 230 Infiltration                                   | 9.851  | 9.812 | 10.417 | 9.930      | 9.939 | 10.234 | 9.812                          | 10.417 | 10.031 | 6.0%                     | 10.265   |
| 240 Internal Gains                                 | 5.116  | 5.443 | 5.944  | 5.279      | 5.539 | 5.657  | 5.116                          | 5.944  | 5.496  | 15.1%                    | 5.688    |
| 250 Exterior Shortwave Absorptance                 | 4.733  | 5.044 | 5.373  | 4.899      | 4.935 | 5.105  | 4.733                          | 5.373  | 5.015  | 12.8%                    | 5.126    |
| 270 South Solar Windows                            |        | 4.346 | 4.273  | 4.385      | 4.576 | 4.631  | 4.273                          | 4.631  | 4.442  | 8.1%                     | 4.627    |
| 280 Cavity Albedo                                  |        | 4.525 | 4.619  | 4.570      | 4.738 | 4.870  | 4.525                          | 4.870  | 4.664  | 7.4%                     | 4.866    |
| 290 South Shading                                  |        | 4.424 | 4.381  | 4.424      | 4.745 | 4.725  | 4.381                          | 4.745  | 4.540  | 8.0%                     | 4.722    |
| 300 East/West Window                               |        | 4.318 | 4.460  | 4.425      | 4.668 | 4.726  | 4.318                          | 4.726  | 4.519  | 9.0%                     | 4.722    |
| 310 East/West Shading                              |        | 4.580 | 4.846  | 4.691      | 5.240 | 5.163  | 4.580                          | 5.240  | 4.904  | 13.4%                    | 5.161    |
| 320 Thermostat                                     |        | 3.677 | 3.599  | 3.771      | 3.970 | 4.031  | 3.599                          | 4.031  | 3.810  | 11.3%                    | 4.027    |
| 395 Low Mass Solid Conduction                      | 4.565  | 4.855 | 5.145  | 4.641      | 4.866 | 4.908  | 4.565                          | 5.145  | 4.830  | 12.0%                    | 4.904    |
| 400 Low Mass High Cond. Wall Elements              | 5.906  | 6.536 | 7.047  | 6.348      | 6.610 | 6.769  | 5.906                          | 7.047  | 6.536  | 17.5%                    | 6.800    |
| 410 Low Mass Infiltration                          | 7.630  | 8.045 | 8.661  | 8.080      | 8.212 | 8.445  | 7.630                          | 8.661  | 8.179  | 12.6%                    | 8.476    |
| 420 Low Mass Internal Gains                        | 6.399  | 6.834 | 7.433  | 6.906      | 7.027 | 7.236  | 6.399                          | 7.433  | 6.973  | 14.8%                    | 7.268    |
| 430 Low Mass Ext. Shortwave Absorptance            | 5.171  | 5.454 | 5.954  | 5.620      | 5.545 | 5.851  | 5.171                          | 5.954  | 5.599  | 14.0%                    | 5.872    |
| 440 Low Mass Cavity Albedo                         |        | 4.156 | 4.330  | 4.500      | 4.504 | 4.721  | 4.156                          | 4.721  | 4.442  | 12.7%                    | 4.717    |
| 450 Constant Interior and Exterior Surf Coeffs     | 3.743  | 3.990 | 3.375  | 3.962      | 3.850 | 3.871  | 3.375                          | 3.990  | 3.799  | 16.2%                    | 3.869    |
| 460 Constant Interior Surface Coefficients         | 3.828  | 4.056 | 3.873  | 4.194      | 4.263 | 4.290  | 3.828                          | 4.290  | 4.084  | 11.3%                    | 4.287    |
| 470 Constant Exterior Surface Coefficients         | 4.042  | 3.899 | 3.540  | 4.094      | 3.960 | 4.075  | 3.540                          | 4.094  | 3.935  | 14.1%                    | 4.072    |
| 800 High Mass High Cond. Wall Elements             | 5.141  | 4.906 | 5.403  | 5.116      | 4.980 | 5.369  | 4.906                          | 5.403  | 5.152  | 9.7%                     | 5.370    |
| 810 High Mass Cavity Albedo                        |        | 2.038 | 2.454  | 2.342      | 2.185 | 2.610  | 2.038                          | 2.610  | 2.326  | 24.6%                    | 2.595    |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]



**ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results**

**By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-2. Annual Sensible Cooling Loads (MWh)**

| Simulation Model:<br>Case                          | BSIMAC | CSE   | DeST  | EnergyPlus | ESP-r | TRNSYS | Statistics for Example Results |       |       |                          | TRNSYS18 |
|--|--------|-------|-------|------------|-------|--------|--------------------------------|-------|-------|--------------------------|----------|
|  |        |       |       |            |       |        | Min                            | Max   | Mean  | (Max-Min)/<br>Mean** (%) |          |
| 600 Base Case, South Windows                       | 5.822  | 5.913 | 5.432 | 6.027      | 6.162 | 5.780  | 5.432                          | 6.162 | 5.856 | 12.5%                    | 5.779    |
| 610 S. Windows + Overhang                          | 4.299  | 4.382 | 4.173 | 4.333      | 4.233 | 4.117  | 4.117                          | 4.382 | 4.256 | 6.2%                     | 4.105    |
| 620 East & West Windows                            | 4.404  | 4.079 | 3.909 | 4.060      | 4.246 | 3.841  | 3.841                          | 4.404 | 4.090 | 13.8%                    | 3.839    |
| 630 E&W Windows + Overhang & Fins                  | 3.074  | 3.020 | 2.787 | 2.836      | 2.595 | 2.573  | 2.573                          | 3.074 | 2.814 | 17.8%                    | 2.568    |
| 640 Case 600 with Htg Temp. Setback                | 5.804  | 5.644 | 5.237 | 5.763      | 5.893 | 5.477  | 5.237                          | 5.893 | 5.636 | 11.6%                    | 5.477    |
| 650 Case 600 with Night Ventilation                | 4.629  | 4.654 | 4.186 | 4.817      | 4.945 | 4.632  | 4.186                          | 4.945 | 4.644 | 16.3%                    | 4.632    |
| 660 Low-E Windows                                  | 3.014  | 3.340 | 3.260 | 3.232      | 3.219 | 2.966  | 2.966                          | 3.340 | 3.172 | 11.8%                    | 2.966    |
| 670 Single-Pane Windows                            | 6.539  | 6.578 | 5.954 | 6.623      | 6.520 | 6.198  | 5.954                          | 6.623 | 6.402 | 10.4%                    | 6.198    |
| 680 Case 600 with Increased Insulation             | 5.938  | 6.430 | 5.932 | 6.444      | 6.529 | 6.310  | 5.932                          | 6.529 | 6.264 | 9.5%                     | 6.310    |
| 685 Case 600 with "20/20" Thermostat               | 9.130  | 8.859 | 8.238 | 9.119      | 9.121 | 8.851  | 8.238                          | 9.130 | 8.886 | 10.0%                    | 8.851    |
| 695 Case 685 with Increased Insulation             | 8.755  | 8.974 | 8.386 | 9.172      | 9.149 | 9.039  | 8.386                          | 9.172 | 8.912 | 8.8%                     | 9.039    |
| 900 South Windows                                  | 2.714  | 2.464 | 2.383 | 2.489      | 2.488 | 2.267  | 2.267                          | 2.714 | 2.467 | 18.1%                    | 2.267    |
| 910 S. Windows + Overhang                          | 1.484  | 1.415 | 1.490 | 1.383      | 1.283 | 1.191  | 1.191                          | 1.490 | 1.374 | 21.8%                    | 1.187    |
| 920 East & West Windows                            | 3.128  | 2.789 | 2.706 | 2.731      | 2.814 | 2.549  | 2.549                          | 3.128 | 2.786 | 20.8%                    | 2.547    |
| 930 E&W Windows + Overhang & Fins                  | 2.161  | 2.075 | 1.908 | 1.919      | 1.654 | 1.672  | 1.654                          | 2.161 | 1.898 | 26.7%                    | 1.668    |
| 940 Case 900 with Htg. Temp. Setback               | 2.613  | 2.397 | 2.343 | 2.424      | 2.428 | 2.203  | 2.203                          | 2.613 | 2.401 | 17.1%                    | 2.203    |
| 950 Case 900 with Night Ventilation                | 0.586  | 0.598 | 0.618 | 0.707      | 0.656 | 0.642  | 0.586                          | 0.707 | 0.634 | 19.1%                    | 0.642    |
| 960 Sunspace                                       |        | 0.926 | 0.909 | 0.907      | 0.950 | 0.789  | 0.789                          | 0.950 | 0.896 | 17.9%                    | 0.789    |
| 980 Case 900 with Increased Insulation             | 3.501  | 3.995 | 3.758 | 3.712      | 3.775 | 3.519  | 3.501                          | 3.995 | 3.710 | 13.3%                    | 3.518    |
| 985 Case 900 with "20/20" Thermostat               | 7.273  | 6.234 | 5.880 | 6.359      | 6.249 | 6.113  | 5.880                          | 7.273 | 6.351 | 21.9%                    | 6.115    |
| 995 Case 985 with Increased Insulation             | 7.482  | 7.202 | 6.771 | 7.203      | 7.149 | 7.064  | 6.771                          | 7.482 | 7.145 | 10.0%                    | 7.064    |
| 195 Solid Conduction                               | 0.712  | 0.606 | 0.628 | 0.612      | 0.611 | 0.592  | 0.592                          | 0.712 | 0.627 | 19.2%                    | 0.592    |
| 200 Surface Convection (Int & Ext IR="off")        | 0.839  | 0.800 | 0.835 | 0.814      | 0.800 | 0.788  | 0.788                          | 0.839 | 0.813 | 6.2%                     | 0.791    |
| 210 Infrared Radiation (Int IR="off", Ext IR="on") | 0.688  | 0.503 | 0.496 | 0.560      | 0.519 | 0.459  | 0.459                          | 0.688 | 0.537 | 42.6%                    | 0.461    |
| 215 Infrared Radiation (Int IR="on", Ext IR="off") | 0.952  | 0.946 | 0.922 | 0.877      | 0.895 | 0.850  | 0.850                          | 0.952 | 0.907 | 11.2%                    | 0.855    |
| 220 In-Depth Base Case                             | 0.803  | 0.611 | 0.550 | 0.610      | 0.576 | 0.498  | 0.498                          | 0.803 | 0.608 | 50.2%                    | 0.500    |
| 230 Infiltration                                   | 1.184  | 0.991 | 0.929 | 0.991      | 0.955 | 0.897  | 0.897                          | 1.184 | 0.991 | 29.0%                    | 0.900    |
| 240 Internal Gains                                 | 1.287  | 0.982 | 0.876 | 0.979      | 0.922 | 0.834  | 0.834                          | 1.287 | 0.980 | 46.2%                    | 0.836    |
| 250 Exterior Shortwave Absorptance                 | 3.612  | 3.429 | 3.471 | 3.182      | 3.467 | 2.904  | 2.904                          | 3.612 | 3.344 | 21.2%                    | 2.930    |
| 270 South Solar Windows                            |        | 7.271 | 6.698 | 7.522      | 7.309 | 7.289  | 6.698                          | 7.522 | 7.217 | 11.4%                    | 7.288    |
| 280 Cavity Albedo                                  |        | 4.996 | 4.215 | 5.183      | 5.206 | 4.808  | 4.215                          | 5.206 | 4.882 | 20.3%                    | 4.808    |
| 290 South Shading                                  |        | 5.610 | 5.310 | 5.743      | 5.321 | 5.461  | 5.310                          | 5.743 | 5.489 | 7.9%                     | 5.447    |
| 300 East/West Window                               |        | 5.055 | 4.805 | 5.152      | 5.038 | 4.913  | 4.805                          | 5.152 | 4.993 | 7.0%                     | 4.911    |
| 310 East/West Shading                              |        | 3.752 | 3.402 | 3.669      | 3.128 | 3.324  | 3.128                          | 3.752 | 3.455 | 18.1%                    | 3.317    |
| 320 Thermostat                                     |        | 4.859 | 4.420 | 4.986      | 4.913 | 4.788  | 4.420                          | 4.986 | 4.793 | 11.8%                    | 4.787    |
| 395 Low Mass Solid Conduction                      | 0.021  | 0.008 | 0.006 | 0.010      | 0.006 | 0.004  | 0.004                          | 0.021 | 0.009 | 193.7%                   | 0.004    |
| 400 Low Mass High Cond. Wall Elements              | 0.063  | 0.023 | 0.017 | 0.031      | 0.024 | 0.013  | 0.013                          | 0.063 | 0.028 | 176.6%                   | 0.013    |
| 410 Low Mass Infiltration                          | 0.096  | 0.048 | 0.041 | 0.057      | 0.052 | 0.035  | 0.035                          | 0.096 | 0.055 | 110.6%                   | 0.036    |
| 420 Low Mass Internal Gains                        | 0.228  | 0.141 | 0.119 | 0.153      | 0.142 | 0.109  | 0.109                          | 0.228 | 0.149 | 79.8%                    | 0.110    |
| 430 Low Mass Ext. Shortwave Absorptance            | 1.084  | 0.906 | 0.944 | 0.856      | 0.953 | 0.739  | 0.739                          | 1.084 | 0.914 | 37.8%                    | 0.744    |
| 440 Low Mass Cavity Albedo                         |        | 3.985 | 3.458 | 4.085      | 4.414 | 3.741  | 3.458                          | 4.414 | 3.937 | 24.3%                    | 3.741    |
| 450 Constant Interior and Exterior Surf Coeffs     | 6.172  | 5.689 | 6.161 | 6.507      | 6.613 | 6.531  | 5.689                          | 6.613 | 6.279 | 14.7%                    | 6.529    |
| 460 Constant Interior Surface Coefficients         | 6.260  | 5.940 | 5.929 | 6.475      | 6.729 | 6.243  | 5.929                          | 6.729 | 6.263 | 12.8%                    | 6.242    |
| 470 Constant Exterior Surface Coefficients         | 5.987  | 5.644 | 5.649 | 6.029      | 6.005 | 6.056  | 5.644                          | 6.056 | 5.895 | 7.0%                     | 6.056    |
| 800 High Mass High Cond. Wall Elements             | 0.473  | 0.380 | 0.362 | 0.374      | 0.391 | 0.282  | 0.282                          | 0.473 | 0.377 | 50.6%                    | 0.284    |
| 810 High Mass Cavity Albedo                        |        | 1.481 | 1.357 | 1.508      | 1.606 | 1.295  | 1.295                          | 1.606 | 1.449 | 21.5%                    | 1.294    |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF

(TRNSYS18) vs. Annex B8, Section B8.1 Example Results

By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

Note: The statistics in the tables below are based on the listed example results.

These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-3. Annual Hourly Integrated Peak Heating Loads**

| Simulation Model:<br>Case                          | BSIMAC |     |        | CSE   |     |        | DeST  |     |        | EnergyPlus |     |        | ESP-r |     |        | TRNSYS |     |        | Example Result Statistics |           |            |                          | TRNSYS18 |     |        |
|--|--------|-----|--------|-------|-----|--------|-------|-----|--------|------------|-----|--------|-------|-----|--------|--------|-----|--------|---------------------------|-----------|------------|--------------------------|----------|-----|--------|
|  | kW     | Mo. | Day Hr | kW    | Mo. | Day Hr | kW    | Mo. | Day Hr | kW         | Mo. | Day Hr | kW    | Mo. | Day Hr | kW     | Mo. | Day Hr | Min<br>kW                 | Max<br>kW | Mean<br>kW | (Max-Min)/<br>Mean** (%) | kW       | Mo. | Day Hr |
| 600 Base Case, South Windows                       | 3.255  | Nov | 26 8   | 3.020 | Jan | 1 1    | 3.035 | Jan | 1 0    | 3.204      | Dec | 31 24  | 3.228 | Jan | 1 1    | 3.359  | Jan | 1 1    | 3.020                     | 3.359     | 3.184      | 10.6%                    | 3.278    | Dec | 31 24  |
| 610 S. Windows + Overhang                          | 3.166  | Nov | 26 8   | 3.021 | Jan | 1 1    | 3.039 | Jan | 1 0    | 3.192      | Dec | 31 24  | 3.233 | Jan | 1 1    | 3.360  | Jan | 1 1    | 3.021                     | 3.360     | 3.168      | 10.7%                    | 3.280    | Dec | 31 24  |
| 620 East & West Windows                            | 3.145  | Dec | 31 24  | 3.038 | Jan | 1 1    | 3.068 | Jan | 1 0    | 3.229      | Dec | 31 24  | 3.253 | Jan | 1 1    | 3.385  | Jan | 1 1    | 3.038                     | 3.385     | 3.186      | 10.9%                    | 3.326    | Dec | 31 24  |
| 630 E&W Windows + Overhang & Fins                  | 3.252  | Dec | 31 24  | 3.039 | Jan | 1 1    | 3.072 | Jan | 1 0    | 3.207      | Dec | 31 24  | 3.259 | Jan | 1 1    | 3.388  | Jan | 1 1    | 3.039                     | 3.388     | 3.203      | 10.9%                    | 3.331    | Dec | 31 24  |
| 640 Case 600 with Htg. Temp. Setback               | 4.633  | Feb | 8 9    | 4.222 | Nov | 26 8   | 4.658 | Nov | 26 7   | 4.559      | Nov | 26 8   | 4.101 | Nov | 26 8   | 4.039  | Nov | 26 8   | 4.039                     | 4.658     | 4.369      | 14.2%                    | 4.039    | Nov | 26 8   |
| 650 Case 600 with Night Ventilation                | 0.000  |     |        | 0.000 | Jan | 1 1    | 0.000 |     |        | 0.000      | Jan | 1 1    | 0.000 | Jan | 1 1    | 0.000  | Dec | 31 0   | 0.000                     | 0.000     | 0.000      | ----                     | 0.000    | Jan | 1 1    |
| 660 Low-E Windows                                  | 2.620  | Nov | 26 8   | 2.758 | Jan | 1 1    | 2.798 | Jan | 1 0    | 2.831      | Dec | 31 24  | 2.846 | Jan | 1 1    | 2.955  | Jan | 1 1    | 2.620                     | 2.955     | 2.801      | 12.0%                    | 2.869    | Dec | 31 24  |
| 670 Single-Pane Windows                            | 4.122  | Nov | 26 8   | 3.655 | Jan | 1 1    | 3.812 | Jan | 1 0    | 3.854      | Nov | 26 7   | 3.992 | Nov | 26 7   | 4.221  | Nov | 26 8   | 3.655                     | 4.221     | 3.943      | 14.3%                    | 4.221    | Nov | 26 8   |
| 680 Case 600 with Increased Insulation             | 2.126  | Nov | 26 8   | 1.778 | Feb | 9 6    | 1.811 | Jan | 1 1    | 2.052      | Nov | 26 7   | 2.022 | Feb | 9 7    | 2.115  | Nov | 26 8   | 1.778                     | 2.126     | 1.984      | 17.6%                    | 2.115    | Nov | 26 8   |
| 685 Case 600 with "20/20" Thermostat               | 3.169  | Nov | 26 8   | 3.032 | Jan | 1 1    | 3.054 | Jan | 1 0    | 3.223      | Dec | 31 24  | 3.247 | Jan | 1 1    | 3.374  | Jan | 1 1    | 3.032                     | 3.374     | 3.183      | 10.8%                    | 3.306    | Dec | 31 24  |
| 695 Case 685 with Increased Insulation             | 2.138  | Nov | 26 8   | 1.795 | Jan | 1 1    | 1.855 | Jan | 1 1    | 2.072      | Dec | 31 24  | 2.025 | Nov | 26 7   | 2.118  | Nov | 26 8   | 1.795                     | 2.138     | 2.000      | 17.1%                    | 2.118    | Nov | 26 8   |
| 900 South Windows                                  | 2.551  | Feb | 8 24   | 2.443 | Feb | 9 6    | 2.453 | Feb | 9 5    | 2.687      | Feb | 9 6    | 2.633 | Feb | 9 7    | 2.778  | Feb | 9 7    | 2.443                     | 2.778     | 2.591      | 12.9%                    | 2.779    | Feb | 9 7    |
| 910 S. Windows + Overhang                          | 2.761  | Feb | 8 24   | 2.469 | Feb | 9 6    | 2.474 | Feb | 9 5    | 2.699      | Feb | 9 6    | 2.684 | Feb | 9 7    | 2.799  | Feb | 9 6    | 2.469                     | 2.799     | 2.648      | 12.5%                    | 2.800    | Feb | 9 6    |
| 920 East & West Windows                            | 2.895  | Nov | 26 8   | 2.512 | Feb | 9 6    | 2.513 | Feb | 9 5    | 2.770      | Feb | 9 6    | 2.706 | Feb | 9 7    | 2.864  | Feb | 9 6    | 2.512                     | 2.895     | 2.710      | 14.1%                    | 2.864    | Feb | 9 6    |
| 930 E&W Windows + Overhang & Fins                  | 2.968  | Dec | 31 24  | 2.537 | Feb | 9 6    | 2.549 | Feb | 9 5    | 2.785      | Feb | 9 6    | 2.765 | Feb | 9 6    | 2.900  | Feb | 9 6    | 2.537                     | 2.968     | 2.751      | 15.7%                    | 2.901    | Feb | 9 6    |
| 940 Case 900 with Htg. Temp. Setback               | 3.882  | Feb | 8 9    | 3.052 | Jan | 1 9    | 3.659 | Feb | 9 7    | 3.143      | Dec | 31 9   | 3.122 | Feb | 9 9    | 3.405  | Jan | 1 9    | 3.052                     | 3.882     | 3.377      | 24.6%                    | 3.196    | Nov | 3 9    |
| 950 Case 900 with Night Ventilation                | 0.000  |     |        | 0.000 | Jan | 1 1    | 0.000 |     |        | 0.000      | Jan | 1 1    | 0.000 | Jan | 1 1    | 0.000  | Dec | 31 0   | 0.000                     | 0.000     | 0.000      | ----                     | 0.000    | Jan | 1 1    |
| 960 Sunspace                                       |        |     |        | 2.132 | Feb | 9 6    | 2.085 | Jan | 1 0    | 2.259      | Feb | 9 6    | 2.201 | Feb | 9 6    | 2.300  | Feb | 9 6    | 2.085                     | 2.300     | 2.196      | 9.8%                     | 2.300    | Feb | 9 6    |
| 980 Case 900 with Increased Insulation             | 1.693  | Feb | 8 24   | 1.254 | Feb | 9 6    | 1.382 | Feb | 9 5    | 1.538      | Feb | 9 6    | 1.473 | Feb | 9 7    | 1.592  | Feb | 9 7    | 1.254                     | 1.693     | 1.489      | 29.5%                    | 1.592    | Feb | 9 7    |
| 985 Case 900 with "20/20" Thermostat               | 2.754  | Feb | 8 24   | 2.452 | Feb | 9 6    | 2.458 | Feb | 9 5    | 2.695      | Feb | 9 6    | 2.642 | Feb | 9 7    | 2.785  | Feb | 9 6    | 2.452                     | 2.785     | 2.631      | 12.7%                    | 2.786    | Feb | 9 6    |
| 995 Case 985 with Increased Insulation             | 1.711  | Nov | 26 8   | 1.370 | Feb | 9 6    | 1.462 | Feb | 9 5    | 1.622      | Feb | 9 6    | 1.560 | Feb | 9 7    | 1.662  | Feb | 9 6    | 1.370                     | 1.711     | 1.564      | 21.8%                    | 1.662    | Feb | 9 6    |
| 195 Solid Conduction                               | 1.802  | Dec | 31 24  | 1.791 | Jan | 1 1    | 1.799 | Jan | 1 0    | 1.794      | Dec | 31 24  | 1.802 | Jan | 1 1    | 1.796  | Jan | 1 1    | 1.791                     | 1.802     | 1.797      | 0.6%                     | 1.792    | Dec | 31 24  |
| 200 Surface Convection (Int & Ext IR="off")        | 2.272  | Nov | 26 8   | 2.226 | Nov | 26 8   | 2.308 | Jan | 1 0    | 2.341      | Nov | 26 8   | 2.275 | Dec | 31 24  | 2.353  | Nov | 26 8   | 2.226                     | 2.353     | 2.296      | 5.5%                     | 2.362    | Nov | 26 8   |
| 210 Infrared Radiation (Int IR="off", Ext IR="on") | 2.374  | Dec | 31 24  | 2.629 | Jan | 1 2    | 2.605 | Jan | 1 0    | 2.565      | Dec | 31 24  | 2.671 | Jan | 1 1    | 2.750  | Jan | 1 1    | 2.374                     | 2.750     | 2.599      | 14.5%                    | 2.705    | Dec | 31 24  |
| 215 Infrared Radiation (Int IR="on", Ext IR="off") | 2.521  | Nov | 26 8   | 2.420 | Nov | 26 8   | 2.520 | Jan | 1 0    | 2.478      | Nov | 26 8   | 2.390 | Nov | 26 8   | 2.489  | Nov | 26 8   | 2.390                     | 2.521     | 2.470      | 5.3%                     | 2.503    | Nov | 26 8   |
| 220 In-Depth Base Case                             | 2.631  | Nov | 26 8   | 2.839 | Jan | 1 1    | 2.863 | Jan | 1 0    | 2.692      | Dec | 31 24  | 2.788 | Jan | 1 1    | 2.879  | Jan | 1 1    | 2.631                     | 2.879     | 2.782      | 8.9%                     | 2.835    | Dec | 31 24  |
| 230 Infiltration                                   | 4.219  | Dec | 31 24  | 4.133 | Jan | 1 1    | 4.223 | Jan | 1 0    | 4.316      | Dec | 31 24  | 4.160 | Jan | 1 1    | 4.315  | Jan | 1 1    | 4.133                     | 4.316     | 4.228      | 4.3%                     | 4.277    | Dec | 31 24  |
| 240 Internal Gains                                 | 2.431  | Nov | 26 8   | 2.651 | Jan | 1 1    | 2.685 | Jan | 1 0    | 2.507      | Dec | 31 24  | 2.605 | Jan | 1 1    | 2.693  | Jan | 1 1    | 2.431                     | 2.693     | 2.595      | 10.1%                    | 2.650    | Dec | 31 24  |
| 250 Exterior Shortwave Absorptance                 | 2.631  | Nov | 26 8   | 2.837 | Jan | 1 1    | 2.855 | Jan | 1 0    | 2.687      | Dec | 31 24  | 2.780 | Jan | 1 1    | 2.874  | Jan | 1 1    | 2.631                     | 2.874     | 2.777      | 8.8%                     | 2.828    | Dec | 31 24  |
| 270 South Solar Windows                            |        |     |        | 2.611 | Jan | 1 2    | 2.560 | Jan | 1 1    | 2.597      | Dec | 31 24  | 2.748 | Jan | 1 1    | 2.843  | Jan | 1 2    | 2.560                     | 2.843     | 2.672      | 10.6%                    | 2.772    | Dec | 31 24  |
| 280 Cavity Albedo                                  |        |     |        | 2.612 | Jan | 1 2    | 2.568 | Jan | 1 1    | 2.602      | Dec | 31 24  | 2.752 | Jan | 1 1    | 2.849  | Jan | 1 1    | 2.568                     | 2.849     | 2.677      | 10.5%                    | 2.783    | Dec | 31 24  |
| 290 South Shading                                  |        |     |        | 2.611 | Jan | 1 2    | 2.561 | Jan | 1 1    | 2.583      | Dec | 31 24  | 2.750 | Jan | 1 1    | 2.843  | Jan | 1 2    | 2.561                     | 2.843     | 2.670      | 10.6%                    | 2.773    | Dec | 31 24  |
| 300 East/West Window                               |        |     |        | 2.614 | Jan | 1 1    | 2.589 | Jan | 1 0    | 2.603      | Dec | 31 24  | 2.766 | Jan | 1 1    | 2.854  | Jan | 1 1    | 2.589                     | 2.854     | 2.685      | 9.9%                     | 2.794    | Dec | 31 24  |
| 310 East/West Shading                              |        |     |        | 2.615 | Jan | 1 1    | 2.592 | Jan | 1 0    | 2.580      | Dec | 31 24  | 2.771 | Jan | 1 1    | 2.856  | Jan | 1 1    | 2.580                     | 2.856     | 2.683      | 10.3%                    | 2.798    | Dec | 31 24  |
| 320 Thermostat                                     |        |     |        | 2.609 | Jan | 1 1    | 2.546 | Jan | 1 1    | 2.573      | Dec | 31 24  | 2.733 | Jan | 1 2    | 2.834  | Jan | 1 2    | 2.546                     | 2.834     | 2.659      | 10.8%                    | 2.749    | Feb | 9 6    |
| 395 Low Mass Solid Conduction                      | 1.948  | Dec | 31 24  | 2.157 | Jan | 1 2    | 2.085 | Jan | 1 1    | 1.952      | Dec | 31 24  | 2.090 | Jan | 1 2    | 2.161  | Jan | 1 2    | 1.948                     | 2.161     | 2.066      | 10.3%                    | 2.041    | Dec | 31 24  |
| 400 Low Mass High Cond. Wall Elements              | 2.559  | Nov | 26 8   | 2.839 | Jan | 1 1    | 2.863 | Jan | 1 0    | 2.692      | Dec | 31 24  | 2.788 | Jan | 1 1    | 2.879  | Jan | 1 1    | 2.559                     | 2.879     | 2.770      | 11.5%                    | 2.835    | Dec | 31 24  |
| 410 Low Mass Infiltration                          | 3.338  | Dec | 31 24  | 3.441 | Jan | 1 1    | 3.543 | Jan | 1 0    | 3.504      | Dec | 31 24  | 3.473 | Jan | 1 1    | 3.597  | Jan | 1 1    | 3.338                     | 3.597     | 3.483      | 7.4%                     | 3.556    | Dec | 31 24  |
| 420 Low Mass Internal Gains                        | 3.138  | Dec | 31 24  | 3.256 | Jan | 1 1    | 3.365 | Jan | 1 0    | 3.319      | Dec | 31 24  | 3.290 | Jan | 1 1    | 3.411  | Jan | 1 1    | 3.138                     | 3.411     | 3.297      | 8.3%                     | 3.371    | Dec | 31 24  |
| 430 Low Mass Ext. Shortwave Absorptance            | 3.300  | Dec | 31 24  | 3.254 | Jan | 1 1    | 3.360 | Jan | 1 0    | 3.316      | Dec | 31 24  | 3.285 | Jan | 1 1    | 3.409  | Jan | 1 1    | 3.254                     | 3.409     | 3.321      | 4.7%                     | 3.366    | Dec | 31 24  |
| 440 Low Mass Cavity Albedo                         |        |     |        | 3.027 | Jan | 1 1    | 3.060 | Jan | 1 0    | 3.219      | Dec | 31 24  | 3.237 | Jan | 1 1    | 3.374  | Jan | 1 1    | 3.027                     | 3.374     | 3.183      | 10.9%                    | 3.306    | Dec | 31 24  |
| 450 Constant Interior and Exterior Surf Coeffs     | 2.989  | Nov | 26 8   | 2.978 | Jan | 1 1    | 2.753 | Jan | 1 0    | 3.100      | Dec | 31 24  | 3.042 | Jan | 1 1    | 3.037  | Jan | 1 1    | 2.753                     | 3.100     | 2.983      | 11.6%                    | 2.978    | Dec | 31 24  |
| 460 Constant Interior Surface Coefficients         | 3.055  | Nov | 26 8   | 2.971 | Jan | 1 1    | 2.980 | Jan | 1 0    | 3.091      | Dec | 31 24  | 3.101 | Jan | 1 1    | 3.160  | Jan | 1 1    | 2.971                     | 3.160     | 3.060      | 6.2%                     | 3.092    | Dec | 31 24  |
| 470 Constant Exterior Surface Coefficients         | 3.118  | Nov | 26 8   | 3.001 | Jan | 1 1    | 2.807 | Jan | 1 0    | 3.207      | Dec | 31 24  | 3.169 | Jan | 1 1    | 3.231  | Jan | 1 1    | 2.807                     | 3.231     | 3.089      | 13.7%                    | 3.163    | Dec | 31 24  |
| 800 High Mass High Cond. Wall Elements             | 2.957  | Dec | 31 24  | 2.778 | Feb | 9 6    | 2.864 | Feb | 9 5    | 2.924      | Feb | 9 6    | 2.840 | Feb | 9 7    | 2.967  | Feb | 9 6    | 2.778                     | 2.967     | 2.888      | 6.6%                     | 2.980    | Feb | 9 6    |
| 810 High Mass Cavity Albedo                        |        |     |        | 2.500 | Feb | 9 6    | 2.512 | Feb | 9 5    | 2.749      | Feb | 9 6    | 2.695 | Feb | 9 7    | 2.845  | Feb | 9 6    | 2.500                     | 2.845     | 2.660      | 13.0%                    | 2.845    | Feb | 9 6    |

\*\* ABSJ (Max-Min) / (Mean of Example Simulation Results)

**ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-4. Annual Hourly Integrated Peak Sensible Cooling Loads**

| Simulation Model:<br>Case                          | BSIMAC |     |     |    | CSE   |     |     |    | DeST  |     |     |    | EnergyPlus |     |     |    | ESP-r |     |     |    | TRNSYS |     |     |    | Example Result Statistics |       |       |       | TRNSYS18 |        |         |                      |    |     |     |
|--|--------|-----|-----|----|-------|-----|-----|----|-------|-----|-----|----|------------|-----|-----|----|-------|-----|-----|----|--------|-----|-----|----|---------------------------|-------|-------|-------|----------|--------|---------|----------------------|----|-----|-----|
|  | kW     | Mo. | Day | Hr | kW    | Mo. | Day | Hr | kW    | Mo. | Day | Hr | kW         | Mo. | Day | Hr | kW    | Mo. | Day | Hr | kW     | Mo. | Day | Hr | kW                        | Mo.   | Day   | Hr    | Min kW   | Max kW | Mean kW | (Max-Min)/Mean** (%) | kW | Mo. | Day |
| 600 Base Case, South Windows                       | 5.650  | Jan | 22  | 15 | 6.481 | Jan | 22  | 14 | 5.422 | Jan | 22  | 14 | 6.352      | Jan | 22  | 14 | 6.193 | Jan | 22  | 14 | 6.046  | Jan | 22  | 14 | 5.422                     | 6.481 | 6.024 | 17.6% | 6.045    | Jan    | 22      | 14                   |    |     |     |
| 610 S. Windows + Overhang                          | 5.466  | Jan | 22  | 15 | 6.432 | Dec | 1   | 14 | 5.331 | Jan | 22  | 14 | 6.135      | Dec | 1   | 14 | 5.934 | Jan | 22  | 14 | 5.868  | Dec | 1   | 14 | 5.331                     | 6.432 | 5.861 | 18.8% | 5.812    | Dec    | 1       | 14                   |    |     |     |
| 620 East & West Windows                            | 4.704  | Jun | 26  | 18 | 4.493 | Jun | 26  | 17 | 3.955 | Jun | 26  | 17 | 4.797      | Jun | 26  | 17 | 4.622 | Jun | 26  | 17 | 4.588  | Jun | 26  | 17 | 3.955                     | 4.797 | 4.527 | 18.6% | 4.588    | Jun    | 26      | 17                   |    |     |     |
| 630 E&W Windows + Overhang & Fins                  | 4.121  | Jun | 26  | 18 | 3.998 | Jun | 26  | 18 | 3.526 | Jun | 26  | 17 | 4.212      | Jun | 26  | 17 | 3.971 | Jun | 26  | 17 | 3.949  | Jun | 26  | 17 | 3.526                     | 4.212 | 3.963 | 17.3% | 3.944    | Jun    | 26      | 17                   |    |     |     |
| 640 Case 600 with Htg. Temp. Setback               | 5.650  | Jan | 22  | 15 | 6.429 | Jan | 22  | 14 | 5.365 | Jan | 22  | 14 | 6.297      | Jan | 22  | 14 | 6.127 | Jan | 22  | 14 | 5.967  | Jan | 22  | 14 | 5.365                     | 6.429 | 5.973 | 17.8% | 5.967    | Jan    | 22      | 14                   |    |     |     |
| 650 Case 600 with Night Ventilation                | 5.648  | Jan | 22  | 15 | 6.290 | Dec | 1   | 14 | 5.045 | Oct | 18  | 14 | 6.138      | Oct | 18  | 14 | 5.961 | Oct | 18  | 14 | 5.797  | Oct | 18  | 14 | 5.045                     | 6.290 | 5.813 | 21.4% | 5.797    | Oct    | 18      | 14                   |    |     |     |
| 660 Low-E Windows                                  | 3.343  | Oct | 18  | 15 | 3.933 | Oct | 1   | 13 | 3.355 | Oct | 11  | 14 | 3.770      | Oct | 18  | 14 | 3.530 | Oct | 1   | 14 | 3.457  | Oct | 18  | 14 | 3.343                     | 3.933 | 3.565 | 16.6% | 3.457    | Oct    | 18      | 14                   |    |     |     |
| 670 Single-Pane Windows                            | 6.217  | Oct | 18  | 14 | 6.925 | Oct | 1   | 13 | 5.839 | Oct | 10  | 13 | 6.806      | Jan | 22  | 14 | 6.482 | Oct | 18  | 14 | 6.401  | Oct | 18  | 14 | 5.839                     | 6.925 | 6.445 | 16.9% | 6.401    | Oct    | 18      | 14                   |    |     |     |
| 680 Case 600 with Increased Insulation             | 5.761  | Jan | 22  | 15 | 7.051 | Jan | 22  | 14 | 5.861 | Jan | 22  | 14 | 6.770      | Jan | 22  | 14 | 6.676 | Jan | 22  | 14 | 6.557  | Jan | 22  | 14 | 5.761                     | 7.051 | 6.446 | 20.0% | 6.557    | Jan    | 22      | 14                   |    |     |     |
| 685 Case 600 with "20/20" Thermostat               | 6.318  | Jan | 22  | 15 | 7.159 | Jan | 22  | 14 | 6.071 | Jan | 22  | 14 | 7.107      | Jan | 22  | 14 | 6.934 | Jan | 22  | 14 | 6.867  | Jan | 22  | 14 | 6.071                     | 7.159 | 6.743 | 16.1% | 6.867    | Jan    | 22      | 14                   |    |     |     |
| 695 Case 685 with Increased Insulation             | 6.232  | Jan | 22  | 15 | 7.541 | Jan | 22  | 14 | 6.355 | Jan | 22  | 14 | 7.334      | Jan | 22  | 14 | 7.239 | Jan | 22  | 14 | 7.175  | Jan | 22  | 14 | 6.232                     | 7.541 | 6.979 | 18.8% | 7.175    | Jan    | 22      | 14                   |    |     |     |
| 900 South Windows                                  | 3.039  | Oct | 1   | 15 | 3.376 | Oct | 1   | 14 | 2.556 | Sep | 11  | 14 | 3.040      | Oct | 1   | 14 | 2.896 | Oct | 12  | 15 | 2.940  | Oct | 1   | 14 | 2.556                     | 3.376 | 2.975 | 27.6% | 2.940    | Oct    | 1       | 14                   |    |     |     |
| 910 S. Windows + Overhang                          | 2.493  | Oct | 18  | 14 | 2.722 | Oct | 2   | 15 | 2.103 | Oct | 12  | 14 | 2.222      | Oct | 18  | 15 | 2.212 | Oct | 2   | 15 | 2.081  | Oct | 12  | 15 | 2.081                     | 2.722 | 2.306 | 27.8% | 2.075    | Oct    | 12      | 15                   |    |     |     |
| 920 East & West Windows                            | 3.481  | Jun | 26  | 18 | 3.057 | Jun | 26  | 18 | 2.710 | Jun | 26  | 17 | 3.260      | Jun | 26  | 18 | 3.099 | Jun | 26  | 18 | 3.154  | Jun | 26  | 18 | 2.710                     | 3.481 | 3.127 | 24.7% | 3.154    | Jun    | 26      | 18                   |    |     |     |
| 930 E&W Windows + Overhang & Fins                  | 3.052  | Jun | 26  | 18 | 2.662 | Jun | 26  | 18 | 2.335 | Jun | 26  | 17 | 2.782      | Jun | 26  | 18 | 2.494 | Jun | 26  | 18 | 2.613  | Jun | 26  | 18 | 2.335                     | 3.052 | 2.656 | 27.0% | 2.612    | Jun    | 26      | 18                   |    |     |     |
| 940 Case 900 with Htg. Temp. Setback               | 3.158  | Oct | 1   | 15 | 3.376 | Oct | 1   | 14 | 2.556 | Sep | 11  | 14 | 3.040      | Oct | 1   | 14 | 2.891 | Oct | 12  | 15 | 2.938  | Oct | 1   | 14 | 2.556                     | 3.376 | 2.993 | 27.4% | 2.937    | Oct    | 1       | 14                   |    |     |     |
| 950 Case 900 with Night Ventilation                | 2.366  | Sep | 10  | 15 | 2.364 | Sep | 4   | 15 | 2.054 | Sep | 11  | 14 | 2.388      | Sep | 11  | 15 | 2.202 | Sep | 10  | 15 | 2.236  | Sep | 11  | 15 | 2.054                     | 2.388 | 2.268 | 14.7% | 2.236    | Sep    | 11      | 15                   |    |     |     |
| 960 Sunspace                                       |        |     |     |    | 1.377 | Jun | 26  | 17 | 1.367 | Jun | 26  | 16 | 1.480      | Jun | 26  | 17 | 1.403 | Jun | 26  | 17 | 1.338  | Jun | 26  | 17 | 1.338                     | 1.480 | 1.393 | 10.2% | 1.338    | Jun    | 26      | 17                   |    |     |     |
| 980 Case 900 with Increased Insulation             | 3.384  | Oct | 18  | 14 | 3.668 | Oct | 2   | 14 | 2.930 | Oct | 18  | 14 | 3.450      | Oct | 18  | 15 | 3.341 | Oct | 12  | 15 | 3.313  | Oct | 12  | 14 | 2.930                     | 3.668 | 3.348 | 22.0% | 3.312    | Oct    | 12      | 14                   |    |     |     |
| 985 Case 900 with "20/20" Thermostat               | 3.977  | Oct | 18  | 14 | 4.225 | Oct | 1   | 14 | 3.208 | Oct | 11  | 14 | 3.915      | Oct | 18  | 15 | 3.736 | Oct | 12  | 15 | 3.885  | Oct | 1   | 14 | 3.208                     | 4.225 | 3.824 | 26.6% | 3.885    | Oct    | 1       | 14                   |    |     |     |
| 995 Case 985 with Increased Insulation             | 4.129  | Jan | 22  | 14 | 4.224 | Jan | 22  | 15 | 3.315 | Jan | 22  | 14 | 4.177      | Jan | 22  | 15 | 3.954 | Jan | 22  | 15 | 4.115  | Jan | 22  | 15 | 3.315                     | 4.224 | 3.986 | 22.8% | 4.114    | Jan    | 22      | 15                   |    |     |     |
| 195 Solid Conduction                               | 1.118  | Jun | 26  | 17 | 0.994 | Jun | 26  | 17 | 0.973 | Jun | 26  | 16 | 1.041      | Jun | 26  | 17 | 0.944 | Jun | 26  | 17 | 0.994  | Jun | 26  | 17 | 0.944                     | 1.118 | 1.011 | 17.2% | 0.994    | Jun    | 26      | 17                   |    |     |     |
| 200 Surface Convection (Int & Ext IR="off")        | 1.271  | Jun | 26  | 17 | 1.215 | Jun | 26  | 17 | 1.239 | Jun | 26  | 16 | 1.307      | Jun | 26  | 17 | 1.198 | Jun | 26  | 17 | 1.259  | Jun | 26  | 17 | 1.198                     | 1.307 | 1.248 | 8.8%  | 1.263    | Jun    | 26      | 17                   |    |     |     |
| 210 Infrared Radiation (Int IR="off", Ext IR="on") | 1.193  | Jun | 26  | 17 | 0.946 | Jun | 13  | 15 | 0.937 | Jun | 26  | 16 | 1.084      | Jun | 26  | 17 | 0.877 | Jun | 14  | 14 | 0.884  | Jun | 26  | 18 | 0.877                     | 1.193 | 0.987 | 32.0% | 0.887    | Jun    | 26      | 18                   |    |     |     |
| 215 Infrared Radiation (Int IR="on", Ext IR="off") | 1.393  | Jun | 26  | 17 | 1.369 | Jun | 26  | 17 | 1.386 | Jun | 26  | 16 | 1.400      | Jun | 26  | 17 | 1.366 | Jun | 26  | 17 | 1.352  | Jun | 26  | 17 | 1.352                     | 1.400 | 1.378 | 3.5%  | 1.358    | Jun    | 26      | 17                   |    |     |     |
| 220 In-Depth Base Case                             | 1.336  | Jun | 26  | 18 | 1.108 | Jun | 13  | 15 | 1.040 | Jun | 26  | 16 | 1.184      | Jun | 26  | 18 | 1.012 | Jun | 14  | 15 | 0.968  | Jun | 26  | 18 | 0.968                     | 1.336 | 1.108 | 33.2% | 0.973    | Jun    | 26      | 18                   |    |     |     |
| 230 Infiltration                                   | 1.994  | Jun | 26  | 17 | 1.728 | Jun | 26  | 17 | 1.734 | Jun | 26  | 16 | 1.841      | Jun | 26  | 17 | 1.701 | Jun | 26  | 17 | 1.694  | Jun | 26  | 17 | 1.694                     | 1.994 | 1.782 | 16.9% | 1.699    | Jun    | 26      | 17                   |    |     |     |
| 240 Internal Gains                                 | 1.534  | Jun | 26  | 18 | 1.295 | Jun | 13  | 15 | 1.218 | Jun | 26  | 16 | 1.366      | Jun | 26  | 18 | 1.192 | Jun | 14  | 15 | 1.150  | Jun | 26  | 18 | 1.150                     | 1.534 | 1.292 | 29.7% | 1.155    | Jun    | 26      | 18                   |    |     |     |
| 250 Exterior Shortwave Absorptance                 | 2.913  | Sep | 12  | 14 | 2.790 | Sep | 12  | 14 | 2.751 | Sep | 3   | 14 | 2.867      | Sep | 12  | 14 | 3.034 | Sep | 12  | 14 | 2.688  | Sep | 12  | 14 | 2.688                     | 3.034 | 2.840 | 12.2% | 2.711    | Sep    | 12      | 14                   |    |     |     |
| 270 South Solar Windows                            |        |     |     |    | 7.011 | Jan | 22  | 14 | 5.832 | Jan | 22  | 14 | 6.839      | Jan | 22  | 14 | 6.613 | Jan | 22  | 14 | 6.637  | Jan | 22  | 14 | 5.832                     | 7.011 | 6.586 | 17.9% | 6.637    | Jan    | 22      | 14                   |    |     |     |
| 280 Cavity Albedo                                  |        |     |     |    | 4.765 | Jan | 22  | 14 | 3.768 | Dec | 1   | 13 | 4.727      | Jan | 22  | 14 | 4.676 | Jan | 22  | 14 | 4.400  | Jan | 22  | 14 | 3.768                     | 4.765 | 4.467 | 22.3% | 4.400    | Jan    | 22      | 14                   |    |     |     |
| 290 South Shading                                  |        |     |     |    | 6.872 | Jan | 22  | 14 | 5.739 | Jan | 22  | 14 | 6.595      | Jan | 22  | 14 | 6.411 | Jan | 22  | 14 | 6.402  | Jan | 22  | 14 | 5.739                     | 6.872 | 6.404 | 17.7% | 6.375    | Jan    | 22      | 14                   |    |     |     |
| 300 East/West Window                               |        |     |     |    | 4.163 | Jun | 26  | 17 | 3.695 | Jun | 26  | 17 | 4.475      | Jun | 26  | 17 | 4.221 | Jun | 26  | 17 | 4.278  | Jun | 26  | 17 | 3.695                     | 4.475 | 4.167 | 18.7% | 4.278    | Jun    | 26      | 17                   |    |     |     |
| 310 East/West Shading                              |        |     |     |    | 3.796 | Jun | 26  | 18 | 3.252 | Jun | 26  | 17 | 3.970      | Jun | 26  | 18 | 3.618 | Jun | 26  | 18 | 3.701  | Jun | 26  | 18 | 3.252                     | 3.970 | 3.667 | 19.6% | 3.699    | Jun    | 26      | 18                   |    |     |     |
| 320 Thermostat                                     |        |     |     |    | 6.473 | Jan | 22  | 14 | 5.304 | Jan | 22  | 14 | 6.209      | Jan | 22  | 14 | 5.993 | Jan | 22  | 14 | 5.949  | Jan | 22  | 14 | 5.304                     | 6.473 | 5.986 | 19.5% | 5.949    | Jan    | 22      | 14                   |    |     |     |
| 395 Low Mass Solid Conduction                      | 0.547  | Jun | 26  | 18 | 0.357 | Jun | 14  | 18 | 0.308 | Jun | 14  | 16 | 0.377      | Jun | 26  | 19 | 0.294 | Aug | 5   | 18 | 0.265  | Jun | 14  | 18 | 0.265                     | 0.547 | 0.358 | 78.7% | 0.265    | Jun    | 14      | 18                   |    |     |     |
| 400 Low Mass High Cond. Wall Elements              | 0.798  | Jun | 26  | 18 | 0.494 | Jun | 14  | 15 | 0.457 | Jun | 26  | 17 | 0.607      | Jun | 26  | 18 | 0.456 | Aug | 5   | 17 | 0.372  | Jun | 14  | 17 | 0.372                     | 0.798 | 0.531 | 80.3% | 0.374    | Jun    | 14      | 17                   |    |     |     |
| 410 Low Mass Infiltration                          | 1.011  | Jun | 26  | 17 | 0.700 | Jun | 26  | 18 | 0.709 | Jun | 26  | 16 | 0.828      | Jun | 26  | 18 | 0.624 | Jun | 26  | 18 | 0.604  | Jun | 26  | 18 | 0.604                     | 1.011 | 0.746 | 54.6% | 0.607    | Jun    | 26      | 18                   |    |     |     |
| 420 Low Mass Internal Gains                        | 1.208  | Jun | 26  | 17 | 0.909 | Jun | 26  | 18 | 0.917 | Jun | 26  | 16 | 1.033      | Jun | 26  | 18 | 0.836 | Jun | 26  | 17 | 0.814  | Jun | 26  | 18 | 0.814                     | 1.208 | 0.953 | 41.3% | 0.816    | Jun    | 26      | 18                   |    |     |     |
| 430 Low Mass Ext. Shortwave Absorptance            | 2.167  | Jun | 26  | 16 | 1.840 | Jun | 26  | 15 | 1.840 | Jun | 26  | 15 | 1.929      | Jun | 26  | 16 | 1.874 | Jul | 17  | 14 | 1.704  | Jun | 26  | 15 | 1.704                     | 2.167 | 1.892 | 24.5% | 1.712    | Jun    | 26      | 15                   |    |     |     |
| 440 Low Mass Cavity Albedo                         |        |     |     |    | 4.666 | Oct | 1   | 13 | 3.766 | Oct | 11  | 13 | 4.686      | Oct | 18  | 14 | 4.679 | Oct | 18  | 14 | 4.308  | Oct | 18  | 14 | 3.766                     | 4.666 | 4.421 | 20.8% | 4.308    | Oct    | 18      | 14                   |    |     |     |
| 450 Constant Interior and Exterior Surf Coeffs     | 5.812  | Jan | 22  | 15 | 6.180 | Jan | 22  | 14 | 6.063 | Jan | 22  | 13 | 6.466      | Jan | 22  | 14 | 6.501 | Jan | 22  | 14 | 6.313  | Jan | 22  | 14 | 5.812                     | 6.501 | 6.223 | 11.1% | 6.312    | Jan    | 22      | 14                   |    |     |     |
| 460 Constant Interior Surface Coefficients         | 5.804  | Jan | 22  | 15 | 6.243 | Jan | 22  | 14 | 5.902 | Jan | 22  | 13 | 6.374      | Jan | 22  | 14 | 6.304 | Jan | 22  | 14 | 6.069  | Jan | 22  | 14 | 5.804                     | 6.374 | 6.116 | 9.3%  | 6.068    | Jan    | 22      | 14                   |    |     |     |
| 470 Constant Exterior Surface Coefficients         | 5.695  | Jan | 22  | 15 | 6.388 | Jan | 22  | 14 | 5.570 | Jan | 22  | 14 | 6.444      | Jan | 22  | 14 | 6.407 | Jan | 22  | 14 | 6.320  | Jan | 22  | 14 | 5.695                     | 6.444 | 6.137 | 14.2% | 6.320    | Jan    | 22      | 14                   |    |     |     |
| 800 High Mass High Cond                            |        |     |     |    |       |     |     |    |       |     |     |    |            |     |     |    |       |     |     |    |        |     |     |    |                           |       |       |       |          |        |         |                      |    |     |     |

**ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-5. Free-Float Temperature Output**

| MAXIMUM ANNUAL HOURLY INTEGRATED ZONE TEMPERATURE |        |        |     |    |        |     |     |      |        |     |            |    |        |       |     |    |        |     |     |                           |               |               |                |                          |        |      |      |       |      |     |    |    |
|---|--------|--------|-----|----|--------|-----|-----|------|--------|-----|------------|----|--------|-------|-----|----|--------|-----|-----|---------------------------|---------------|---------------|----------------|--------------------------|--------|------|------|-------|------|-----|----|----|
| Simulation Model:                                 |        | BSIMAC |     |    | CSE    |     |     | DeST |        |     | EnergyPlus |    |        | ESP-r |     |    | TRNSYS |     |     | Example Result Statistics |               |               |                | TRNSYS18                 |        |      |      |       |      |     |    |    |
| Case  | T (°C) | Mo.    | Day | Hr | T (°C) | Mo. | Day | Hr   | T (°C) | Mo. | Day        | Hr | T (°C) | Mo.   | Day | Hr | T (°C) | Mo. | Day | Hr                        | Min<br>T (°C) | Max<br>T (°C) | Mean<br>T (°C) | (Max-Min)/<br>Mean** (%) | T (°C) | Mo.  | Day  | Hr    |      |     |    |    |
| 600FF - Low Mass with S. Windows                  | 63.4   | Oct    | 18  | 17 | 68.4   | Oct | 1   | 16   | 65.0   | Oct | 11         | 15 | 63.8   | Oct   | 18  | 16 | 64.6   | Oct | 1   | 16                        | 62.4          | Oct           | 1              | 15                       | 62.4   | 68.4 | 64.6 | 9.3%  | 62.4 | Oct | 1  | 15 |
| 900FF - High Mass with S. Windows                 | 46.0   | Oct    | 1   | 17 | 45.1   | Sep | 4   | 15   | 44.5   | Sep | 11         | 15 | 44.3   | Sep   | 12  | 15 | 44.3   | Sep | 12  | 15                        | 43.3          | Sep           | 12             | 15                       | 43.3   | 46.0 | 44.6 | 6.2%  | 43.3 | Sep | 12 | 15 |
| 650FF Case 600FF with Night Ventilation           | 62.1   | Oct    | 18  | 17 | 66.8   | Oct | 1   | 16   | 62.6   | Oct | 11         | 15 | 62.5   | Oct   | 18  | 16 | 63.3   | Oct | 1   | 16                        | 61.1          | Oct           | 1              | 15                       | 61.1   | 66.8 | 63.1 | 9.1%  | 61.1 | Oct | 1  | 15 |
| 950FF Case 900FF with Night Ventilation           | 37.1   | Oct    | 1   | 17 | 36.8   | Sep | 11  | 15   | 36.4   | Sep | 11         | 15 | 36.7   | Sep   | 11  | 16 | 36.4   | Aug | 5   | 16                        | 36.1          | Sep           | 11             | 16                       | 36.1   | 37.1 | 36.6 | 2.7%  | 36.1 | Sep | 11 | 16 |
| 680FF Case 600FF with Increased Insulation        | 72.5   | Jan    | 22  | 17 | 78.5   | Jan | 22  | 16   | 75.0   | Oct | 12         | 15 | 70.1   | Jan   | 22  | 16 | 72.2   | Oct | 12  | 16                        | 69.8          | Jan           | 22             | 16                       | 69.8   | 78.5 | 73.0 | 12.0% | 69.8 | Jan | 22 | 16 |
| 980FF Case 900FF with Increased Insulation        | 49.7   | Oct    | 1   | 17 | 52.2   | Sep | 12  | 15   | 52.8   | Oct | 21         | 14 | 49.6   | Sep   | 12  | 16 | 50.2   | Sep | 12  | 15                        | 48.5          | Sep           | 12             | 15                       | 48.5   | 52.8 | 50.5 | 8.5%  | 48.5 | Sep | 12 | 15 |
| 960 Sunspace                                      |        |        |     |    | 48.9   | Oct | 2   | 16   | 53.2   | Oct | 20         | 14 | 49.9   | Oct   | 12  | 15 | 49.5   | Oct | 12  | 15                        | 48.1          | Oct           | 12             | 15                       | 48.1   | 53.2 | 49.9 | 10.2% | 48.1 | Oct | 12 | 15 |

| MINIMUM ANNUAL HOURLY INTEGRATED ZONE TEMPERATURE |        |        |     |    |        |     |     |      |        |     |            |    |        |       |     |    |        |     |     |                           |               |               |                |                          |        |       |       |        |       |     |    |    |
|---|--------|--------|-----|----|--------|-----|-----|------|--------|-----|------------|----|--------|-------|-----|----|--------|-----|-----|---------------------------|---------------|---------------|----------------|--------------------------|--------|-------|-------|--------|-------|-----|----|----|
| Simulation Model:                                 |        | BSIMAC |     |    | CSE    |     |     | DeST |        |     | EnergyPlus |    |        | ESP-r |     |    | TRNSYS |     |     | Example Result Statistics |               |               |                | TRNSYS18                 |        |       |       |        |       |     |    |    |
| Case  | T (°C) | Mo.    | Day | Hr | T (°C) | Mo. | Day | Hr   | T (°C) | Mo. | Day        | Hr | T (°C) | Mo.   | Day | Hr | T (°C) | Mo. | Day | Hr                        | Min<br>T (°C) | Max<br>T (°C) | Mean<br>T (°C) | (Max-Min)/<br>Mean** (%) | T (°C) | Mo.   | Day   | Hr     |       |     |    |    |
| 600FF - Low Mass with S. Windows                  | -9.9   | Nov    | 26  | 8  | -12.9  | Feb | 9   | 7    | -13.5  | Feb | 9          | 6  | -12.6  | Feb   | 9   | 7  | -13.5  | Feb | 9   | 7                         | -13.8         | Feb           | 9              | 7                        | -13.8  | -9.9  | -12.7 | 31.1%  | -13.8 | Feb | 9  | 7  |
| 900FF - High Mass with S. Windows                 | 0.6    | Feb    | 8   | 11 | 2.2    | Feb | 9   | 7    | 1.3    | Feb | 9          | 7  | 1.2    | Feb   | 9   | 7  | 1.6    | Feb | 9   | 7                         | 0.6           | Feb           | 9              | 7                        | 0.6    | 2.2   | 1.3   | 124.2% | 0.6   | Feb | 9  | 7  |
| 650FF Case 600FF with Night Ventilation           | -16.7  | Dec    | 31  | 24 | -17.8  | Jan | 1   | 1    | -17.4  | Dec | 30         | 23 | -17.1  | Dec   | 31  | 24 | -17.5  | Jan | 1   | 1                         | -17.5         | Dec           | 31             | 24                       | -17.8  | -16.7 | -17.3 | 6.1%   | -17.5 | Dec | 31 | 24 |
| 950FF Case 900FF with Night Ventilation           | -13.2  | Dec    | 31  | 24 | -13.2  | Jan | 1   | 1    | -13.4  | Dec | 30         | 23 | -12.8  | Feb   | 9   | 7  | -12.5  | Feb | 9   | 6                         | -12.8         | Feb           | 9              | 6                        | -13.4  | -12.5 | -13.0 | 6.6%   | -12.8 | Feb | 9  | 6  |
| 680FF Case 600FF with Increased Insulation        | -5.7   | Feb    | 8   | 11 | -6.2   | Feb | 9   | 7    | -6.9   | Feb | 9          | 7  | -7.1   | Feb   | 9   | 7  | -7.2   | Feb | 9   | 7                         | -8.1          | Feb           | 9              | 7                        | -8.1   | -5.7  | -6.9  | 34.6%  | -8.1  | Feb | 9  | 7  |
| 980FF Case 900FF with Increased Insulation        | 7.3    | Feb    | 8   | 11 | 12.5   | Nov | 4   | 7    | 12.4   | Nov | 5          | 6  | 9.9    | Nov   | 4   | 7  | 10.5   | Nov | 4   | 8                         | 9.5           | Nov           | 4              | 7                        | 7.3    | 12.5  | 10.4  | 50.6%  | 9.5   | Nov | 4  | 7  |
| 960 Sunspace                                      |        |        |     |    | 8.0    | Feb | 9   | 8    | 6.7    | Feb | 9          | 6  | 5.1    | Feb   | 9   | 7  | 5.0    | Feb | 9   | 7                         | 4.2           | Feb           | 9              | 7                        | 4.2    | 8.0   | 5.8   | 65.0%  | 4.2   | Feb | 9  | 7  |

| AVERAGE ANNUAL HOURLY INTEGRATED ZONE TEMPERATURE |        |        |  |  |        |  |  |      |        |  |            |  |        |       |  |  |        |  |  |                           |               |               |                |                          |        |      |      |      |      |  |  |  |
|---|--------|--------|--|--|--------|--|--|------|--------|--|------------|--|--------|-------|--|--|--------|--|--|---------------------------|---------------|---------------|----------------|--------------------------|--------|------|------|------|------|--|--|--|
| Simulation Model:                                 |        | BSIMAC |  |  | CSE    |  |  | DeST |        |  | EnergyPlus |  |        | ESP-r |  |  | TRNSYS |  |  | Example Result Statistics |               |               |                | TRNSYS18                 |        |      |      |      |      |  |  |  |
| Case  | T (°C) |        |  |  | T (°C) |  |  |      | T (°C) |  |            |  | T (°C) |       |  |  | T (°C) |  |  |                           | Min<br>T (°C) | Max<br>T (°C) | Mean<br>T (°C) | (Max-Min)/<br>Mean** (%) | T (°C) |      |      |      |      |  |  |  |
| 600FF - Low Mass with S. Windows                  | 26.1   |        |  |  | 25.6   |  |  |      | 25.3   |  |            |  | 24.9   |       |  |  | 25.3   |  |  |                           | 24.3          |               |                |                          | 24.3   | 26.1 | 25.2 | 7.3% | 24.3 |  |  |  |
| 900FF - High Mass with S. Windows                 | 25.5   |        |  |  | 25.7   |  |  |      | 25.3   |  |            |  | 25.1   |       |  |  | 25.3   |  |  |                           | 24.5          |               |                |                          | 24.5   | 25.7 | 25.2 | 4.9% | 24.5 |  |  |  |
| 650FF Case 600FF with Night Ventilation           | 17.6   |        |  |  | 18.5   |  |  |      | 18.0   |  |            |  | 18.4   |       |  |  | 18.9   |  |  |                           | 18.4          |               |                |                          | 17.6   | 18.9 | 18.3 | 7.3% | 18.4 |  |  |  |
| 950FF Case 900FF with Night Ventilation           | 15.0   |        |  |  | 14.7   |  |  |      | 14.4   |  |            |  | 14.8   |       |  |  | 14.8   |  |  |                           | 14.7          |               |                |                          | 14.4   | 15.0 | 14.7 | 4.4% | 14.7 |  |  |  |
| 680FF Case 600FF with Increased Insulation        | 31.8   |        |  |  | 33.1   |  |  |      | 33.3   |  |            |  | 31.0   |       |  |  | 31.7   |  |  |                           | 30.2          |               |                |                          | 30.2   | 33.3 | 31.8 | 9.8% | 30.2 |  |  |  |
| 980FF Case 900FF with Increased Insulation        | 30.7   |        |  |  | 33.3   |  |  |      | 33.3   |  |            |  | 31.2   |       |  |  | 31.8   |  |  |                           | 30.5          |               |                |                          | 30.5   | 33.3 | 31.8 | 8.8% | 30.5 |  |  |  |
| 960 Sunspace                                      |        |        |  |  | 28.6   |  |  |      | 29.5   |  |            |  | 27.7   |       |  |  | 27.7   |  |  |                           | 26.8          |               |                |                          | 26.8   | 29.5 | 28.1 | 9.5% | 26.8 |  |  |  |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-6. Low Mass Basic Sensitivity Tests**

| ANNUAL HEATING [MWh]          |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
|-------------------------------|--------|--------|--------|------------|--------|--------|--------------------------------|--------|--------|--------------------------|----------|
| Case                          | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 610-600 Heat, S. Shade        | 0.113  | 0.074  | 0.097  | 0.050      | 0.165  | 0.089  | 0.050                          | 0.165  | 0.098  | 117.0%                   | 0.090    |
| 620-600 Heat, E&W Orient.     | 0.320  | 0.101  | 0.250  | 0.161      | 0.152  | 0.215  | 0.101                          | 0.320  | 0.200  | 109.6%                   | 0.215    |
| 630-620 Heat, E&W Shade       | 0.553  | 0.262  | 0.380  | 0.298      | 0.536  | 0.420  | 0.262                          | 0.553  | 0.408  | 71.2%                    | 0.422    |
| 640-600 Heat, Htg. Setback    | -1.368 | -1.590 | -1.428 | -1.663     | -1.708 | -1.851 | -1.851                         | -1.368 | -1.601 | 30.2%                    | -1.852   |
| 660-600 Heat, Low-E Win.      | -0.476 | -0.391 | -0.226 | -0.618     | -0.575 | -0.714 | -0.714                         | -0.226 | -0.500 | 97.6%                    | -0.714   |
| 670-600 Heat, 1-Pane Win.     | 1.434  | 1.307  | 1.526  | 1.292      | 1.613  | 1.636  | 1.292                          | 1.636  | 1.468  | 23.5%                    | 1.636    |
| 680-600 Heat, > Ins. 20/27    | -1.831 | -2.207 | -2.315 | -2.145     | -2.230 | -2.217 | -2.315                         | -1.831 | -2.157 | 22.4%                    | -2.216   |
| 685-600 Heat, 20/20 tstat     | 0.482  | 0.582  | 0.599  | 0.553      | 0.542  | 0.539  | 0.482                          | 0.599  | 0.549  | 21.3%                    | 0.539    |
| 695-685 Heat, > Ins. 20/20    | -1.823 | -2.159 | -2.261 | -2.075     | -2.171 | -2.150 | -2.261                         | -1.823 | -2.107 | 20.8%                    | -2.149   |
| ANNUAL SENSIBLE COOLING [MWh] |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| Case                          | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 610-600 Cool, S. Shade        | -1.523 | -1.531 | -1.259 | -1.694     | -1.929 | -1.663 | -1.929                         | -1.259 | -1.600 | 41.9%                    | -1.675   |
| 620-600 Cool, E&W Orient.     | -1.418 | -1.834 | -1.523 | -1.968     | -1.916 | -1.939 | -1.968                         | -1.418 | -1.766 | 31.1%                    | -1.940   |
| 630-620 Cool, E&W Shade       | -1.330 | -1.059 | -1.122 | -1.223     | -1.650 | -1.268 | -1.650                         | -1.059 | -1.275 | 46.4%                    | -1.271   |
| 640-600 Cool, Htg. Setback    | -0.018 | -0.269 | -0.195 | -0.264     | -0.269 | -0.302 | -0.302                         | -0.018 | -0.220 | 129.5%                   | -0.302   |
| 650-600 Cool, Night Vent      | -1.193 | -1.259 | -1.246 | -1.210     | -1.217 | -1.147 | -1.259                         | -1.147 | -1.212 | 9.2%                     | -1.147   |
| 660-600 Heat, Low-E Win.      | -2.808 | -2.573 | -2.172 | -2.796     | -2.943 | -2.813 | -2.943                         | -2.172 | -2.684 | 28.7%                    | -2.813   |
| 670-600 Heat, 1-Pane Win.     | 0.717  | 0.665  | 0.522  | 0.596      | 0.358  | 0.418  | 0.358                          | 0.717  | 0.546  | 65.7%                    | 0.418    |
| 680-600 Heat, > Ins. 20/27    | 0.116  | 0.517  | 0.500  | 0.417      | 0.368  | 0.530  | 0.116                          | 0.530  | 0.408  | 101.6%                   | 0.530    |
| 685-600 Heat, 20/20 tstat     | 3.308  | 2.946  | 2.806  | 3.092      | 2.960  | 3.072  | 2.806                          | 3.308  | 3.031  | 16.6%                    | 3.072    |
| 695-685 Heat, > Ins. 20/20    | -0.375 | 0.115  | 0.148  | 0.053      | 0.028  | 0.188  | -0.375                         | 0.188  | 0.026  | 2164.0%                  | 0.188    |
| PEAK HEATING [kW]             |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| Case                          | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 610-600 Heat, S. Shade        | -0.089 | 0.001  | 0.004  | -0.013     | 0.005  | 0.001  | -0.089                         | 0.005  | -0.015 | 616.7%                   | 0.001    |
| 620-600 Heat, E&W Orient.     | -0.110 | 0.018  | 0.033  | 0.025      | 0.025  | 0.026  | -0.110                         | 0.033  | 0.003  | 5355.3%                  | 0.048    |
| 630-620 Heat, E&W Shade       | 0.107  | 0.002  | 0.004  | -0.023     | 0.006  | 0.003  | -0.023                         | 0.107  | 0.016  | 786.0%                   | 0.005    |
| 640-600 Heat, Htg. Setback    | 1.378  | 1.202  | 1.623  | 1.354      | 0.873  | 0.680  | 0.680                          | 1.623  | 1.185  | 79.6%                    | 0.760    |
| 660-600 Heat, Low-E Win.      | -0.635 | -0.262 | -0.237 | -0.373     | -0.382 | -0.404 | -0.635                         | -0.237 | -0.382 | 104.1%                   | -0.409   |
| 670-600 Heat, 1-Pane Win.     | 0.867  | 0.635  | 0.777  | 0.649      | 0.764  | 0.862  | 0.635                          | 0.867  | 0.759  | 30.5%                    | 0.943    |
| 680-600 Heat, > Ins. 20/27    | -1.129 | -1.243 | -1.224 | -1.152     | -1.206 | -1.244 | -1.244                         | -1.129 | -1.200 | 9.6%                     | -1.163   |
| 685-600 Heat, 20/20 tstat     | -0.086 | 0.012  | 0.019  | 0.019      | 0.019  | 0.016  | -0.086                         | 0.019  | 0.000  | 29982.6%                 | 0.028    |
| 695-685 Heat, > Ins. 20/20    | -1.031 | -1.237 | -1.199 | -1.151     | -1.222 | -1.257 | -1.257                         | -1.031 | -1.183 | 19.1%                    | -1.188   |
| PEAK SENSIBLE COOLING [kW]    |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| Case                          | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 610-600 Cool, S. Shade        | -0.184 | -0.049 | -0.091 | -0.217     | -0.259 | -0.178 | -0.259                         | -0.049 | -0.163 | 129.0%                   | -0.233   |
| 620-600 Cool, E&W Orient.     | -0.946 | -1.988 | -1.467 | -1.554     | -1.571 | -1.457 | -1.988                         | -0.946 | -1.497 | 69.6%                    | -1.457   |
| 630-620 Cool, E&W Shade       | -0.583 | -0.495 | -0.429 | -0.585     | -0.651 | -0.639 | -0.651                         | -0.429 | -0.564 | 39.4%                    | -0.644   |
| 640-600 Cool, Htg. Setback    | 0.000  | -0.052 | -0.057 | -0.054     | -0.066 | -0.079 | -0.079                         | 0.000  | -0.051 | 153.3%                   | -0.079   |
| 650-600 Cool, Night Vent      | -0.002 | -0.191 | -0.377 | -0.213     | -0.232 | -0.248 | -0.377                         | -0.002 | -0.211 | 178.0%                   | -0.248   |
| 660-600 Heat, Low-E Win.      | -2.307 | -2.548 | -2.067 | -2.581     | -2.663 | -2.588 | -2.663                         | -2.067 | -2.459 | 24.2%                    | -2.588   |
| 670-600 Heat, 1-Pane Win.     | 0.567  | 0.444  | 0.417  | 0.455      | 0.289  | 0.356  | 0.289                          | 0.567  | 0.421  | 66.0%                    | 0.356    |
| 680-600 Heat, > Ins. 20/27    | 0.111  | 0.570  | 0.439  | 0.419      | 0.483  | 0.511  | 0.111                          | 0.570  | 0.422  | 108.8%                   | 0.511    |
| 685-600 Heat, 20/20 tstat     | 0.668  | 0.678  | 0.649  | 0.755      | 0.741  | 0.822  | 0.649                          | 0.822  | 0.719  | 24.0%                    | 0.822    |
| 695-685 Heat, > Ins. 20/20    | -0.086 | 0.381  | 0.284  | 0.228      | 0.305  | 0.308  | -0.086                         | 0.381  | 0.237  | 197.5%                   | 0.308    |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
 (TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
 By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

Note: The statistics in the tables below are based on the listed example results.  
 These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-7. High Mass Basic Sensitivity Tests**

| ANNUAL HEATING [MWh]          |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
|-------------------------------|--------|--------|--------|------------|--------|--------|--------------------------------|--------|--------|--------------------------|----------|
| CASES                         | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 900-600 Mass, Heat            | -2.324 | -2.614 | -2.456 | -2.661     | -2.777 | -2.690 | -2.777                         | -2.324 | -2.587 | 17.5%                    | -2.697   |
| 910-900 Heat, S. Shade        | 0.437  | 0.269  | 0.269  | 0.292      | 0.483  | 0.318  | 0.269                          | 0.483  | 0.345  | 62.0%                    | 0.325    |
| 920-900 Heat, E&W Orient.     | 1.774  | 1.577  | 1.668  | 1.673      | 1.715  | 1.793  | 1.577                          | 1.793  | 1.700  | 12.7%                    | 1.787    |
| 930-920 Heat, E&W Shade       | 0.770  | 0.568  | 0.674  | 0.657      | 0.978  | 0.777  | 0.568                          | 0.978  | 0.737  | 55.6%                    | 0.780    |
| 940-900 Heat, Htg. Setback    | -0.337 | -0.516 | -0.442 | -0.596     | -0.570 | -0.645 | -0.645                         | -0.337 | -0.518 | 59.5%                    | -0.646   |
| 960-900 Heat, Sunspace        |        | 1.143  | 1.180  | 1.025      | 1.039  | 1.046  | 1.025                          | 1.180  | 1.087  | 14.2%                    | 1.047    |
| 980-900 Heat, > Ins. 20/27    | -1.006 | -1.133 | -1.325 | -1.253     | -1.234 | -1.364 | -1.364                         | -1.006 | -1.219 | 29.3%                    | -1.352   |
| 985-900 Heat, 20/20 tstat     | 1.075  | 0.741  | 0.688  | 0.706      | 0.699  | 0.722  | 0.688                          | 1.075  | 0.772  | 50.1%                    | 0.724    |
| 995-985 Heat, > Ins. 20/20    | -1.471 | -1.365 | -1.509 | -1.363     | -1.379 | -1.459 | -1.509                         | -1.363 | -1.424 | 10.3%                    | -1.450   |
| ANNUAL SENSIBLE COOLING [MWh] |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                         | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 900-600 Mass, Cool            | -3.108 | -3.449 | -3.049 | -3.538     | -3.674 | -3.512 | -3.674                         | -3.049 | -3.389 | 18.4%                    | -3.513   |
| 910-900 Cool, S. Shade        | -1.230 | -1.049 | -0.893 | -1.105     | -1.205 | -1.076 | -1.230                         | -0.893 | -1.093 | 30.8%                    | -1.079   |
| 920-900 Cool, E&W Orient.     | 0.414  | 0.325  | 0.323  | 0.242      | 0.327  | 0.282  | 0.242                          | 0.414  | 0.319  | 53.9%                    | 0.281    |
| 930-920 Cool, E&W Shade       | -0.967 | -0.714 | -0.798 | -0.812     | -1.161 | -0.877 | -1.161                         | -0.714 | -0.888 | 50.3%                    | -0.879   |
| 940-900 Cool, Htg. Setback    | -0.101 | -0.067 | -0.040 | -0.064     | -0.060 | -0.064 | -0.101                         | -0.040 | -0.066 | 92.3%                    | -0.064   |
| 950-900 Cool, Night Vent      | -2.128 | -1.866 | -1.765 | -1.782     | -1.832 | -1.626 | -2.128                         | -1.626 | -1.833 | 27.4%                    | -1.625   |
| 960-900 Cool, Sunspace        |        | -1.538 | -1.474 | -1.582     | -1.538 | -1.478 | -1.582                         | -1.474 | -1.522 | 7.1%                     | -1.478   |
| 980-900 Heat, > Ins. 20/27    | 0.787  | 1.531  | 1.375  | 1.223      | 1.287  | 1.251  | 0.787                          | 1.531  | 1.242  | 59.9%                    | 1.251    |
| 985-900 Heat, 20/20 tstat     | 4.559  | 3.770  | 3.497  | 3.870      | 3.762  | 3.846  | 3.497                          | 4.559  | 3.884  | 27.3%                    | 3.848    |
| 995-985 Heat, > Ins. 20/20    | 0.209  | 0.969  | 0.891  | 0.844      | 0.900  | 0.950  | 0.209                          | 0.969  | 0.794  | 95.7%                    | 0.949    |
| PEAK HEATING [kW]             |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                         | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 900-600 Mass, Heat            | -0.704 | -0.577 | -0.582 | -0.517     | -0.595 | -0.580 | -0.704                         | -0.517 | -0.593 | 31.6%                    | -0.499   |
| 910-900 Heat, S. Shade        | 0.210  | 0.026  | 0.021  | 0.011      | 0.051  | 0.021  | 0.011                          | 0.210  | 0.057  | 350.6%                   | 0.021    |
| 920-900 Heat, E&W Orient.     | 0.344  | 0.069  | 0.060  | 0.083      | 0.073  | 0.086  | 0.060                          | 0.344  | 0.119  | 238.5%                   | 0.086    |
| 930-920 Heat, E&W Shade       | 0.073  | 0.025  | 0.036  | 0.015      | 0.059  | 0.036  | 0.015                          | 0.073  | 0.041  | 143.7%                   | 0.036    |
| 940-900 Heat, Htg. Setback    | 1.331  | 0.609  | 1.206  | 0.455      | 0.489  | 0.626  | 0.455                          | 1.331  | 0.786  | 111.4%                   | 0.417    |
| 960-900 Heat, Sunspace        |        | -0.311 | -0.368 | -0.428     | -0.432 | -0.478 | -0.478                         | -0.311 | -0.404 | 41.3%                    | -0.478   |
| 980-900 Heat, > Ins. 20/27    | -0.858 | -1.190 | -1.071 | -1.150     | -1.160 | -1.186 | -1.190                         | -0.858 | -1.102 | 30.1%                    | -1.186   |
| 985-900 Heat, 20/20 tstat     | 0.203  | 0.009  | 0.005  | 0.008      | 0.009  | 0.007  | 0.005                          | 0.203  | 0.040  | 493.6%                   | 0.007    |
| 995-985 Heat, > Ins. 20/20    | -1.043 | -1.083 | -0.996 | -1.073     | -1.082 | -1.123 | -1.123                         | -0.996 | -1.067 | 11.9%                    | -1.123   |
| PEAK SENSIBLE COOLING [kW]    |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                         | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 900-600 Mass, Cool            | -2.611 | -3.105 | -2.866 | -3.311     | -3.297 | -3.106 | -3.311                         | -2.611 | -3.049 | 23.0%                    | -3.106   |
| 910-900 Cool, S. Shade        | -0.546 | -0.654 | -0.453 | -0.818     | -0.684 | -0.859 | -0.859                         | -0.453 | -0.669 | 60.7%                    | -0.865   |
| 920-900 Cool, E&W Orient.     | 0.442  | -0.320 | 0.154  | 0.220      | 0.203  | 0.214  | -0.320                         | 0.442  | 0.152  | 500.5%                   | 0.214    |
| 930-920 Cool, E&W Shade       | -0.429 | -0.395 | -0.375 | -0.479     | -0.605 | -0.541 | -0.605                         | -0.375 | -0.471 | 48.9%                    | -0.542   |
| 940-900 Cool, Htg. Setback    | 0.119  | 0.000  | 0.000  | 0.000      | -0.005 | -0.002 | -0.005                         | 0.119  | 0.019  | 669.9%                   | -0.002   |
| 950-900 Cool, Night Vent      | -0.673 | -1.013 | -0.502 | -0.653     | -0.694 | -0.704 | -1.013                         | -0.502 | -0.706 | 72.3%                    | -0.704   |
| 960-900 Cool, Sunspace        |        | -1.999 | -1.189 | -1.561     | -1.493 | -1.602 | -1.999                         | -1.189 | -1.569 | 51.7%                    | -1.601   |
| 980-900 Heat, > Ins. 20/27    | 0.345  | 0.292  | 0.374  | 0.410      | 0.445  | 0.372  | 0.292                          | 0.445  | 0.373  | 41.1%                    | 0.373    |
| 985-900 Heat, 20/20 tstat     | 0.938  | 0.849  | 0.652  | 0.874      | 0.840  | 0.945  | 0.652                          | 0.945  | 0.850  | 34.4%                    | 0.945    |

**ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

|                            |       |        |       |       |       |       |        |       |       |        |       |
|----------------------------|-------|--------|-------|-------|-------|-------|--------|-------|-------|--------|-------|
| 995-985 Heat, > Ins. 20/20 | 0.152 | -0.001 | 0.107 | 0.263 | 0.218 | 0.230 | -0.001 | 0.263 | 0.161 | 163.7% | 0.230 |
|----------------------------|-------|--------|-------|-------|-------|-------|--------|-------|-------|--------|-------|

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF

(TRNSYS18) vs. Annex B8, Section B8.1 Example Results

By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

Note: The statistics in the tables below are based on the listed example results.

These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

Table B8-8. Low Mass In-Depth (Cases 195 thru 320) Sensitivity Tests

| ANNUAL HEATING [MWh]          |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
|-------------------------------|--------|--------|--------|------------|--------|--------|--------------------------------|--------|--------|--------------------------|----------|
| CASES                         | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 200-195 Surface Convection    | 0.824  | 0.823  | 1.069  | 1.036      | 0.970  | 1.049  | 0.823                          | 1.069  | 0.962  | 25.5%                    | 1.065    |
| 210-200 Ext IR (Int IR "off") | 0.586  | 1.153  | 1.305  | 0.941      | 1.397  | 1.287  | 0.586                          | 1.397  | 1.111  | 72.9%                    | 1.294    |
| 220-215 Ext IR (Int IR "on")  | 0.725  | 1.360  | 1.481  | 1.050      | 1.545  | 1.424  | 0.725                          | 1.545  | 1.264  | 64.8%                    | 1.436    |
| 215-200 Int IR (Ext IR "off") | 0.611  | 0.493  | 0.471  | 0.300      | 0.261  | 0.301  | 0.261                          | 0.611  | 0.406  | 86.3%                    | 0.307    |
| 220-210 Int IR (Ext IR "on")  | 0.750  | 0.700  | 0.647  | 0.409      | 0.409  | 0.438  | 0.409                          | 0.750  | 0.559  | 61.1%                    | 0.449    |
| 230-220 Infiltration          | 3.474  | 3.146  | 3.239  | 3.475      | 3.213  | 3.366  | 3.146                          | 3.475  | 3.319  | 9.9%                     | 3.366    |
| 240-220 Internal Gains        | -1.261 | -1.224 | -1.234 | -1.176     | -1.186 | -1.211 | -1.261                         | -1.176 | -1.215 | 7.0%                     | -1.210   |
| 250-220 Ext Solar Abs.        | -1.644 | -1.622 | -1.805 | -1.556     | -1.791 | -1.763 | -1.805                         | -1.556 | -1.697 | 14.7%                    | -1.772   |
| 270-220 South Windows         |        | -2.320 | -2.905 | -2.070     | -2.149 | -2.237 | -2.905                         | -2.070 | -2.336 | 35.8%                    | -2.271   |
| 280-270 Cavity Albedo         |        | 0.178  | 0.346  | 0.185      | 0.162  | 0.239  | 0.162                          | 0.346  | 0.222  | 83.0%                    | 0.239    |
| 320-270 Thermostat            |        | -0.669 | -0.674 | -0.614     | -0.607 | -0.600 | -0.674                         | -0.600 | -0.633 | 11.7%                    | -0.600   |
| 290-270 South Shading         |        | 0.078  | 0.108  | 0.039      | 0.168  | 0.094  | 0.039                          | 0.168  | 0.097  | 132.8%                   | 0.095    |
| 300-270 E&W Windows           |        | -0.028 | 0.187  | 0.039      | 0.092  | 0.094  | -0.028                         | 0.187  | 0.077  | 280.1%                   | 0.094    |
| 310-300 E&W Shading           |        | 0.262  | 0.386  | 0.267      | 0.572  | 0.437  | 0.262                          | 0.572  | 0.385  | 80.5%                    | 0.439    |
| ANNUAL SENSIBLE COOLING [MWh] |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                         | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 200-195 Surface Convection    | 0.127  | 0.195  | 0.207  | 0.203      | 0.189  | 0.197  | 0.127                          | 0.207  | 0.186  | 42.9%                    | 0.200    |
| 210-200 Ext IR (Int IR "off") | -0.151 | -0.297 | -0.339 | -0.254     | -0.282 | -0.329 | -0.339                         | -0.151 | -0.275 | 68.3%                    | -0.330   |
| 220-215 Ext IR (Int IR "on")  | -0.149 | -0.335 | -0.372 | -0.268     | -0.319 | -0.353 | -0.372                         | -0.149 | -0.299 | 74.5%                    | -0.354   |
| 215-200 Int IR (Ext IR "off") | 0.113  | 0.146  | 0.087  | 0.063      | 0.094  | 0.062  | 0.062                          | 0.146  | 0.094  | 88.6%                    | 0.064    |
| 220-210 Int IR (Ext IR "on")  | 0.115  | 0.108  | 0.054  | 0.050      | 0.058  | 0.038  | 0.038                          | 0.115  | 0.070  | 108.6%                   | 0.040    |
| 230-220 Infiltration          | 0.381  | 0.381  | 0.379  | 0.381      | 0.379  | 0.399  | 0.379                          | 0.399  | 0.383  | 5.3%                     | 0.399    |
| 240-220 Internal Gains        | 0.484  | 0.372  | 0.326  | 0.369      | 0.346  | 0.336  | 0.326                          | 0.484  | 0.372  | 42.5%                    | 0.336    |
| 250-220 Ext Solar Abs.        | 2.809  | 2.818  | 2.921  | 2.572      | 2.891  | 2.406  | 2.406                          | 2.921  | 2.736  | 18.8%                    | 2.429    |
| 270-220 South Windows         |        | 6.660  | 6.148  | 6.912      | 6.732  | 6.791  | 6.148                          | 6.912  | 6.649  | 11.5%                    | 6.787    |
| 280-270 Cavity Albedo         |        | -2.274 | -2.483 | -2.339     | -2.103 | -2.480 | -2.483                         | -2.103 | -2.336 | 16.3%                    | -2.480   |
| 320-270 Thermostat            |        | -2.412 | -2.278 | -2.536     | -2.396 | -2.501 | -2.536                         | -2.278 | -2.424 | 10.6%                    | -2.501   |
| 290-270 South Shading         |        | -1.661 | -1.388 | -1.779     | -1.988 | -1.827 | -1.988                         | -1.388 | -1.729 | 34.7%                    | -1.840   |
| 300-270 E&W Windows           |        | -2.216 | -1.893 | -2.370     | -2.271 | -2.376 | -2.376                         | -1.893 | -2.225 | 21.7%                    | -2.377   |
| 310-300 E&W Shading           |        | -1.303 | -1.403 | -1.483     | -1.910 | -1.589 | -1.910                         | -1.303 | -1.538 | 39.5%                    | -1.594   |
| PEAK HEATING [kW]             |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                         | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 200-195 Surface Convection    | 0.470  | 0.435  | 0.509  | 0.547      | 0.473  | 0.557  | 0.435                          | 0.557  | 0.499  | 24.4%                    | 0.570    |
| 210-200 Ext IR (Int IR "off") | 0.102  | 0.403  | 0.297  | 0.223      | 0.396  | 0.397  | 0.102                          | 0.403  | 0.303  | 99.3%                    | 0.343    |
| 220-215 Ext IR (Int IR "on")  | 0.110  | 0.419  | 0.343  | 0.214      | 0.398  | 0.389  | 0.110                          | 0.419  | 0.312  | 99.1%                    | 0.333    |
| 215-200 Int IR (Ext IR "off") | 0.249  | 0.194  | 0.212  | 0.136      | 0.115  | 0.137  | 0.115                          | 0.249  | 0.174  | 77.1%                    | 0.140    |
| 220-210 Int IR (Ext IR "on")  | 0.257  | 0.210  | 0.258  | 0.127      | 0.117  | 0.129  | 0.117                          | 0.258  | 0.183  | 77.0%                    | 0.130    |
| 230-220 Infiltration          | 1.588  | 1.294  | 1.360  | 1.624      | 1.372  | 1.437  | 1.294                          | 1.624  | 1.446  | 22.9%                    | 1.442    |
| 240-220 Internal Gains        | -0.200 | -0.188 | -0.178 | -0.185     | -0.183 | -0.185 | -0.200                         | -0.178 | -0.187 | 11.8%                    | -0.185   |
| 250-220 Ext Solar Abs.        | 0.000  | -0.002 | -0.008 | -0.005     | -0.008 | -0.004 | -0.008                         | 0.000  | -0.005 | 176.8%                   | -0.007   |
| 270-220 South Windows         |        | -0.228 | -0.303 | -0.095     | -0.040 | -0.035 | -0.303                         | -0.035 | -0.140 | 190.7%                   | -0.063   |
| 280-270 Cavity Albedo         |        | 0.001  | 0.008  | 0.005      | 0.004  | 0.005  | 0.001                          | 0.008  | 0.005  | 150.6%                   | 0.010    |
| 320-270 Thermostat            |        | -0.002 | -0.014 | -0.023     | -0.015 | -0.010 | -0.023                         | -0.002 | -0.013 | 161.1%                   | -0.023   |
| 290-270 South Shading         |        | 0.000  | 0.001  | -0.013     | 0.002  | 0.000  | -0.013                         | 0.002  | -0.002 | 763.1%                   | 0.001    |
| 300-270 E&W Windows           |        | 0.003  | 0.029  | 0.007      | 0.018  | 0.010  | 0.003                          | 0.029  | 0.013  | 197.7%                   | 0.022    |
| 310-300 E&W Shading           |        | 0.001  | 0.003  | -0.023     | 0.005  | 0.003  | -0.023                         | 0.005  | -0.002 | 1211.6%                  | 0.005    |
| PEAK SENSIBLE COOLING [kW]    |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                         | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 200-195 Surface Convection    | 0.153  | 0.221  | 0.266  | 0.266      | 0.254  | 0.265  | 0.153                          | 0.266  | 0.238  | 47.8%                    | 0.269    |
| 210-200 Ext IR (Int IR "off") | -0.078 | -0.270 | -0.302 | -0.223     | -0.321 | -0.375 | -0.375                         | -0.078 | -0.261 | 113.5%                   | -0.376   |
| 220-215 Ext IR (Int IR "on")  | -0.057 | -0.261 | -0.346 | -0.216     | -0.354 | -0.384 | -0.384                         | -0.057 | -0.270 | 121.3%                   | -0.385   |
| 215-200 Int IR (Ext IR "off") | 0.122  | 0.154  | 0.147  | 0.093      | 0.168  | 0.093  | 0.093                          | 0.154  | 0.130  | 58.0%                    | 0.095    |
| 220-210 Int IR (Ext IR "on")  | 0.143  | 0.163  | 0.103  | 0.100      | 0.135  | 0.084  | 0.084                          | 0.163  | 0.121  | 65.1%                    | 0.086    |
| 230-220 Infiltration          | 0.658  | 0.620  | 0.694  | 0.656      | 0.689  | 0.726  | 0.620                          | 0.726  | 0.674  | 15.7%                    | 0.726    |
| 240-220 Internal Gains        | 0.198  | 0.186  | 0.178  | 0.181      | 0.180  | 0.182  | 0.178                          | 0.198  | 0.184  | 10.9%                    | 0.181    |
| 250-220 Ext Solar Abs.        | 1.577  | 1.682  | 1.711  | 1.682      | 2.022  | 1.720  | 1.577                          | 2.022  | 1.732  | 25.7%                    | 1.738    |
| 270-220 South Windows         |        | 5.903  | 4.792  | 5.654      | 5.601  | 5.669  | 4.792                          | 5.903  | 5.524  | 20.1%                    | 5.664    |
| 280-270 Cavity Albedo         |        | -2.246 | -2.064 | -2.112     | -1.937 | -2.238 | -2.246                         | -1.937 | -2.119 | 14.6%                    | -2.237   |
| 320-270 Thermostat            |        | -0.538 | -0.528 | -0.630     | -0.620 | -0.688 | -0.688                         | -0.528 | -0.601 | 26.6%                    | -0.688   |
| 290-270 South Shading         |        | -0.139 | -0.093 | -0.244     | -0.202 | -0.236 | -0.244                         | -0.093 | -0.183 | 82.8%                    | -0.261   |
| 300-270 E&W Windows           |        | -2.848 | -2.137 | -2.363     | -2.392 | -2.359 | -2.848                         | -2.137 | -2.420 | 29.4%                    | -2.359   |



**ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results**

**By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

|                     |  |        |        |        |        |        |        |        |        |       |        |
|---------------------|--|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|
| 310-300 E&W Shading |  | -0.367 | -0.443 | -0.506 | -0.603 | -0.577 | -0.603 | -0.367 | -0.499 | 47.2% | -0.579 |
|---------------------|--|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF

(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-9. Low Mass In-Depth (Cases 395 thru 440) Sensitivity Tests**

| ANNUAL HEATING [MWh]              |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
|-----------------------------------|--------|--------|--------|------------|--------|--------|--------------------------------|--------|--------|--------------------------|----------|
| CASES                             | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 400-395 Surf. Conv. & IR          | 1.341  | 1.681  | 1.902  | 1.707      | 1.744  | 1.861  | 1.341                          | 1.902  | 1.706  | 32.9%                    | 1.896    |
| 410-400 Infiltration              | 1.724  | 1.509  | 1.614  | 1.733      | 1.602  | 1.676  | 1.509                          | 1.733  | 1.643  | 13.6%                    | 1.676    |
| 420-410 Internal Gains            | -1.231 | -1.211 | -1.228 | -1.175     | -1.185 | -1.209 | -1.231                         | -1.175 | -1.206 | 4.7%                     | -1.208   |
| 430-420 Ext Solar Abs.            | -1.228 | -1.380 | -1.479 | -1.286     | -1.482 | -1.386 | -1.482                         | -1.228 | -1.374 | 18.5%                    | -1.395   |
| 600-430 South Windows             | -1.121 | -1.461 | -1.907 | -1.296     | -1.183 | -1.347 | -1.907                         | -1.121 | -1.386 | 56.7%                    | -1.372   |
| 440-600 Cavity Albedo             |        | 0.163  | 0.283  | 0.176      | 0.142  | 0.217  | 0.142                          | 0.283  | 0.196  | 71.9%                    | 0.217    |
| 450-600 Const Int&Ext Surf Coefs  | -0.307 | -0.002 | -0.672 | -0.362     | -0.512 | -0.633 | -0.672                         | -0.002 | -0.415 | 161.5%                   | -0.631   |
| 460-600 Const Int Surf Coefs      | -0.222 | 0.063  | -0.174 | -0.131     | -0.099 | -0.214 | -0.222                         | 0.063  | -0.130 | 219.8%                   | -0.213   |
| 460-450 Auto Ext Surf Heat Transf | 0.085  | 0.065  | 0.498  | 0.231      | 0.412  | 0.419  | 0.065                          | 0.498  | 0.285  | 151.9%                   | 0.418    |
| 470-600 Const Ext Surf Coefs      | -0.008 | -0.093 | -0.507 | -0.231     | -0.402 | -0.429 | -0.507                         | -0.008 | -0.278 | 179.3%                   | -0.428   |
| 470-450 Auto Int Surf Heat Transf | 0.299  | -0.091 | 0.165  | 0.131      | 0.109  | 0.204  | -0.091                         | 0.299  | 0.136  | 286.2%                   | 0.203    |
| ANNUAL SENSIBLE COOLING [MWh]     |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                             | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 400-395 Surf. Conv. & IR          | 0.042  | 0.016  | 0.011  | 0.020      | 0.019  | 0.009  | 0.009                          | 0.042  | 0.019  | 168.7%                   | 0.009    |
| 410-400 Infiltration              | 0.033  | 0.025  | 0.024  | 0.027      | 0.028  | 0.022  | 0.022                          | 0.033  | 0.027  | 39.8%                    | 0.023    |
| 420-410 Internal Gains            | 0.132  | 0.092  | 0.078  | 0.095      | 0.090  | 0.074  | 0.074                          | 0.132  | 0.094  | 61.7%                    | 0.074    |
| 430-420 Ext Solar Abs.            | 0.856  | 0.766  | 0.825  | 0.703      | 0.811  | 0.630  | 0.630                          | 0.856  | 0.765  | 29.6%                    | 0.635    |
| 600-430 South Windows             | 4.738  | 5.007  | 4.488  | 5.171      | 5.209  | 5.040  | 4.488                          | 5.209  | 4.942  | 14.6%                    | 5.035    |
| 440-600 Cavity Albedo             |        | -1.928 | -1.974 | -1.942     | -1.748 | -2.038 | -2.038                         | -1.748 | -1.926 | 15.1%                    | -2.038   |
| 450-600 Const Int&Ext Surf Coefs  | 0.350  | -0.224 | 0.729  | 0.480      | 0.451  | 0.751  | -0.224                         | 0.751  | 0.423  | 230.6%                   | 0.750    |
| 460-600 Const Int Surf Coefs      | 0.438  | 0.027  | 0.497  | 0.448      | 0.567  | 0.464  | 0.027                          | 0.567  | 0.407  | 132.9%                   | 0.463    |
| 460-450 Auto Ext Surf Heat Transf | 0.088  | 0.251  | -0.232 | -0.033     | 0.116  | -0.287 | -0.287                         | 0.251  | -0.016 | 3319.8%                  | -0.287   |
| 470-600 Const Ext Surf Coefs      | 0.165  | -0.269 | 0.217  | 0.002      | -0.156 | 0.276  | -0.269                         | 0.276  | 0.039  | 1392.5%                  | 0.276    |
| 470-450 Auto Int Surf Heat Transf | -0.185 | -0.045 | -0.512 | -0.478     | -0.608 | -0.475 | -0.608                         | -0.045 | -0.384 | 146.6%                   | -0.474   |
| PEAK HEATING [kW]                 |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                             | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 400-395 Surf. Conv. & IR          | 0.611  | 0.682  | 0.778  | 0.740      | 0.698  | 0.717  | 0.611                          | 0.778  | 0.704  | 23.7%                    | 0.794    |
| 410-400 Infiltration              | 0.779  | 0.601  | 0.680  | 0.812      | 0.685  | 0.718  | 0.601                          | 0.812  | 0.713  | 29.6%                    | 0.721    |
| 420-410 Internal Gains            | -0.200 | -0.184 | -0.178 | -0.185     | -0.183 | -0.185 | -0.200                         | -0.178 | -0.186 | 11.8%                    | -0.185   |
| 430-420 Ext Solar Abs.            | 0.162  | -0.002 | -0.005 | -0.003     | -0.005 | -0.003 | -0.005                         | 0.162  | 0.024  | 695.2%                   | -0.005   |
| 600-430 South Windows             | -0.045 | -0.234 | -0.325 | -0.112     | -0.057 | -0.050 | -0.325                         | -0.045 | -0.137 | 204.3%                   | -0.088   |
| 440-600 Cavity Albedo             |        | 0.007  | 0.025  | 0.014      | 0.009  | 0.015  | 0.007                          | 0.025  | 0.014  | 127.7%                   | 0.027    |
| 450-600 Const Int&Ext Surf Coefs  | -0.266 | -0.042 | -0.282 | -0.105     | -0.186 | -0.322 | -0.322                         | -0.042 | -0.200 | 139.6%                   | -0.300   |
| 460-600 Const Int Surf Coefs      | -0.200 | -0.049 | -0.055 | -0.113     | -0.127 | -0.199 | -0.200                         | -0.049 | -0.124 | 122.0%                   | -0.186   |
| 460-450 Auto Ext Surf Heat Transf | 0.066  | -0.007 | 0.227  | -0.009     | 0.059  | 0.122  | -0.009                         | 0.227  | 0.076  | 308.4%                   | 0.113    |
| 470-600 Const Ext Surf Coefs      | -0.137 | -0.020 | -0.228 | 0.002      | -0.059 | -0.127 | -0.228                         | 0.002  | -0.095 | 243.0%                   | -0.115   |
| 470-450 Auto Int Surf Heat Transf | 0.129  | 0.022  | 0.054  | 0.107      | 0.127  | 0.194  | 0.022                          | 0.194  | 0.106  | 162.7%                   | 0.185    |
| PEAK SENSIBLE COOLING [kW]        |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                             | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 400-395 Surf. Conv. & IR          | 0.251  | 0.136  | 0.149  | 0.229      | 0.162  | 0.107  | 0.107                          | 0.251  | 0.172  | 83.7%                    | 0.109    |
| 410-400 Infiltration              | 0.213  | 0.206  | 0.252  | 0.221      | 0.168  | 0.232  | 0.168                          | 0.252  | 0.215  | 39.0%                    | 0.233    |
| 420-410 Internal Gains            | 0.197  | 0.209  | 0.208  | 0.205      | 0.212  | 0.210  | 0.197                          | 0.212  | 0.207  | 7.3%                     | 0.210    |
| 430-420 Ext Solar Abs.            | 0.959  | 0.931  | 0.923  | 0.897      | 1.038  | 0.890  | 0.890                          | 1.038  | 0.940  | 15.7%                    | 0.896    |
| 600-430 South Windows             | 3.483  | 4.641  | 3.582  | 4.422      | 4.319  | 4.342  | 3.483                          | 4.641  | 4.132  | 28.0%                    | 4.333    |
| 440-600 Cavity Albedo             |        | -1.815 | -1.656 | -1.666     | -1.514 | -1.738 | -1.815                         | -1.514 | -1.678 | 18.0%                    | -1.738   |
| 450-600 Const Int&Ext Surf Coefs  | 0.162  | -0.301 | 0.641  | 0.115      | 0.308  | 0.268  | -0.301                         | 0.641  | 0.199  | 474.2%                   | 0.267    |
| 460-600 Const Int Surf Coefs      | 0.154  | -0.238 | 0.480  | 0.023      | 0.111  | 0.023  | -0.238                         | 0.480  | 0.092  | 779.6%                   | 0.022    |
| 460-450 Auto Ext Surf Heat Transf | -0.008 | 0.063  | -0.161 | -0.092     | -0.197 | -0.244 | -0.244                         | 0.063  | -0.107 | 288.5%                   | -0.244   |
| 470-600 Const Ext Surf Coefs      | 0.045  | -0.093 | 0.148  | 0.092      | 0.214  | 0.274  | -0.093                         | 0.274  | 0.113  | 324.3%                   | 0.274    |
| 470-450 Auto Int Surf Heat Transf | -0.117 | 0.208  | -0.493 | -0.023     | -0.094 | 0.007  | -0.493                         | 0.208  | -0.085 | 821.0%                   | 0.008    |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

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(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

Table B8-10. High Mass Basic and In-Depth Sensitivity Tests

| ANNUAL HEATING [MWh]              |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
|-----------------------------------|--------|--------|--------|------------|--------|--------|--------------------------------|--------|--------|--------------------------|----------|
| CASES                             | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 800-430 Mass, w/ High Cond. Wall  | -0.030 | -0.548 | -0.551 | -0.505     | -0.565 | -0.481 | -0.565                         | -0.030 | -0.447 | 119.8%                   | -0.502   |
| 900-800 Himass, S. Win.           | -3.415 | -3.527 | -3.812 | -3.452     | -3.395 | -3.555 | -3.812                         | -3.395 | -3.526 | 11.8%                    | -3.567   |
| 900-810 Himass, Int. Sol. Abs.    |        | -0.659 | -0.863 | -0.678     | -0.600 | -0.796 | -0.863                         | -0.600 | -0.719 | 36.5%                    | -0.793   |
| 910-610 Mass, w/ S. Shade         | -2.000 | -2.419 | -2.284 | -2.419     | -2.460 | -2.460 | -2.460                         | -2.000 | -2.340 | 19.7%                    | -2.462   |
| 920-620 Mass, w/ E&W Win.         | -0.870 | -1.138 | -1.038 | -1.149     | -1.215 | -1.112 | -1.215                         | -0.870 | -1.087 | 31.7%                    | -1.126   |
| 930-630 Mass w/ E&W Shade         | -0.653 | -0.832 | -0.744 | -0.790     | -0.773 | -0.754 | -0.832                         | -0.653 | -0.758 | 23.7%                    | -0.768   |
| 940-640 Mass, w/ Htg. Setback     | -1.293 | -1.540 | -1.470 | -1.594     | -1.640 | -1.484 | -1.640                         | -1.293 | -1.503 | 23.1%                    | -1.492   |
| 980-680 Mass, w/ Insulation 20/27 | -1.499 | -1.540 | -1.466 | -1.769     | -1.781 | -1.836 | -1.836                         | -1.466 | -1.648 | 22.4%                    | -1.833   |
| 985-685 Mass, w/ 20/20 Tstat      | -1.731 | -2.454 | -2.367 | -2.508     | -2.620 | -2.506 | -2.620                         | -1.731 | -2.364 | 37.6%                    | -2.512   |
| 995-695 Mass, w/ Insulation 20/20 | -1.379 | -1.660 | -1.615 | -1.795     | -1.827 | -1.815 | -1.827                         | -1.379 | -1.682 | 26.7%                    | -1.813   |
| ANNUAL SENSIBLE COOLING [MWh]     |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                             | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 800-430 Mass, w/ High Cond. Wall  | -0.611 | -0.526 | -0.582 | -0.482     | -0.561 | -0.457 | -0.611                         | -0.457 | -0.537 | 28.7%                    | -0.461   |
| 900-800 Himass, S. Win.           | 2.241  | 2.084  | 2.021  | 2.115      | 2.096  | 1.985  | 1.985                          | 2.241  | 2.090  | 12.2%                    | 1.983    |
| 900-810 Himass, Int. Sol. Abs.    |        | 0.983  | 1.026  | 0.981      | 0.882  | 0.973  | 0.882                          | 1.026  | 0.969  | 14.9%                    | 0.972    |
| 910-610 Mass, w/ S. Shade         | -2.815 | -2.967 | -2.683 | -2.949     | -2.950 | -2.926 | -2.967                         | -2.683 | -2.882 | 9.9%                     | -2.917   |
| 920-620 Mass, w/ E&W Win.         | -1.276 | -1.290 | -1.203 | -1.329     | -1.431 | -1.292 | -1.431                         | -1.203 | -1.303 | 17.5%                    | -1.292   |
| 930-630 Mass w/ E&W Shade         | -0.913 | -0.945 | -0.879 | -0.917     | -0.942 | -0.901 | -0.945                         | -0.879 | -0.916 | 7.2%                     | -0.900   |
| 940-640 Mass, w/ Htg. Setback     | -3.191 | -3.247 | -2.894 | -3.339     | -3.465 | -3.274 | -3.465                         | -2.894 | -3.235 | 17.7%                    | -3.274   |
| 950-650 Mass, w/ Night Vent       | -4.043 | -4.056 | -3.568 | -4.110     | -4.289 | -3.991 | -4.289                         | -3.568 | -4.009 | 18.0%                    | -3.991   |
| 980-680 Mass, w/ Insulation 20/27 | -2.437 | -2.435 | -2.174 | -2.732     | -2.755 | -2.791 | -2.791                         | -2.174 | -2.554 | 24.2%                    | -2.792   |
| 985-685 Mass, w/ 20/20 Tstat      | -1.857 | -2.626 | -2.358 | -2.760     | -2.872 | -2.738 | -2.872                         | -1.857 | -2.535 | 40.0%                    | -2.736   |
| 995-695 Mass, w/ Insulation 20/20 | -1.273 | -1.772 | -1.615 | -1.969     | -2.000 | -1.975 | -2.000                         | -1.273 | -1.767 | 41.1%                    | -1.975   |
| PEAK HEATING [kW]                 |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                             | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 800-430 Mass, w/ High Cond. Wall  | -0.343 | -0.476 | -0.496 | -0.393     | -0.445 | -0.442 | -0.496                         | -0.343 | -0.432 | 35.4%                    | -0.386   |
| 900-800 Himass, S. Win.           | -0.406 | -0.334 | -0.411 | -0.236     | -0.207 | -0.188 | -0.411                         | -0.188 | -0.297 | 74.9%                    | -0.202   |
| 900-810 Himass, Int. Sol. Abs.    |        | -0.057 | -0.059 | -0.062     | -0.062 | -0.066 | -0.066                         | -0.057 | -0.061 | 15.4%                    | -0.066   |
| 910-610 Mass, w/ S. Shade         | -0.405 | -0.552 | -0.565 | -0.493     | -0.549 | -0.560 | -0.565                         | -0.405 | -0.521 | 30.7%                    | -0.480   |
| 920-620 Mass, w/ E&W Win.         | -0.250 | -0.525 | -0.555 | -0.459     | -0.547 | -0.520 | -0.555                         | -0.250 | -0.476 | 64.1%                    | -0.462   |
| 930-630 Mass w/ E&W Shade         | -0.284 | -0.502 | -0.523 | -0.422     | -0.494 | -0.487 | -0.523                         | -0.284 | -0.452 | 52.9%                    | -0.431   |
| 940-640 Mass, w/ Htg. Setback     | -0.751 | -1.171 | -0.999 | -1.416     | -0.979 | -0.634 | -1.416                         | -0.634 | -0.992 | 78.9%                    | -0.843   |
| 980-680 Mass, w/ Insulation 20/27 | -0.433 | -0.524 | -0.429 | -0.515     | -0.549 | -0.523 | -0.549                         | -0.429 | -0.495 | 24.2%                    | -0.522   |
| 985-685 Mass, w/ 20/20 Tstat      | -0.415 | -0.580 | -0.596 | -0.528     | -0.605 | -0.589 | -0.605                         | -0.415 | -0.552 | 34.4%                    | -0.520   |
| 995-695 Mass, w/ Insulation 20/20 | -0.427 | -0.426 | -0.393 | -0.450     | -0.465 | -0.456 | -0.465                         | -0.393 | -0.436 | 16.5%                    | -0.456   |
| PEAK SENSIBLE COOLING [kW]        |        |        |        |            |        |        | Statistics for Example Results |        |        |                          | TRNSYS18 |
| CASES                             | BSIMAC | CSE    | DeST   | EnergyPlus | ESP-r  | TRNSYS | Min                            | Max    | Mean   | (Max-Min)/<br>Mean** (%) |          |
| 800-430 Mass, w/ High Cond. Wall  | -0.881 | -0.738 | -0.683 | -0.884     | -0.822 | -0.768 | -0.884                         | -0.683 | -0.796 | 25.2%                    | -0.770   |
| 900-800 Himass, S. Win.           | 1.753  | 2.275  | 1.399  | 1.995      | 1.844  | 2.004  | 1.399                          | 2.275  | 1.878  | 46.6%                    | 1.998    |
| 900-810 Himass, Int. Sol. Abs.    |        | 0.966  | 0.616  | 0.770      | 0.717  | 0.827  | 0.616                          | 0.966  | 0.779  | 44.9%                    | 0.827    |
| 910-610 Mass, w/ S. Shade         | -2.973 | -3.710 | -3.228 | -3.912     | -3.722 | -3.787 | -3.912                         | -2.973 | -3.555 | 26.4%                    | -3.738   |
| 920-620 Mass, w/ E&W Win.         | -1.223 | -1.436 | -1.245 | -1.537     | -1.523 | -1.434 | -1.537                         | -1.223 | -1.400 | 22.4%                    | -1.434   |
| 930-630 Mass w/ E&W Shade         | -1.069 | -1.336 | -1.191 | -1.431     | -1.477 | -1.336 | -1.477                         | -1.069 | -1.307 | 31.2%                    | -1.332   |
| 940-640 Mass, w/ Htg. Setback     | -2.492 | -3.053 | -2.809 | -3.257     | -3.236 | -3.029 | -3.257                         | -2.492 | -2.979 | 25.7%                    | -3.029   |
| 950-650 Mass, w/ Night Vent       | -3.282 | -3.926 | -2.991 | -3.751     | -3.759 | -3.561 | -3.926                         | -2.991 | -3.545 | 26.4%                    | -3.561   |
| 980-680 Mass, w/ Insulation 20/27 | -2.377 | -3.383 | -2.931 | -3.320     | -3.335 | -3.244 | -3.383                         | -2.377 | -3.098 | 32.5%                    | -3.244   |
| 985-685 Mass, w/ 20/20 Tstat      | -2.341 | -2.934 | -2.863 | -3.192     | -3.198 | -2.983 | -3.198                         | -2.341 | -2.918 | 29.4%                    | -2.982   |
| 995-695 Mass, w/ Insulation 20/20 | -2.103 | -3.317 | -3.040 | -3.157     | -3.285 | -3.060 | -3.317                         | -2.103 | -2.994 | 40.6%                    | -3.061   |

\*\* ABS[(Max-Min) / (Mean of Example Simulation Results)]

**ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-11. Annual Transmissivity Coefficient of Windows**  
(ANNUAL UNSHADED TRANSMITTED SOLAR RADIATION)/(ANNUAL UNSHADED INCIDENT SOLAR RADIATION)

| Simulation Model:<br>Case | BSIMAC | CSE   | DeST  | EnergyPlus | ESP-r | TRNSYS | Statistics for Example Results |       |       |                         | TRNSYS18 |
|---------------------------|--------|-------|-------|------------|-------|--------|--------------------------------|-------|-------|-------------------------|----------|
|                           |        |       |       |            |       |        | Min                            | Max   | Mean  | (Max-Min)/<br>Mean* (%) |          |
| 600 South                 | 0.591  | 0.627 | 0.624 | 0.587      | 0.597 | 0.594  | 0.587                          | 0.627 | 0.603 | 6.7%                    | 0.594    |
| 620 West                  | 0.600  |       | 0.629 | 0.601      | 0.616 | 0.640  | 0.600                          | 0.640 | 0.617 | 6.5%                    | 0.640    |
| 660 South, Low-E          | 0.322  | 0.381 | 0.392 | 0.318      | 0.325 | 0.324  | 0.318                          | 0.392 | 0.344 | 21.6%                   | 0.324    |
| 670 South, Single-Pane    | 0.748  | 0.750 | 0.770 | 0.747      | 0.754 | 0.751  | 0.747                          | 0.770 | 0.753 | 3.1%                    | 0.751    |

\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**Table B8-12. Annual Shading Coefficient of Window Shading Devices: Overhangs & Fins**  
(1-(ANNUAL SHADED TRANSMITTED SOLAR RADIATION))/(ANNUAL UNSHADED TRANSMITTED SOLAR RADIATION)

| Simulation Model:<br>Case | BSIMAC | CSE   | DeST  | EnergyPlus | ESP-r | TRNSYS | Statistics for Example Results |       |       |                         | TRNSYS18 |
|---------------------------|--------|-------|-------|------------|-------|--------|--------------------------------|-------|-------|-------------------------|----------|
|                           |        |       |       |            |       |        | Min                            | Max   | Mean  | (Max-Min)/<br>Mean* (%) |          |
| 610/600 South             | 0.218  | 0.194 | 0.176 | 0.196      | 0.224 | 0.195  | 0.176                          | 0.224 | 0.201 | 24.0%                   | 0.197    |
| 630/620 West              | 0.268  |       | 0.299 | 0.278      | 0.342 | 0.286  | 0.268                          | 0.342 | 0.294 | 25.2%                   | 0.287    |

\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**Table B8-13. Case 600 Annual Incident Solar Radiation (kWh/m<sup>2</sup>)**

| Simulation Model:<br>Case | BSIMAC | CSE  | DeST | EnergyPlus | ESP-r | TRNSYS | Statistics for Example Results |      |      |                         | TRNSYS18 |
|---------------------------|--------|------|------|------------|-------|--------|--------------------------------|------|------|-------------------------|----------|
|                           |        |      |      |            |       |        | Min                            | Max  | Mean | (Max-Min)/<br>Mean* (%) |          |
| Horizontal                | 1670   | 1663 | 1667 | 1664       | 1665  | 1669   | 1663                           | 1670 | 1666 | 0.4%                    | 1669     |
| North                     | 453    | 399  | 477  | 438        | 432   | 440    | 399                            | 477  | 440  | 17.8%                   | 440      |
| East                      | 1061   | 1027 | 1017 | 1062       | 1054  | 1068   | 1017                           | 1068 | 1048 | 4.9%                    | 1068     |
| South                     | 1387   | 1317 | 1291 | 1370       | 1363  | 1384   | 1291                           | 1387 | 1352 | 7.1%                    | 1384     |
| West                      | 997    | 903  | 906  | 967        | 961   | 974    | 903                            | 997  | 951  | 9.9%                    | 974      |

\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**Table B8-14. Annual Transmitted Solar Radiation - Unshaded (kWh/m<sup>2</sup>)**

| Simulation Model:<br>Case | BSIMAC | CSE | DeST | EnergyPlus | ESP-r | TRNSYS | Statistics for Example Results |      |      |                         | TRNSYS18 |
|---------------------------|--------|-----|------|------------|-------|--------|--------------------------------|------|------|-------------------------|----------|
|                           |        |     |      |            |       |        | Min                            | Max  | Mean | (Max-Min)/<br>Mean* (%) |          |
| 600 South                 | 820    | 826 | 805  | 804        | 814   | 823    | 804                            | 826  | 815  | 2.6%                    | 823      |
| 620 West                  | 598    |     | 569  | 581        | 592   | 624    | 569                            | 624  | 593  | 9.2%                    | 624      |
| 660 South                 | 447    | 501 | 506  | 436        | 443   | 448    | 436                            | 506  | 464  | 15.2%                   | 448      |
| 670 South                 | 1037   | 988 | 994  | 1024       | 1028  | 1039   | 988                            | 1039 | 1018 | 5.0%                    | 1039     |

\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**Table B8-15. Annual Transmitted Solar Radiation - Shaded (kWh/m<sup>2</sup>)**

| Simulation Model:<br>Case | BSIMAC | CSE | DeST | EnergyPlus | ESP-r | TRNSYS | Statistics for Example Results |     |      |                         | TRNSYS18 |
|---------------------------|--------|-----|------|------------|-------|--------|--------------------------------|-----|------|-------------------------|----------|
|                           |        |     |      |            |       |        | Min                            | Max | Mean | (Max-Min)/<br>Mean* (%) |          |
| 610 South                 | 641    | 665 | 663  | 646        | 631   | 662    | 631                            | 665 | 651  | 5.2%                    | 661      |
| 630 West                  | 438    |     | 399  | 419        | 390   | 446    | 390                            | 446 | 418  | 13.4%                   | 445      |

\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF  
(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-16. Sky Temperature Output, Case 600**

| MAXIMUM ANNUAL HOURLY INTEGRATED SKY TEMPERATURE |        |     |     |       |     |    |        |       |     |            |        |       |       |    |        |        |     |    |                                    |       |     |    |                           |               |                |                          |          |       |     |    |    |
|--|--------|-----|-----|-------|-----|----|--------|-------|-----|------------|--------|-------|-------|----|--------|--------|-----|----|------------------------------------|-------|-----|----|---------------------------|---------------|----------------|--------------------------|----------|-------|-----|----|----|
| Simulation Model:                                | BSIMAC |     |     | CSE   |     |    | DeST   |       |     | EnergyPlus |        |       | ESP-r |    |        | TRNSYS |     |    | TestSpec-Alt<br>Alternative Values |       |     |    | Example Result Statistics |               |                |                          | TRNSYS18 |       |     |    |    |
|  | T (°C) | Mo. | Day | Mo.   | Day | Hr | T (°C) | Mo.   | Day | Hr         | T (°C) | Mo.   | Day   | Hr | T (°C) | Mo.    | Day | Hr | T (°C)                             | Mo.   | Day | Hr | Min<br>T (°C)             | Max<br>T (°C) | Mean<br>T (°C) | (Max-Min)/<br>Mean** (%) | T (°C)   | Mo.   | Day | Hr |    |
| Average Annual Hourly Integrated                 |        |     |     | -3.9  |     |    | -5.9   |       |     | -2.0       |        |       | -5.2  |    |        | -5.1   |     |    | -5.9                               |       |     |    | -5.9                      | -2.0          | -4.7           | 83.2%                    | -5.1     |       |     |    |    |
| Minimum Annual Hourly Integrated                 |        |     |     | -46.2 | Dec | 31 | 24     | -46.9 | Dec | 31         | 23     | -38.0 | Dec   | 31 | 24     | -46.9  | Dec | 31 | 23                                 | -46.2 | Dec | 31 | 24                        | -46.9         | -38.0          | -45.2                    | 19.8%    | -46.2 | Dec | 31 | 24 |
| Maximum Annual Hourly Integrated                 |        |     |     | 30.1  | Jun | 13 | 15     | 24.6  | Aug | 4          | 15     | 24.7  | Aug   | 4  | 16     | 26.7   | Aug | 4  | 15                                 | 26.0  | Jun | 13 | 18                        | 24.6          | 30.1           | 26.1                     | 20.9%    | 26.0  | Jun | 13 | 18 |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**SHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980F (TRNSYS18) vs. Annex B8, Section B8.1 Example Results**  
**By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
 These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-M1. Monthly Heating Loads (kWh)**

| Simulation Model: | BSIMAC | CSE   | DeST  | EnergyPlus | ESP-r | TRNSYS | Statistics for Example Results |       |       |                          | TRNSYS18 |
|-------------------|--------|-------|-------|------------|-------|--------|--------------------------------|-------|-------|--------------------------|----------|
|                   |        |       |       |            |       |        | Min                            | Max   | Mean  | (Max-Min)/<br>Mean** (%) |          |
| <b>Case 600</b>   |        |       |       |            |       |        |                                |       |       |                          |          |
| Jan               | 664.0  | 655.6 | 672.7 | 711.9      | 732.0 | 734.9  | 655.6                          | 734.9 | 695.2 | 11.4%                    | 731.2    |
| Feb               | 653.3  | 626.3 | 635.3 | 682.6      | 682.0 | 702.1  | 626.3                          | 702.1 | 663.6 | 11.4%                    | 702.1    |
| Mar               | 433.5  | 435.7 | 450.5 | 472.2      | 481.0 | 495.0  | 433.5                          | 495.0 | 461.3 | 13.3%                    | 495.0    |
| Apr               | 511.0  | 457.0 | 448.0 | 510.1      | 479.0 | 517.3  | 448.0                          | 517.3 | 487.1 | 14.2%                    | 517.3    |
| May               | 112.8  | 127.8 | 128.0 | 136.8      | 139.0 | 150.7  | 112.8                          | 150.7 | 132.5 | 28.6%                    | 150.7    |
| Jun               | 2.7    | 11.7  | 11.2  | 10.1       | 14.0  | 16.0   | 2.7                            | 16.0  | 10.9  | 120.7%                   | 16.0     |
| Jul               | 4.8    | 11.5  | 10.1  | 12.0       | 14.0  | 16.7   | 4.8                            | 16.7  | 11.5  | 103.0%                   | 16.7     |
| Aug               | 1.4    | 6.9   | 8.4   | 6.6        | 9.0   | 9.6    | 1.4                            | 9.6   | 7.0   | 118.1%                   | 9.6      |
| Sep               | 51.8   | 74.3  | 76.7  | 73.3       | 81.0  | 84.8   | 51.8                           | 84.8  | 73.7  | 44.9%                    | 84.8     |
| Oct               | 317.0  | 328.4 | 324.1 | 347.7      | 354.0 | 367.1  | 317.0                          | 367.1 | 339.7 | 14.7%                    | 367.1    |
| Nov               | 598.7  | 575.6 | 585.8 | 625.3      | 629.0 | 645.8  | 575.6                          | 645.8 | 610.0 | 11.5%                    | 645.8    |
| Dec               | 698.7  | 682.0 | 697.8 | 735.7      | 750.0 | 763.5  | 682.0                          | 763.5 | 721.3 | 11.3%                    | 763.6    |
| <b>Case 900</b>   |        |       |       |            |       |        |                                |       |       |                          |          |
| Jan               | 277.8  | 206.1 | 275.3 | 255.8      | 266.0 | 291.9  | 206.1                          | 291.9 | 262.2 | 32.7%                    | 280.2    |
| Feb               | 307.4  | 243.2 | 292.9 | 294.2      | 283.0 | 322.1  | 243.2                          | 322.1 | 290.5 | 27.2%                    | 322.2    |
| Mar               | 134.4  | 102.4 | 120.0 | 125.5      | 115.0 | 143.8  | 102.4                          | 143.8 | 123.5 | 33.5%                    | 143.9    |
| Apr               | 275.7  | 222.4 | 214.2 | 268.7      | 228.0 | 275.5  | 214.2                          | 275.7 | 247.4 | 24.9%                    | 275.5    |
| May               | 20.1   | 33.3  | 26.8  | 33.4       | 29.0  | 37.5   | 20.1                           | 37.5  | 30.0  | 58.0%                    | 37.5     |
| Jun               | 0.0    | 0.0   | 0.0   | 0.0        | 0.0   | 0.0    | 0.0                            | 0.0   | 0.0   | #DIV/0!                  | 0.0      |
| Jul               | 0.0    | 0.0   | 0.0   | 0.0        | 0.0   | 0.0    | 0.0                            | 0.0   | 0.0   | #DIV/0!                  | 0.0      |
| Aug               | 0.0    | 0.0   | 0.0   | 0.0        | 0.0   | 0.0    | 0.0                            | 0.0   | 0.0   | #DIV/0!                  | 0.0      |
| Sep               | 2.1    | 0.0   | 0.0   | 0.1        | 0.0   | 0.5    | 0.0                            | 2.1   | 0.5   | 458.3%                   | 0.5      |
| Oct               | 80.5   | 65.1  | 63.6  | 81.1       | 70.0  | 85.0   | 63.6                           | 85.0  | 74.2  | 28.9%                    | 85.0     |
| Nov               | 298.2  | 251.6 | 283.9 | 297.0      | 286.0 | 318.2  | 251.6                          | 318.2 | 289.2 | 23.0%                    | 318.3    |
| Dec               | 329.8  | 254.7 | 314.3 | 307.9      | 308.0 | 339.4  | 254.7                          | 339.4 | 309.0 | 27.4%                    | 339.4    |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**Table B8-M2. Monthly Sensible Cooling Loads (kWh)**

| Simulation Model: | BSIMAC | CSE   | DeST  | EnergyPlus | ESP-r | TRNSYS | Statistics for Example Results |       |       |                          | TRNSYS18 |
|-------------------|--------|-------|-------|------------|-------|--------|--------------------------------|-------|-------|--------------------------|----------|
|                   |        |       |       |            |       |        | Min                            | Max   | Mean  | (Max-Min)/<br>Mean** (%) |          |
| <b>Case 600</b>   |        |       |       |            |       |        |                                |       |       |                          |          |
| Jan               | 475.4  | 554.0 | 417.9 | 521.8      | 523.0 | 495.0  | 417.9                          | 554.0 | 497.9 | 27.3%                    | 495.0    |
| Feb               | 349.2  | 394.3 | 315.4 | 387.5      | 398.0 | 367.4  | 315.4                          | 398.0 | 368.6 | 22.4%                    | 367.4    |
| Mar               | 450.3  | 474.4 | 410.7 | 484.4      | 489.0 | 457.4  | 410.7                          | 489.0 | 461.0 | 17.0%                    | 457.4    |
| Apr               | 218.7  | 220.1 | 230.2 | 240.5      | 263.0 | 235.4  | 218.7                          | 263.0 | 234.6 | 18.9%                    | 235.4    |
| May               | 342.7  | 321.2 | 338.6 | 339.9      | 364.0 | 325.2  | 321.2                          | 364.0 | 338.6 | 12.7%                    | 325.2    |
| Jun               | 578.3  | 497.4 | 526.4 | 539.6      | 550.0 | 516.1  | 497.4                          | 578.3 | 534.6 | 15.1%                    | 516.1    |
| Jul               | 568.4  | 505.9 | 525.1 | 536.4      | 556.0 | 514.4  | 505.9                          | 568.4 | 534.4 | 11.7%                    | 514.4    |
| Aug               | 658.2  | 606.5 | 621.1 | 648.5      | 674.0 | 634.1  | 606.5                          | 674.0 | 640.4 | 10.5%                    | 634.1    |
| Sep               | 724.8  | 705.2 | 672.1 | 733.7      | 743.0 | 710.5  | 672.1                          | 743.0 | 714.9 | 9.9%                     | 710.5    |
| Oct               | 628.4  | 676.1 | 611.1 | 675.3      | 681.0 | 649.5  | 611.1                          | 681.0 | 653.6 | 10.7%                    | 649.5    |
| Nov               | 394.3  | 454.7 | 377.1 | 437.7      | 444.0 | 418.6  | 377.1                          | 454.7 | 421.1 | 18.4%                    | 418.5    |
| Dec               | 433.3  | 503.3 | 386.2 | 481.9      | 476.0 | 456.1  | 386.2                          | 503.3 | 456.1 | 25.7%                    | 456.0    |
| <b>Case 900</b>   |        |       |       |            |       |        |                                |       |       |                          |          |
| Jan               | 73.3   | 67.8  | 33.5  | 53.3       | 42.0  | 44.6   | 33.5                           | 73.3  | 52.4  | 76.0%                    | 44.5     |
| Feb               | 24.0   | 15.1  | 4.7   | 12.3       | 11.0  | 9.2    | 4.7                            | 24.0  | 12.7  | 151.4%                   | 9.2      |
| Mar               | 86.4   | 68.5  | 40.9  | 65.4       | 56.0  | 50.6   | 40.9                           | 86.4  | 61.3  | 74.2%                    | 50.5     |
| Apr               | 29.3   | 12.3  | 18.3  | 18.5       | 22.0  | 16.1   | 12.3                           | 29.3  | 19.4  | 87.8%                    | 16.0     |
| May               | 131.1  | 117.8 | 128.6 | 114.5      | 125.0 | 98.4   | 98.4                           | 131.1 | 119.2 | 27.5%                    | 98.3     |
| Jun               | 447.5  | 372.3 | 408.5 | 401.3      | 404.0 | 365.8  | 365.8                          | 447.5 | 399.9 | 20.4%                    | 365.8    |
| Jul               | 440.9  | 380.4 | 408.1 | 398.7      | 410.0 | 365.5  | 365.5                          | 440.9 | 400.6 | 18.8%                    | 365.5    |
| Aug               | 532.6  | 485.7 | 510.2 | 510.3      | 531.0 | 487.6  | 485.7                          | 532.6 | 509.6 | 9.2%                     | 487.5    |
| Sep               | 517.9  | 484.0 | 466.1 | 492.8      | 492.0 | 458.9  | 458.9                          | 517.9 | 485.3 | 12.2%                    | 458.8    |
| Oct               | 296.2  | 305.6 | 269.6 | 292.7      | 281.0 | 260.9  | 260.9                          | 305.6 | 284.3 | 15.7%                    | 260.8    |
| Nov               | 72.7   | 80.5  | 56.2  | 68.0       | 63.0  | 60.2   | 56.2                           | 80.5  | 66.8  | 36.4%                    | 60.1     |
| Dec               | 62.1   | 73.7  | 38.1  | 60.9       | 48.0  | 49.5   | 38.1                           | 73.7  | 55.4  | 64.4%                    | 49.3     |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

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(TRNSYS18) vs. Annex B8, Section B8.1 Example Results  
By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

Note: The statistics in the tables below are based on the listed example results.  
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-M3. Monthly Hourly Integrated Peak Heating Loads**

| Simulation Model: | BSIMAC |     |    | CSE   |     |    | DeST  |     |    | EnergyPlus |     |    | ESP-r |     |    | TRNSYS |     |    | Example Result Statistics |           |            |                          | TRNSYS18 |     |    |  |
|-------------------|--------|-----|----|-------|-----|----|-------|-----|----|------------|-----|----|-------|-----|----|--------|-----|----|---------------------------|-----------|------------|--------------------------|----------|-----|----|--|
|                   | kW     | Day | Hr | kW    | Day | Hr | kW    | Day | Hr | kW         | Day | Hr | kW    | Day | Hr | kW     | Day | Hr | Min<br>kW                 | Max<br>kW | Mean<br>kW | (Max-Min)/<br>Mean** (%) | kW       | Day | Hr |  |
| <b>Case 600</b>   |        |     |    |       |     |    |       |     |    |            |     |    |       |     |    |        |     |    |                           |           |            |                          |          |     |    |  |
| Jan               | 3.100  | 29  | 7  | 3.020 | 1   | 1  | 3.036 | 1   | 0  | 2.978      | 1   | 3  | 3.230 | 1   | 1  | 3.359  | 1   | 1  | 2.978                     | 3.359     | 3.120      | 12.2%                    | 2.991    | 4   | 6  |  |
| Feb               | 3.041  | 9   | 7  | 2.900 | 9   | 6  | 2.922 | 9   | 5  | 3.067      | 9   | 6  | 3.140 | 9   | 6  | 3.225  | 9   | 6  | 2.900                     | 3.225     | 3.049      | 10.7%                    | 3.225    | 9   | 6  |  |
| Mar               | 2.275  | 2   | 7  | 2.034 | 17  | 6  | 2.065 | 17  | 5  | 2.115      | 17  | 6  | 2.230 | 17  | 6  | 2.287  | 17  | 6  | 2.034                     | 2.287     | 2.168      | 11.7%                    | 2.287    | 17  | 6  |  |
| Apr               | 2.446  | 3   | 6  | 2.207 | 11  | 6  | 2.238 | 11  | 5  | 2.322      | 11  | 5  | 2.380 | 11  | 6  | 2.457  | 11  | 6  | 2.207                     | 2.457     | 2.342      | 10.7%                    | 2.457    | 11  | 6  |  |
| May               | 1.645  | 3   | 5  | 1.592 | 1   | 5  | 1.569 | 1   | 4  | 1.624      | 1   | 5  | 1.750 | 1   | 5  | 1.778  | 1   | 5  | 1.569                     | 1.778     | 1.660      | 12.6%                    | 1.778    | 1   | 5  |  |
| Jun               | 0.805  | 9   | 5  | 0.778 | 9   | 5  | 0.748 | 9   | 4  | 0.732      | 9   | 5  | 0.760 | 10  | 5  | 0.853  | 9   | 5  | 0.732                     | 0.853     | 0.779      | 15.4%                    | 0.853    | 9   | 5  |  |
| Jul               | 0.599  | 25  | 6  | 0.540 | 26  | 5  | 0.512 | 26  | 4  | 0.514      | 26  | 5  | 0.570 | 26  | 5  | 0.619  | 26  | 5  | 0.512                     | 0.619     | 0.559      | 19.1%                    | 0.619    | 26  | 5  |  |
| Aug               | 0.572  | 10  | 7  | 0.553 | 17  | 6  | 0.532 | 17  | 5  | 0.479      | 17  | 6  | 0.560 | 17  | 6  | 0.591  | 17  | 6  | 0.479                     | 0.591     | 0.548      | 20.5%                    | 0.591    | 17  | 6  |  |
| Sep               | 1.229  | 28  | 24 | 1.120 | 29  | 1  | 1.114 | 29  | 2  | 1.130      | 28  | 24 | 1.190 | 29  | 1  | 1.212  | 28  | 24 | 1.114                     | 1.229     | 1.166      | 9.9%                     | 1.212    | 28  | 24 |  |
| Oct               | 1.702  | 6   | 7  | 1.624 | 15  | 6  | 1.619 | 9   | 5  | 1.682      | 15  | 5  | 1.770 | 9   | 6  | 1.813  | 15  | 6  | 1.619                     | 1.813     | 1.702      | 11.4%                    | 1.813    | 15  | 6  |  |
| Nov               | 3.255  | 26  | 8  | 2.850 | 26  | 8  | 2.931 | 26  | 7  | 3.106      | 26  | 7  | 3.110 | 26  | 7  | 3.207  | 26  | 8  | 2.850                     | 3.255     | 3.076      | 13.2%                    | 3.207    | 26  | 8  |  |
| Dec               | 3.171  | 31  | 24 | 2.941 | 31  | 24 | 2.972 | 31  | 23 | 3.204      | 31  | 24 | 3.170 | 31  | 24 | 3.278  | 31  | 24 | 2.941                     | 3.278     | 3.123      | 10.8%                    | 3.278    | 31  | 24 |  |
| <b>Case 900</b>   |        |     |    |       |     |    |       |     |    |            |     |    |       |     |    |        |     |    |                           |           |            |                          |          |     |    |  |
| Jan               | 2.322  | 7   | 7  | 2.077 | 1   | 5  | 2.178 | 1   | 4  | 1.903      | 29  | 7  | 2.200 | 1   | 5  | 2.379  | 1   | 5  | 1.903                     | 2.379     | 2.176      | 21.9%                    | 1.915    | 29  | 7  |  |
| Feb               | 2.551  | 8   | 24 | 2.443 | 9   | 6  | 2.453 | 9   | 5  | 2.687      | 9   | 6  | 2.630 | 9   | 7  | 2.778  | 9   | 7  | 2.443                     | 2.778     | 2.591      | 12.9%                    | 2.779    | 9   | 7  |  |
| Mar               | 1.774  | 16  | 7  | 1.613 | 17  | 6  | 1.646 | 17  | 5  | 1.744      | 17  | 6  | 1.760 | 17  | 7  | 1.858  | 17  | 6  | 1.613                     | 1.858     | 1.733      | 14.2%                    | 1.858    | 17  | 6  |  |
| Apr               | 1.997  | 2   | 7  | 1.771 | 3   | 4  | 1.725 | 3   | 3  | 2.004      | 3   | 4  | 1.930 | 3   | 4  | 2.036  | 3   | 4  | 1.725                     | 2.036     | 1.910      | 16.3%                    | 2.036    | 3   | 4  |  |
| May               | 1.295  | 4   | 6  | 1.142 | 1   | 5  | 1.124 | 1   | 5  | 1.268      | 1   | 5  | 1.230 | 1   | 5  | 1.324  | 1   | 5  | 1.124                     | 1.324     | 1.231      | 16.3%                    | 1.324    | 1   | 5  |  |
| Jun               | 0.000  |     |    | 0.000 | 1   | 1  |       |     |    | 0.000      | 1   | 1  | 0.000 | 1   | 1  | 0.000  | 31  | 0  | 0.000                     | 0.000     | 0.000      | ---                      | 0.000    | 1   | 1  |  |
| Jul               | 0.000  |     |    | 0.000 | 1   | 1  |       |     |    | 0.000      | 1   | 1  | 0.000 | 1   | 1  | 0.000  | 31  | 0  | 0.000                     | 0.000     | 0.000      | ---                      | 0.000    | 1   | 1  |  |
| Aug               | 0.000  |     |    | 0.000 | 1   | 1  |       |     |    | 0.000      | 1   | 1  | 0.000 | 1   | 1  | 0.000  | 31  | 0  | 0.000                     | 0.000     | 0.000      | ---                      | 0.000    | 1   | 1  |  |
| Sep               | 0.113  | 28  | 6  | 0.000 | 1   | 1  |       |     |    | 0.064      | 29  | 7  | 0.000 | 1   | 1  | 0.194  | 29  | 7  | 0.000                     | 0.194     | 0.074      | 261.6%                   | 0.195    | 29  | 7  |  |
| Oct               | 1.201  | 6   | 7  | 1.188 | 7   | 7  | 1.158 | 7   | 6  | 1.326      | 7   | 7  | 1.210 | 7   | 7  | 1.331  | 7   | 7  | 1.158                     | 1.331     | 1.236      | 14.0%                    | 1.331    | 7   | 7  |  |
| Nov               | 2.427  | 1   | 7  | 2.086 | 26  | 8  | 2.201 | 26  | 7  | 2.316      | 26  | 7  | 2.280 | 26  | 8  | 2.463  | 26  | 8  | 2.086                     | 2.463     | 2.296      | 16.4%                    | 2.463    | 26  | 8  |  |
| Dec               | 2.120  | 31  | 8  | 1.927 | 31  | 8  | 1.981 | 9   | 6  | 2.175      | 31  | 7  | 2.040 | 9   | 7  | 2.180  | 9   | 7  | 1.927                     | 2.180     | 2.070      | 12.2%                    | 2.180    | 9   | 7  |  |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**Table B8-M4. Monthly Hourly Integrated Peak Sensible Cooling Loads**

| Simulation Model: | BSIMAC |     |    | CSE   |     |    | DeST  |     |    | EnergyPlus |     |    | ESP-r |     |    | TRNSYS |     |    | Example Result Statistics |           |            |                          | TRNSYS18 |     |    |  |
|-------------------|--------|-----|----|-------|-----|----|-------|-----|----|------------|-----|----|-------|-----|----|--------|-----|----|---------------------------|-----------|------------|--------------------------|----------|-----|----|--|
|                   | kW     | Day | Hr | kW    | Day | Hr | kW    | Day | Hr | kW         | Day | Hr | kW    | Day | Hr | kW     | Day | Hr | Min<br>kW                 | Max<br>kW | Mean<br>kW | (Max-Min)/<br>Mean** (%) | kW       | Day | Hr |  |
| <b>Case 600</b>   |        |     |    |       |     |    |       |     |    |            |     |    |       |     |    |        |     |    |                           |           |            |                          |          |     |    |  |
| Jan               | 5.650  | 22  | 15 | 6.481 | 22  | 14 | 5.422 | 22  | 14 | 6.352      | 22  | 14 | 6.190 | 22  | 14 | 6.046  | 22  | 14 | 5.422                     | 6.481     | 6.023      | 17.6%                    | 6.045    | 22  | 14 |  |
| Feb               | 4.921  | 15  | 15 | 5.393 | 15  | 14 | 4.444 | 15  | 14 | 5.537      | 2   | 14 | 5.420 | 2   | 14 | 5.155  | 2   | 14 | 4.444                     | 5.537     | 5.145      | 21.2%                    | 5.155    | 2   | 14 |  |
| Mar               | 4.458  | 24  | 14 | 5.148 | 24  | 13 | 4.252 | 9   | 14 | 5.009      | 9   | 14 | 5.040 | 9   | 14 | 4.740  | 9   | 14 | 4.252                     | 5.148     | 4.774      | 18.8%                    | 4.740    | 9   | 14 |  |
| Apr               | 3.473  | 12  | 14 | 4.015 | 27  | 14 | 3.600 | 7   | 14 | 3.931      | 12  | 14 | 4.040 | 12  | 14 | 3.803  | 12  | 14 | 3.473                     | 4.040     | 3.810      | 14.9%                    | 3.803    | 12  | 14 |  |
| May               | 2.774  | 10  | 14 | 3.080 | 21  | 14 | 2.894 | 10  | 14 | 3.086      | 10  | 13 | 3.100 | 10  | 14 | 3.040  | 21  | 14 | 2.774                     | 3.100     | 2.996      | 10.9%                    | 3.040    | 21  | 14 |  |
| Jun               | 3.253  | 26  | 15 | 3.249 | 13  | 13 | 3.067 | 14  | 14 | 3.449      | 13  | 13 | 3.430 | 13  | 14 | 3.379  | 13  | 13 | 3.067                     | 3.449     | 3.304      | 11.6%                    | 3.379    | 13  | 13 |  |
| Jul               | 3.319  | 17  | 14 | 3.290 | 17  | 14 | 3.155 | 29  | 13 | 3.628      | 17  | 14 | 3.640 | 17  | 14 | 3.497  | 17  | 14 | 3.155                     | 3.640     | 3.422      | 14.2%                    | 3.497    | 17  | 14 |  |
| Aug               | 4.192  | 26  | 14 | 4.120 | 8   | 14 | 4.038 | 29  | 13 | 4.672      | 26  | 14 | 4.700 | 29  | 14 | 4.651  | 27  | 13 | 4.038                     | 4.700     | 4.395      | 15.1%                    | 4.651    | 27  | 13 |  |
| Sep               | 5.086  | 30  | 14 | 5.450 | 2   | 14 | 4.911 | 30  | 13 | 5.715      | 30  | 13 | 5.580 | 30  | 14 | 5.420  | 30  | 14 | 4.911                     | 5.715     | 5.360      | 15.0%                    | 5.420    | 30  | 14 |  |
| Oct               | 5.577  | 18  | 14 | 6.270 | 1   | 13 | 5.278 | 10  | 13 | 6.222      | 18  | 14 | 6.070 | 18  | 14 | 5.923  | 18  | 14 | 5.278                     | 6.270     | 5.890      | 16.8%                    | 5.922    | 18  | 14 |  |
| Nov               | 5.476  | 28  | 14 | 6.149 | 28  | 13 | 5.229 | 29  | 13 | 6.194      | 28  | 13 | 6.030 | 28  | 14 | 5.824  | 28  | 14 | 5.229                     | 6.194     | 5.817      | 16.6%                    | 5.824    | 28  | 14 |  |
| Dec               | 5.537  | 1   | 14 | 6.450 | 1   | 14 | 5.294 | 1   | 13 | 6.251      | 1   | 14 | 6.120 | 1   | 14 | 5.942  | 1   | 14 | 5.294                     | 6.450     | 5.932      | 19.5%                    | 5.942    | 1   | 14 |  |
| <b>Case 900</b>   |        |     |    |       |     |    |       |     |    |            |     |    |       |     |    |        |     |    |                           |           |            |                          |          |     |    |  |
| Jan               | 1.982  | 22  | 16 | 2.242 | 22  | 15 | 1.637 | 22  | 15 | 2.078      | 22  | 15 | 1.810 | 22  | 16 | 1.878  | 22  | 15 | 1.637                     | 2.242     | 1.938      | 31.2%                    | 1.877    | 22  | 15 |  |
| Feb               | 1.096  | 15  | 16 | 0.996 | 15  | 15 | 0.588 | 15  | 15 | 0.979      | 15  | 15 | 0.850 | 15  | 16 | 0.829  | 15  | 15 | 0.588                     | 1.096     | 0.890      | 57.1%                    | 0.829    | 15  | 15 |  |
| Mar               | 1.508  | 10  | 15 | 1.434 | 24  | 15 | 1.143 | 10  | 14 | 1.493      | 11  | 14 | 1.270 | 10  | 15 | 1.426  | 11  | 14 | 1.143                     | 1.508     | 1.379      | 26.5%                    | 1.425    | 11  | 14 |  |
| Apr               | 1.093  | 7   | 15 | 0.631 | 19  | 14 | 1.032 | 8   | 14 | 0.953      | 7   | 15 | 0.950 | 8   | 15 | 0.837  | 8   | 15 | 0.631                     | 1.093     | 0.916      | 50.4%                    | 0.837    | 8   | 15 |  |
| May               | 1.555  | 11  | 15 | 1.427 | 21  | 14 | 1.446 | 11  | 14 | 1.534      | 11  | 14 | 1.460 | 11  | 15 | 1.465  | 11  | 14 | 1.427                     | 1.555     | 1.481      | 8.6%                     | 1.464    | 11  | 14 |  |
| Jun               | 2.101  | 26  | 15 | 1.897 | 14  | 14 | 1.873 | 14  | 14 | 1.966      | 14  | 14 | 1.890 | 14  | 15 | 1.974  | 14  | 14 | 1.873                     | 2.101     | 1.950      | 11.7%                    | 1.974    | 14  | 14 |  |
| Jul               | 2.140  | 17  | 15 | 1.943 | 17  | 14 | 1.830 | 17  | 14 | 2.068      | 17  | 15 | 1.970 | 17  | 15 | 1.975  | 17  | 15 | 1.830                     | 2.140     | 1.988      | 15.6%                    | 1.975    | 17  | 15 |  |
| Aug               | 2.632  | 26  | 15 | 2.485 | 5   | 14 | 2.212 | 29  | 14 | 2.526      | 29  | 15 | 2.510 | 29  | 15 | 2.534  | 29  | 15 | 2.212                     | 2.632     | 2.483      | 16.9%                    | 2.534    | 29  | 15 |  |
| Sep               | 2.961  | 30  | 15 | 3.137 | 4   | 14 | 2.556 | 11  | 14 | 2.989      | 11  | 15 | 2.810 | 11  | 15 | 2.871  | 11  | 15 | 2.556                     | 3.137     | 2.887      | 20.1%                    | 2.871    | 11  | 15 |  |
| Oct               | 3.039  | 1   | 15 | 3.376 | 1   | 14 | 2.549 | 12  | 14 | 3.040      | 1   | 14 | 2.900 | 12  | 15 | 2.940  | 1   | 14 | 2.549                     | 3.376     | 2.974      | 27.8%                    | 2.940    | 1   | 14 |  |
| Nov               | 1.982  | 6   | 15 | 2.233 | 20  | 15 | 1.683 | 20  | 14 | 2.002      | 20  | 15 | 1.940 | 20  | 15 | 1.941  | 22  | 14 | 1.683                     | 2.233     | 1.963      | 28.0%                    | 1.940    | 22  | 14 |  |
| Dec               | 2.069  | 1   | 15 | 2.105 | 1   | 15 | 1.595 | 2   | 14 | 1.968      | 2   | 15 | 1.670 | 2   | 15 | 1.690  | 2   | 15 | 1.595                     | 2.105     | 1.850      | 27.6%                    | 1.689    | 2   | 15 |  |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]



**IAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-4 (TRNSYS18) vs. Annex B8, Section B8.1 Example Results**  
**By Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023**

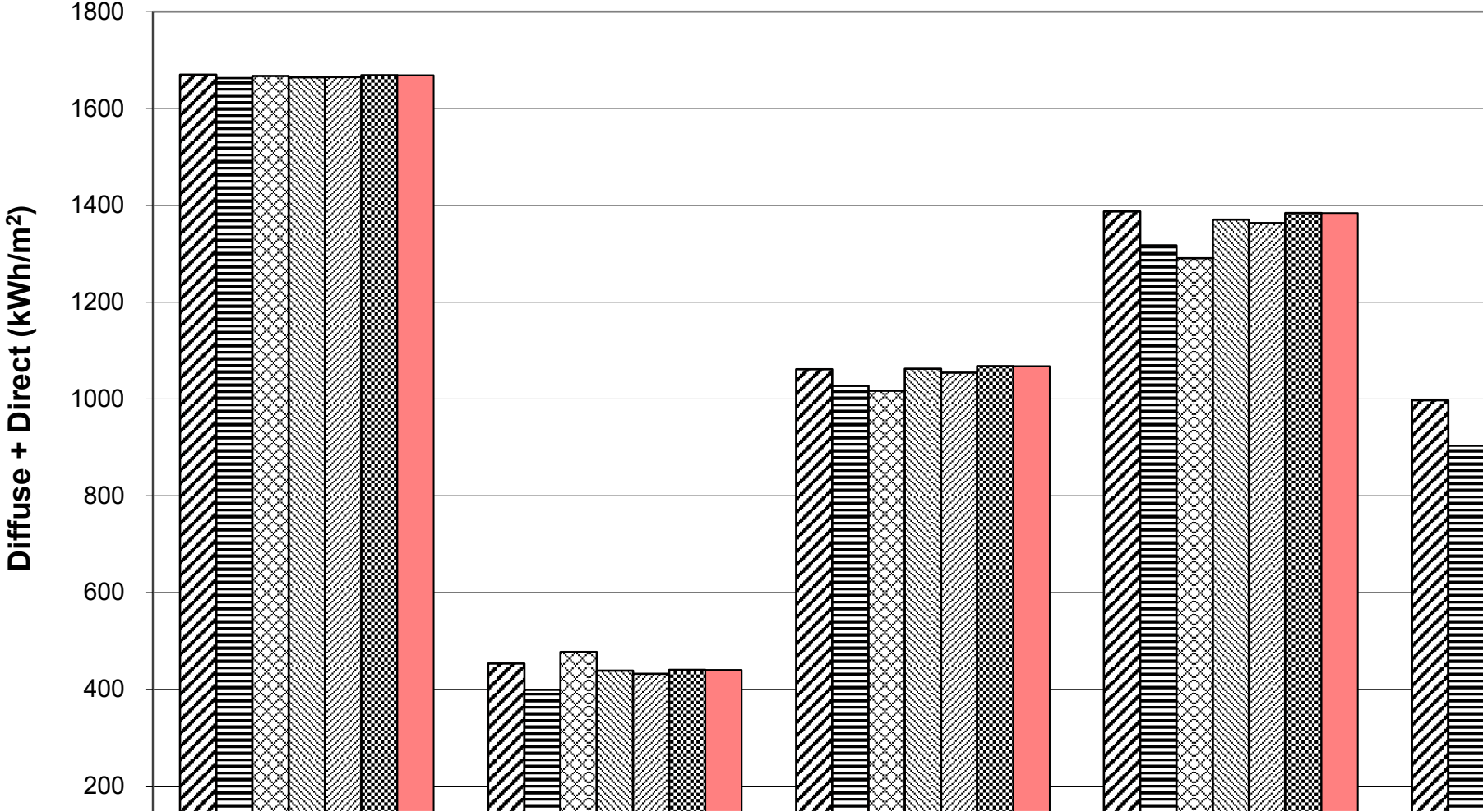
Note: The statistics in the tables below are based on the listed example results.  
 These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

**Table B8-M5. Monthly Load 600-900 Sensitivity Tests**

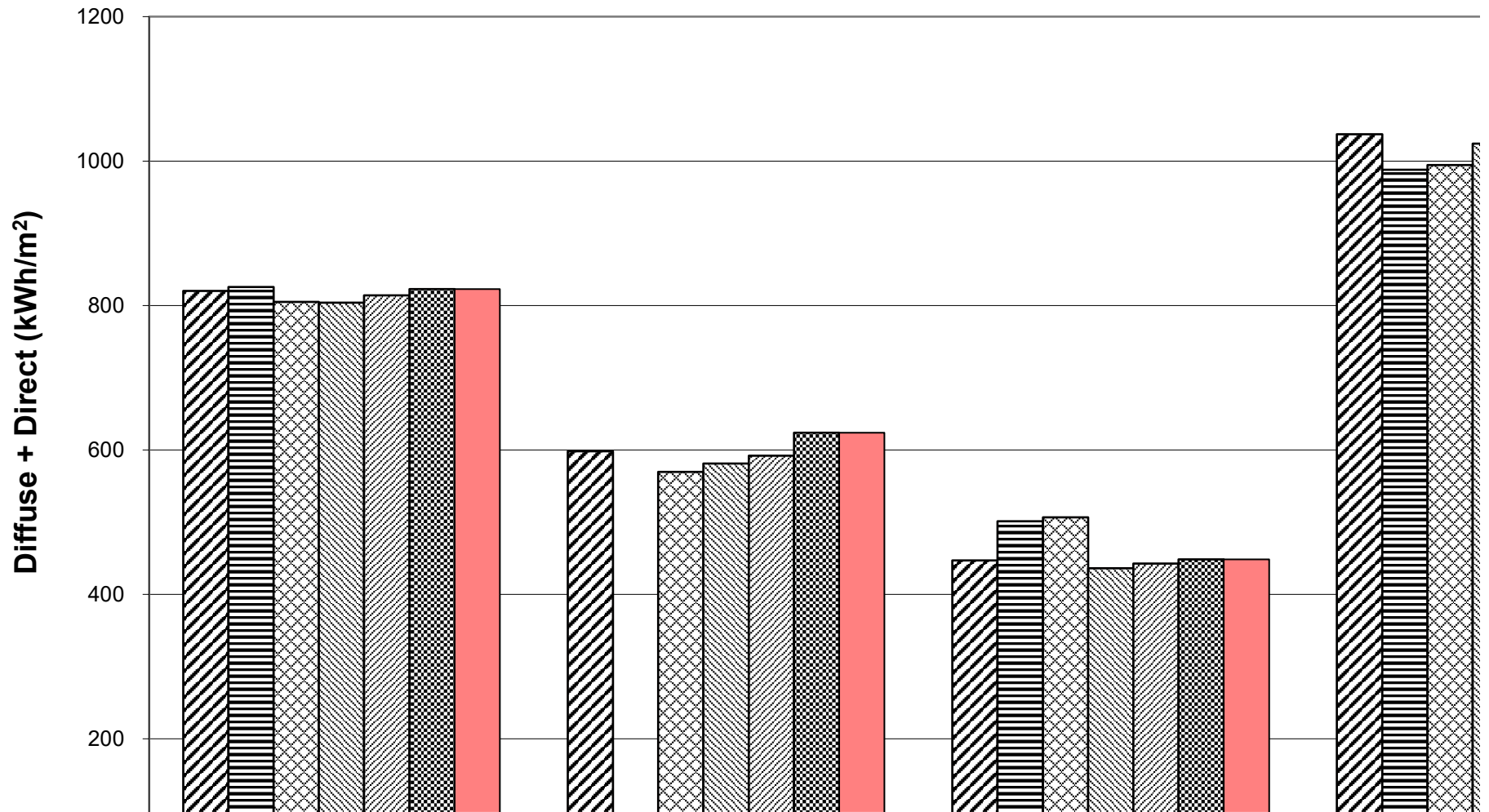
| ANNUAL HEATING [MWh]          |        |       |       |            |       |        | Statistics for Example Results |       |       |                          | TRNSYS18 |
|-------------------------------|--------|-------|-------|------------|-------|--------|--------------------------------|-------|-------|--------------------------|----------|
| Month                         | BSIMAC | CSE   | DeST  | EnergyPlus | ESP-r | TRNSYS | Min                            | Max   | Mean  | (Max-Min)/<br>Mean** (%) |          |
| Jan                           | 386.2  | 449.5 | 397.4 | 456.0      | 466.0 | 443.0  | 386.2                          | 466.0 | 433.0 | 18.4%                    | 451.1    |
| Feb                           | 345.9  | 383.0 | 342.4 | 388.5      | 399.0 | 379.9  | 342.4                          | 399.0 | 373.1 | 15.2%                    | 379.9    |
| Mar                           | 299.1  | 333.3 | 330.5 | 346.7      | 366.0 | 351.2  | 299.1                          | 366.0 | 337.8 | 19.8%                    | 351.1    |
| Apr                           | 235.3  | 234.6 | 233.8 | 241.5      | 251.0 | 241.8  | 233.8                          | 251.0 | 239.7 | 7.2%                     | 241.8    |
| May                           | 92.7   | 94.4  | 101.2 | 103.4      | 110.0 | 113.2  | 92.7                           | 113.2 | 102.5 | 20.1%                    | 113.2    |
| Jun                           | 2.7    | 11.7  | 11.2  | 10.1       | 14.0  | 16.0   | 2.7                            | 16.0  | 10.9  | 120.7%                   | 16.0     |
| Jul                           | 4.8    | 11.5  | 10.1  | 12.0       | 14.0  | 16.7   | 4.8                            | 16.7  | 11.5  | 103.0%                   | 16.7     |
| Aug                           | 1.4    | 6.9   | 8.4   | 6.6        | 9.0   | 9.6    | 1.4                            | 9.6   | 7.0   | 118.1%                   | 9.6      |
| Sep                           | 49.7   | 74.3  | 76.7  | 73.2       | 81.0  | 84.3   | 49.7                           | 84.3  | 73.2  | 47.3%                    | 84.3     |
| Oct                           | 236.5  | 263.3 | 260.6 | 266.6      | 284.0 | 282.0  | 236.5                          | 284.0 | 265.5 | 17.9%                    | 282.0    |
| Nov                           | 300.5  | 324.0 | 301.9 | 328.3      | 343.0 | 327.6  | 300.5                          | 343.0 | 320.9 | 13.3%                    | 327.5    |
| Dec                           | 368.9  | 427.3 | 383.5 | 427.9      | 442.0 | 424.2  | 368.9                          | 442.0 | 412.3 | 17.7%                    | 424.2    |
| ANNUAL SENSIBLE COOLING [MWh] |        |       |       |            |       |        | Statistics for Example Results |       |       |                          | TRNSYS18 |
| Month                         | BSIMAC | CSE   | DeST  | EnergyPlus | ESP-r | TRNSYS | Min                            | Max   | Mean  | (Max-Min)/<br>Mean** (%) |          |
| Jan                           | 402.1  | 486.2 | 384.4 | 468.5      | 481.0 | 450.4  | 384.4                          | 486.2 | 445.4 | 22.8%                    | 450.4    |
| Feb                           | 325.2  | 379.2 | 310.7 | 375.2      | 387.0 | 358.2  | 310.7                          | 387.0 | 355.9 | 21.4%                    | 358.2    |
| Mar                           | 363.9  | 405.8 | 369.8 | 419.0      | 433.0 | 406.8  | 363.9                          | 433.0 | 399.7 | 17.3%                    | 406.9    |
| Apr                           | 189.4  | 207.8 | 211.9 | 222.0      | 241.0 | 219.3  | 189.4                          | 241.0 | 215.2 | 24.0%                    | 219.3    |
| May                           | 211.6  | 203.3 | 210.0 | 225.4      | 239.0 | 226.8  | 203.3                          | 239.0 | 219.4 | 16.3%                    | 226.8    |
| Jun                           | 130.8  | 125.2 | 118.0 | 138.3      | 146.0 | 150.2  | 118.0                          | 150.2 | 134.7 | 24.0%                    | 150.3    |
| Jul                           | 127.5  | 125.4 | 117.0 | 137.7      | 146.0 | 148.9  | 117.0                          | 148.9 | 133.7 | 23.8%                    | 148.9    |
| Aug                           | 125.6  | 120.8 | 110.9 | 138.2      | 143.0 | 146.6  | 110.9                          | 146.6 | 130.8 | 27.2%                    | 146.6    |
| Sep                           | 206.9  | 221.2 | 206.0 | 240.9      | 251.0 | 251.6  | 206.0                          | 251.6 | 229.6 | 19.9%                    | 251.7    |
| Oct                           | 332.2  | 370.6 | 341.6 | 382.6      | 400.0 | 388.6  | 332.2                          | 400.0 | 369.3 | 18.4%                    | 388.7    |
| Nov                           | 321.6  | 374.3 | 320.9 | 369.7      | 381.0 | 358.4  | 320.9                          | 381.0 | 354.3 | 17.0%                    | 358.4    |
| Dec                           | 371.2  | 429.5 | 348.2 | 420.9      | 428.0 | 406.6  | 348.2                          | 429.5 | 400.7 | 20.3%                    | 406.7    |
| PEAK HEATING [kW]             |        |       |       |            |       |        | Statistics for Example Results |       |       |                          | TRNSYS18 |
| Month                         | BSIMAC | CSE   | DeST  | EnergyPlus | ESP-r | TRNSYS | Min                            | Max   | Mean  | (Max-Min)/<br>Mean** (%) |          |
| Jan                           | 0.778  | 0.943 | 0.858 | 1.075      | 1.030 | 0.980  | 0.778                          | 1.075 | 0.944 | 31.4%                    | 1.075    |
| Feb                           | 0.490  | 0.456 | 0.469 | 0.379      | 0.510 | 0.447  | 0.379                          | 0.510 | 0.459 | 28.5%                    | 0.446    |
| Mar                           | 0.501  | 0.422 | 0.419 | 0.370      | 0.470 | 0.429  | 0.370                          | 0.501 | 0.435 | 30.1%                    | 0.429    |
| Apr                           | 0.449  | 0.437 | 0.513 | 0.319      | 0.450 | 0.421  | 0.319                          | 0.513 | 0.431 | 45.0%                    | 0.421    |
| May                           | 0.350  | 0.450 | 0.445 | 0.356      | 0.520 | 0.454  | 0.350                          | 0.520 | 0.429 | 39.6%                    | 0.454    |
| Jun                           | 0.805  | 0.778 | 0.748 | 0.732      | 0.760 | 0.853  | 0.732                          | 0.853 | 0.779 | 15.4%                    | 0.853    |
| Jul                           | 0.599  | 0.540 | 0.512 | 0.514      | 0.570 | 0.619  | 0.512                          | 0.619 | 0.559 | 19.1%                    | 0.619    |
| Aug                           | 0.572  | 0.553 | 0.532 | 0.479      | 0.560 | 0.591  | 0.479                          | 0.591 | 0.548 | 20.5%                    | 0.591    |
| Sep                           | 1.116  | 1.120 | 1.114 | 1.065      | 1.190 | 1.017  | 1.017                          | 1.190 | 1.104 | 15.7%                    | 1.017    |
| Oct                           | 0.501  | 0.435 | 0.461 | 0.356      | 0.560 | 0.482  | 0.356                          | 0.560 | 0.466 | 43.7%                    | 0.482    |
| Nov                           | 0.828  | 0.764 | 0.730 | 0.790      | 0.830 | 0.744  | 0.730                          | 0.830 | 0.781 | 12.8%                    | 0.744    |
| Dec                           | 1.051  | 1.014 | 0.991 | 1.030      | 1.130 | 1.098  | 0.991                          | 1.130 | 1.052 | 13.2%                    | 1.098    |
| PEAK SENSIBLE COOLING [kW]    |        |       |       |            |       |        | Statistics for Example Results |       |       |                          | TRNSYS18 |
| Month                         | BSIMAC | CSE   | DeST  | EnergyPlus | ESP-r | TRNSYS | Min                            | Max   | Mean  | (Max-Min)/<br>Mean** (%) |          |
| Jan                           | 3.668  | 4.239 | 3.785 | 4.274      | 4.380 | 4.168  | 3.668                          | 4.380 | 4.086 | 17.4%                    | 4.168    |
| Feb                           | 3.825  | 4.397 | 3.856 | 4.558      | 4.570 | 4.326  | 3.825                          | 4.570 | 4.255 | 17.5%                    | 4.326    |
| Mar                           | 2.950  | 3.714 | 3.109 | 3.515      | 3.770 | 3.314  | 2.950                          | 3.770 | 3.395 | 24.2%                    | 3.314    |
| Apr                           | 2.380  | 3.384 | 2.568 | 2.978      | 3.090 | 2.966  | 2.380                          | 3.384 | 2.894 | 34.7%                    | 2.966    |
| May                           | 1.219  | 1.652 | 1.448 | 1.553      | 1.640 | 1.576  | 1.219                          | 1.652 | 1.515 | 28.6%                    | 1.576    |
| Jun                           | 1.152  | 1.352 | 1.194 | 1.483      | 1.540 | 1.405  | 1.152                          | 1.540 | 1.354 | 28.7%                    | 1.405    |
| Jul                           | 1.179  | 1.347 | 1.325 | 1.560      | 1.670 | 1.522  | 1.179                          | 1.670 | 1.434 | 34.3%                    | 1.522    |
| Aug                           | 1.560  | 1.634 | 1.826 | 2.146      | 2.190 | 2.117  | 1.560                          | 2.190 | 1.912 | 32.9%                    | 2.117    |
| Sep                           | 2.125  | 2.313 | 2.355 | 2.726      | 2.770 | 2.549  | 2.125                          | 2.770 | 2.473 | 26.1%                    | 2.549    |
| Oct                           | 2.538  | 2.894 | 2.729 | 3.182      | 3.170 | 2.983  | 2.538                          | 3.182 | 2.916 | 22.1%                    | 2.983    |
| Nov                           | 3.494  | 3.916 | 3.546 | 4.192      | 4.090 | 3.883  | 3.494                          | 4.192 | 3.854 | 18.1%                    | 3.884    |
| Dec                           | 3.468  | 4.345 | 3.699 | 4.283      | 4.450 | 4.252  | 3.468                          | 4.450 | 4.083 | 24.1%                    | 4.253    |

\*\* ABS[ (Max-Min) / (Mean of Example Simulation Results) ]

**Figure B8-1.**  
**Annual Incident Solar Radiation**

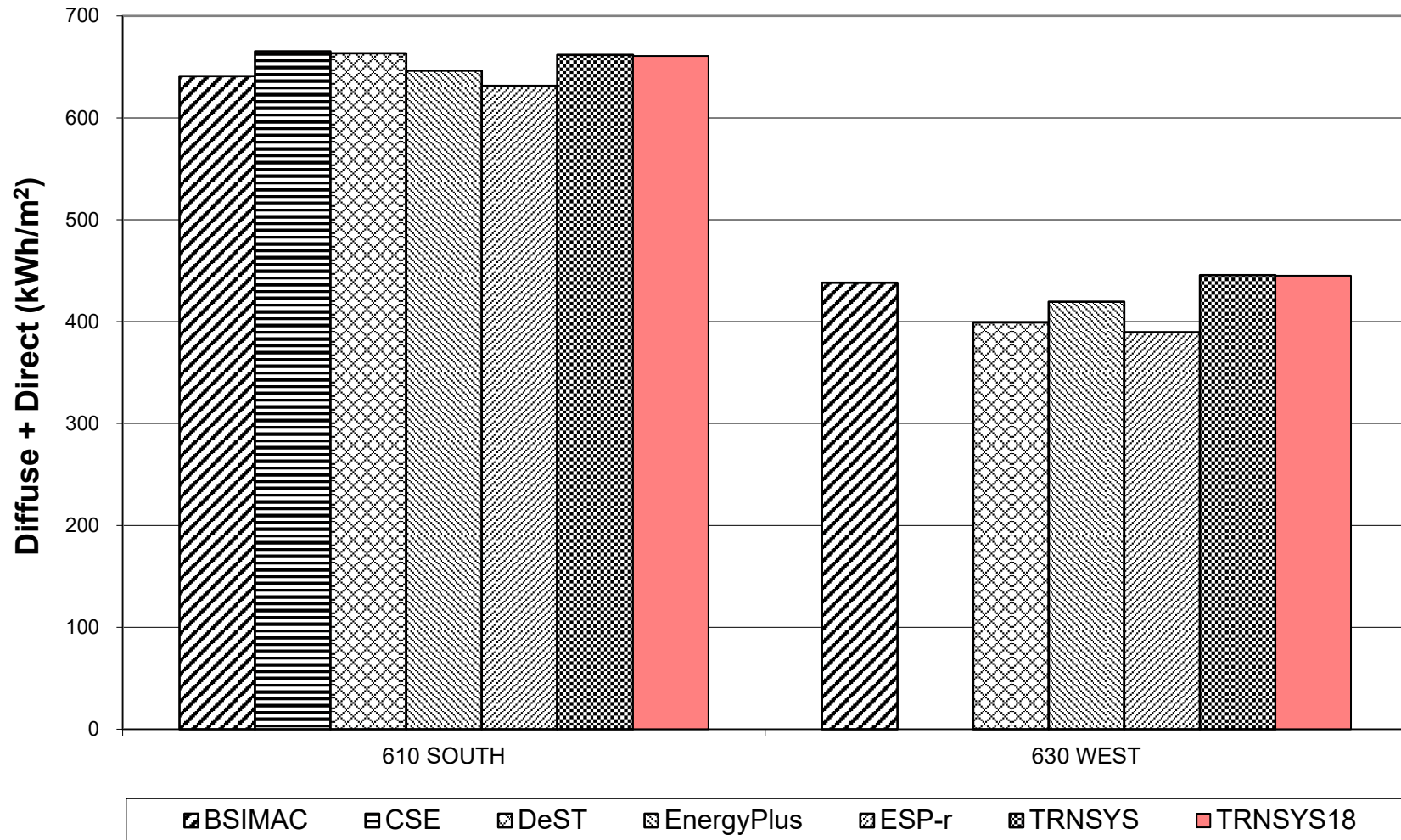


**Figure B8-2.**  
**Annual Transmitted Solar Radiation - Unshaded**

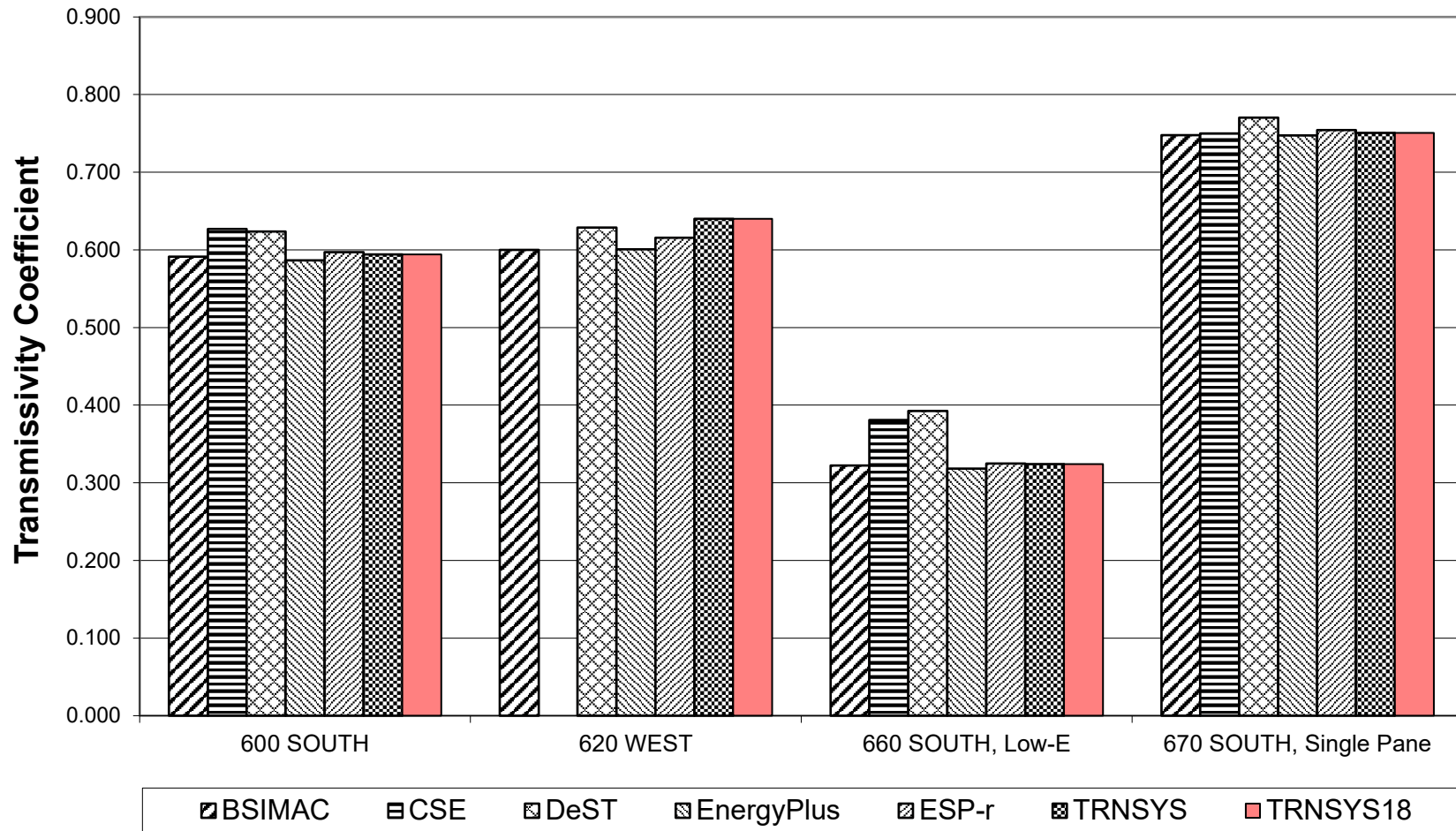


ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

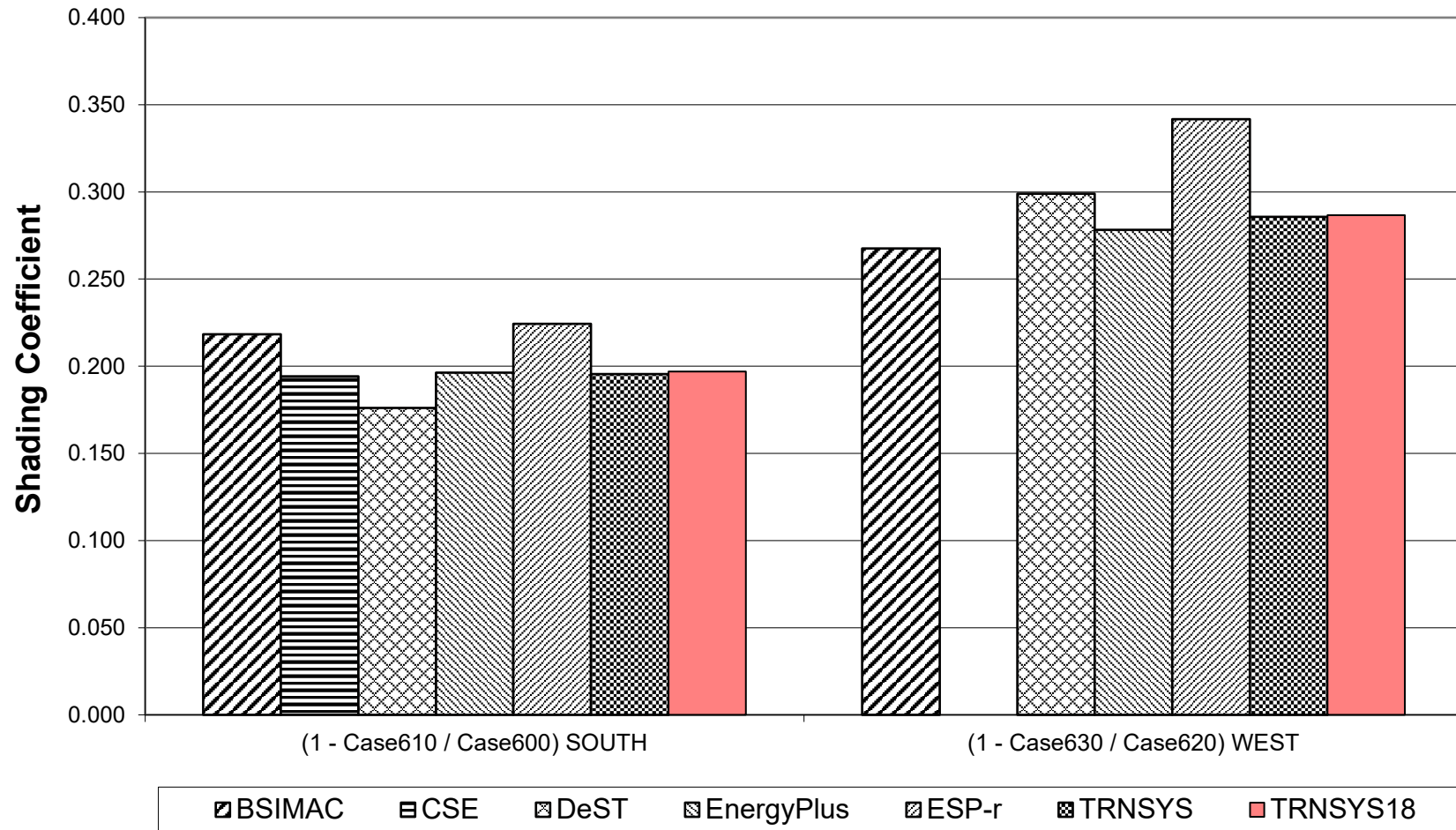
**Figure B8-3.**  
**Annual Transmitted Solar Radiation - Shaded**



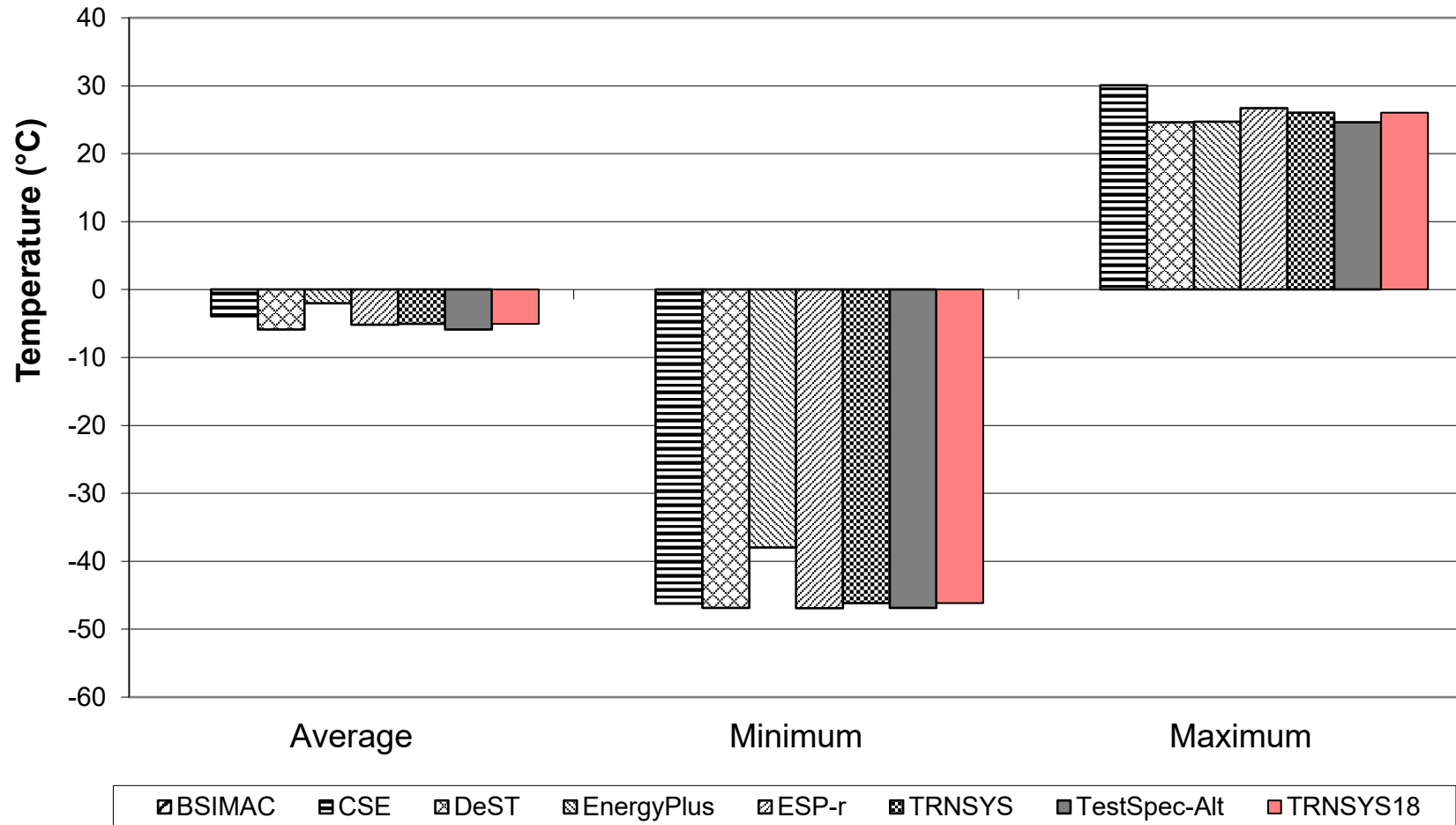
**Figure B8-4.**  
**Annual Transmissivity Coefficient of Windows**  
**(Unshaded Transmitted)/(Incident Solar Radiation)**



**Figure B8-5.**  
**Annual Overhang and Fin Shading Coefficients**  
**(1-(Shaded)/(Unshaded)) Transmitted Solar Radiation**

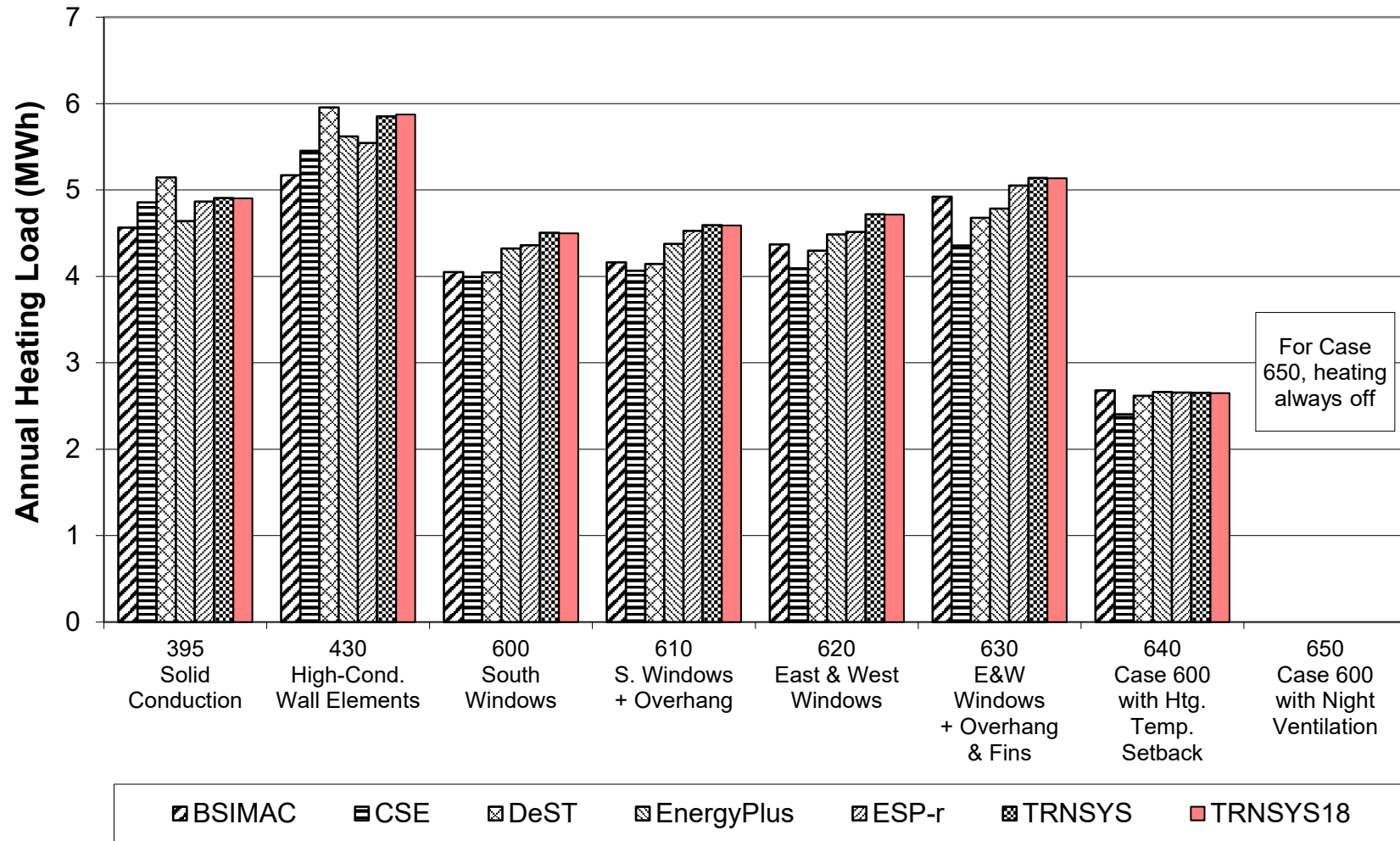


**Figure B8-6.**  
**Average, Minimum and Maximum Sky Temperature**  
**Case 600**



ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

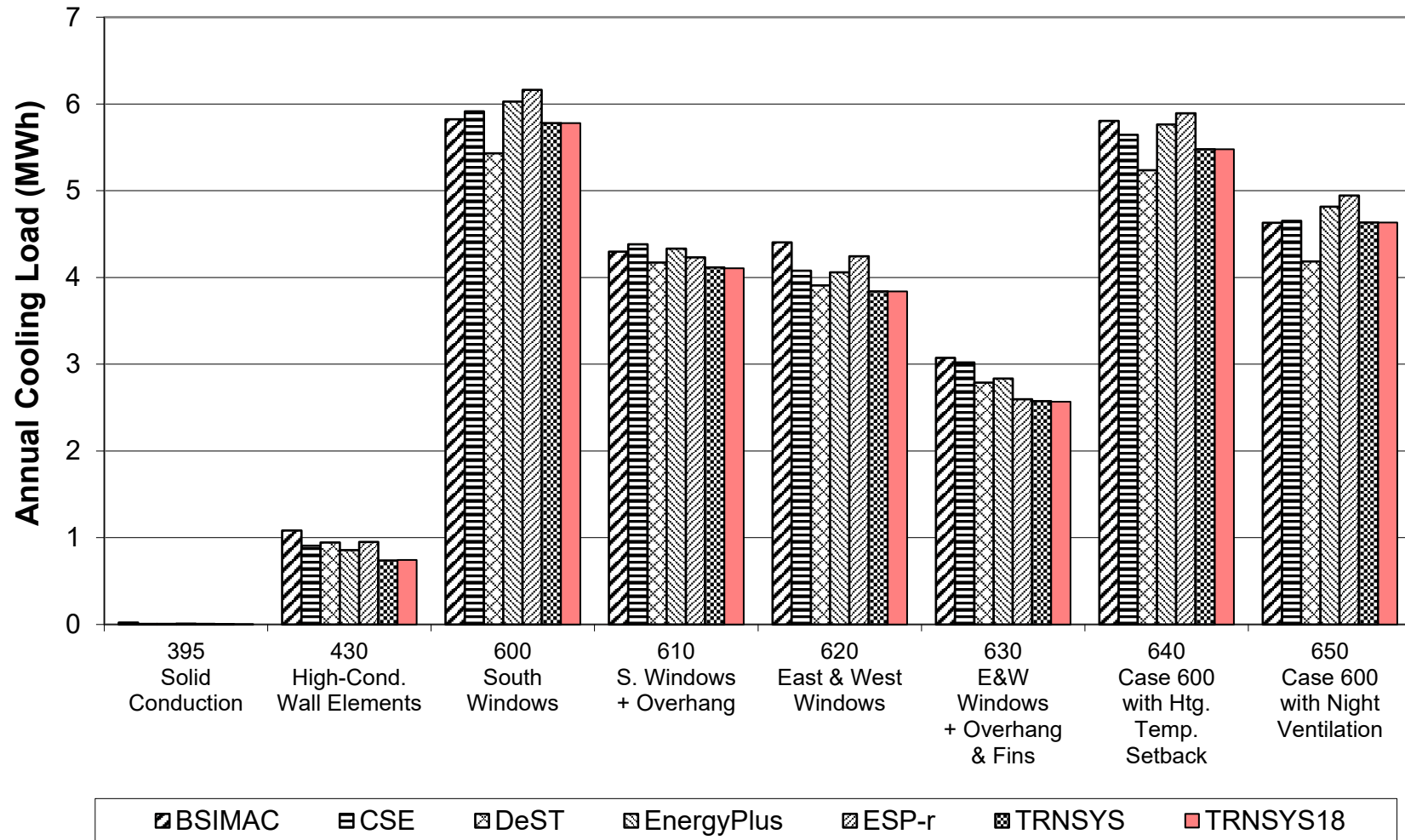
**Figure B8-7. Basic:  
Low Mass Annual Heating**





ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

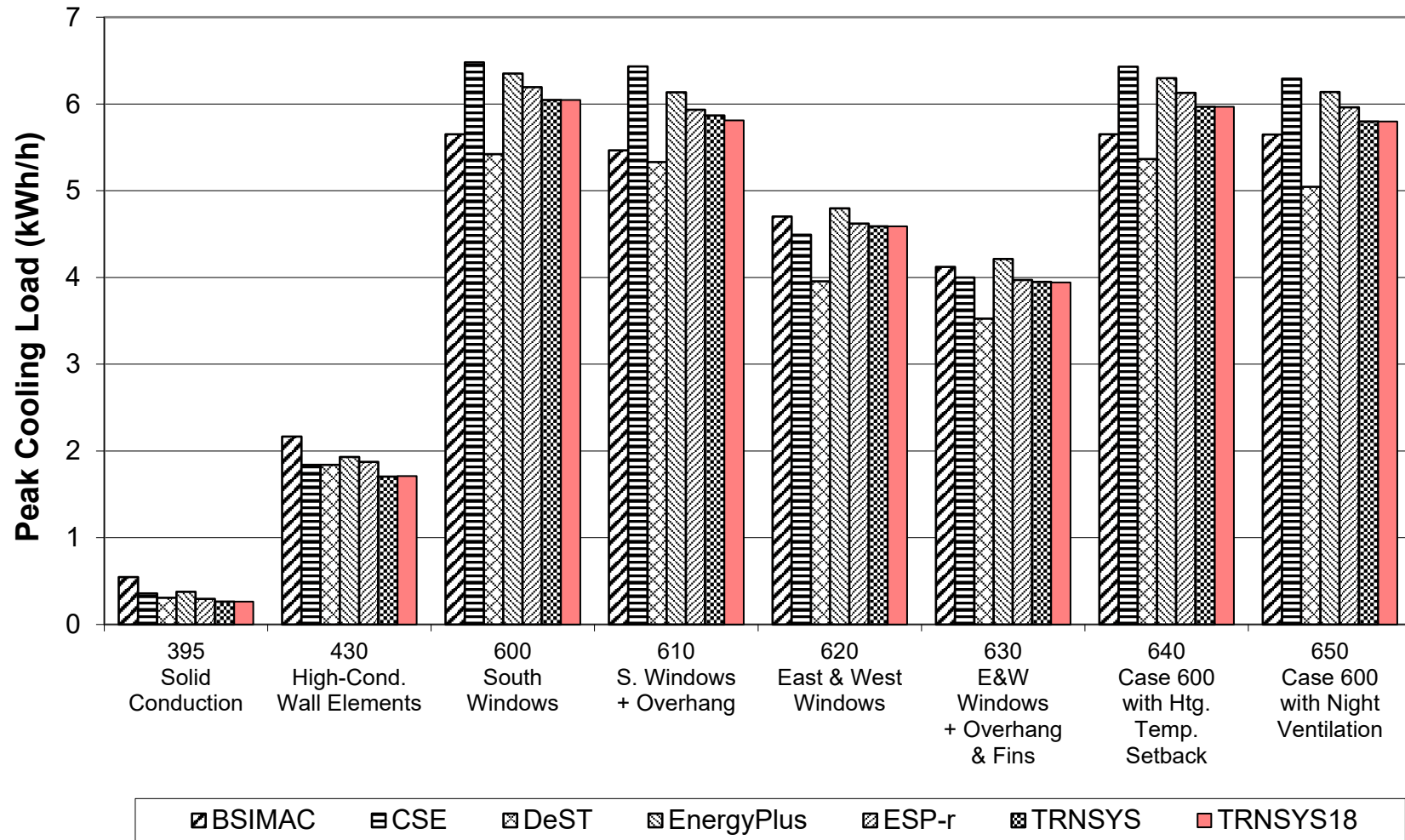
**Figure B8-8. Basic:  
Low Mass Annual Sensible Cooling**





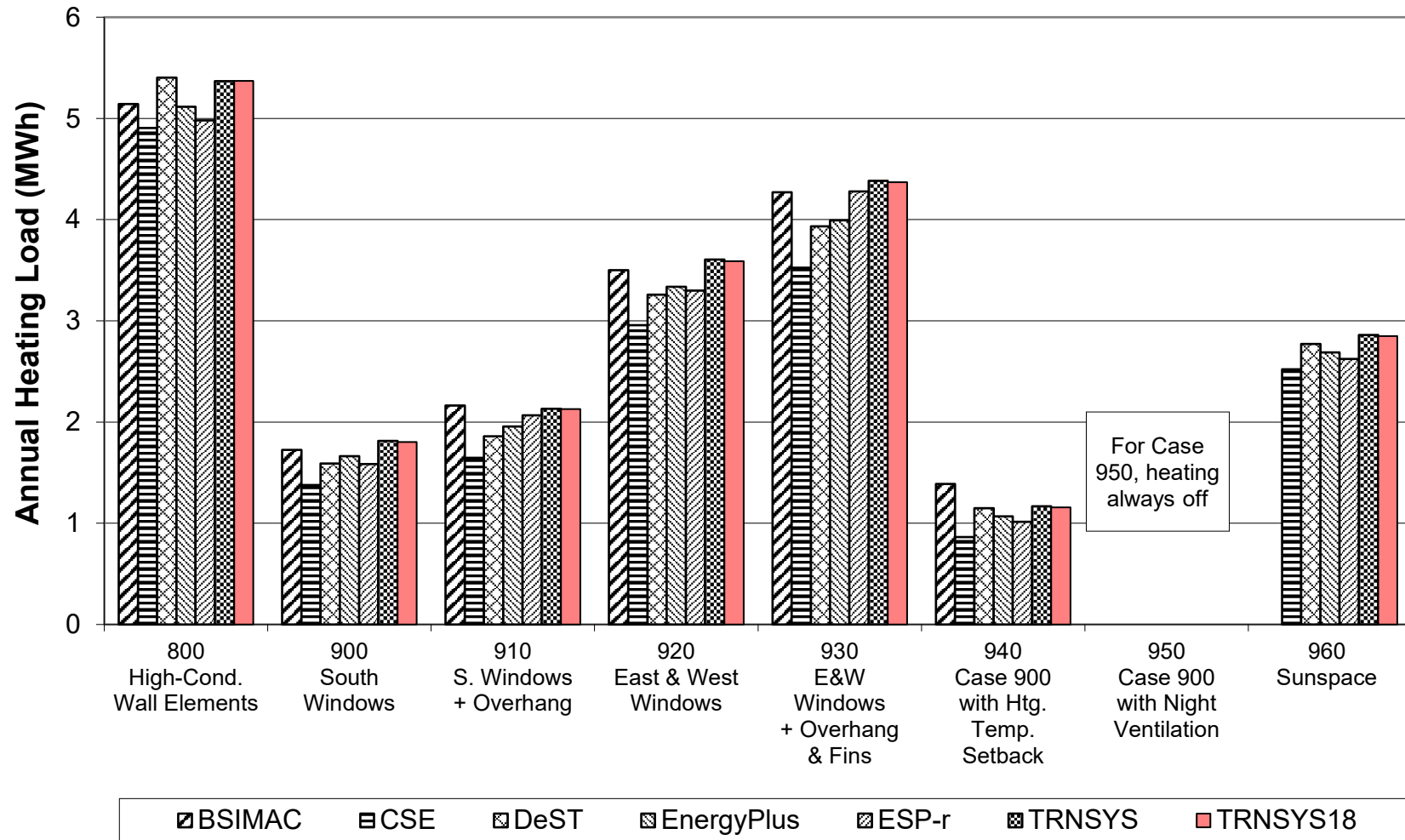
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-10. Basic:  
Low Mass Peak Sensible Cooling**



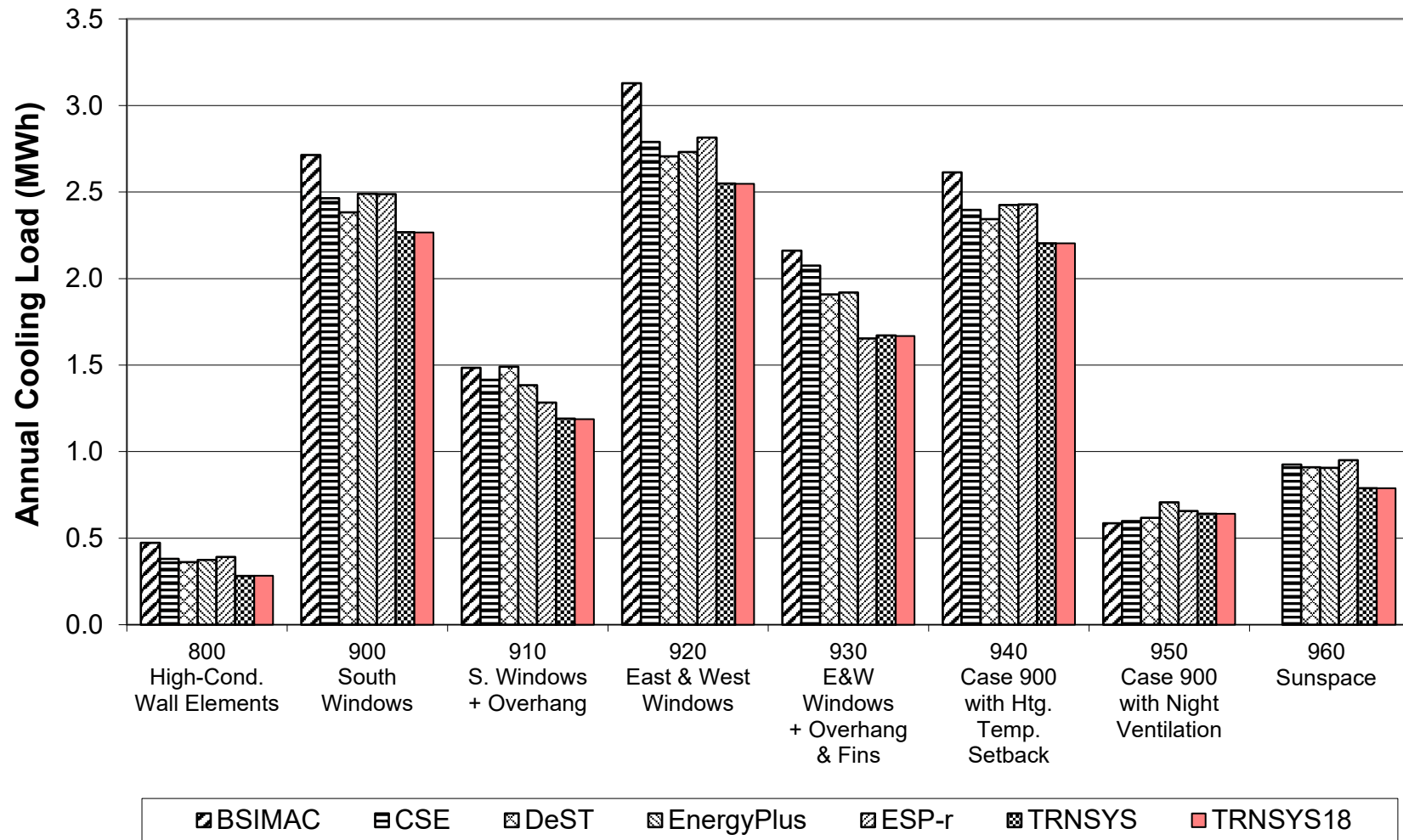
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-11. Basic:  
High Mass Annual Heating**



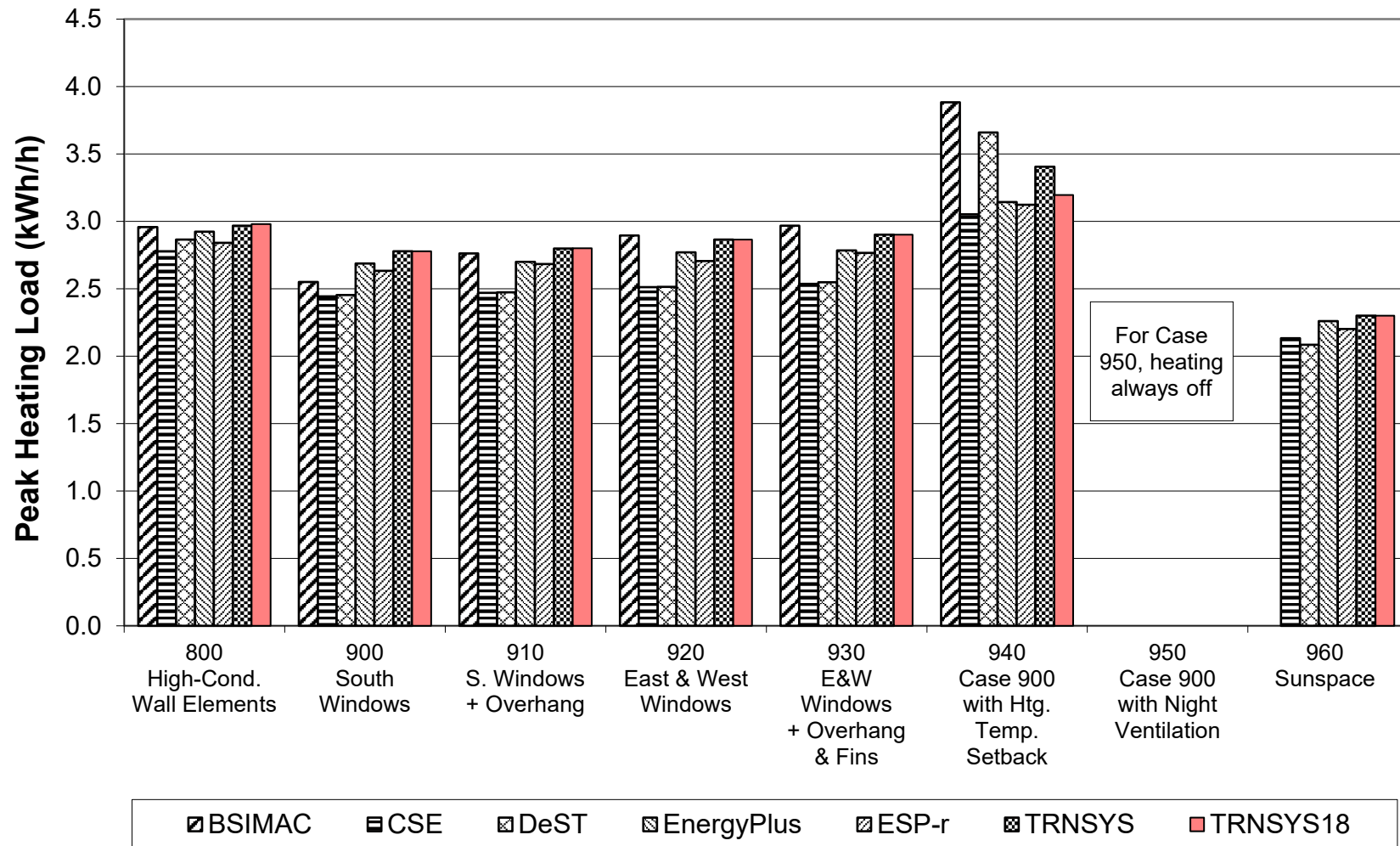
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-12. Basic:  
High Mass Annual Sensible Cooling**



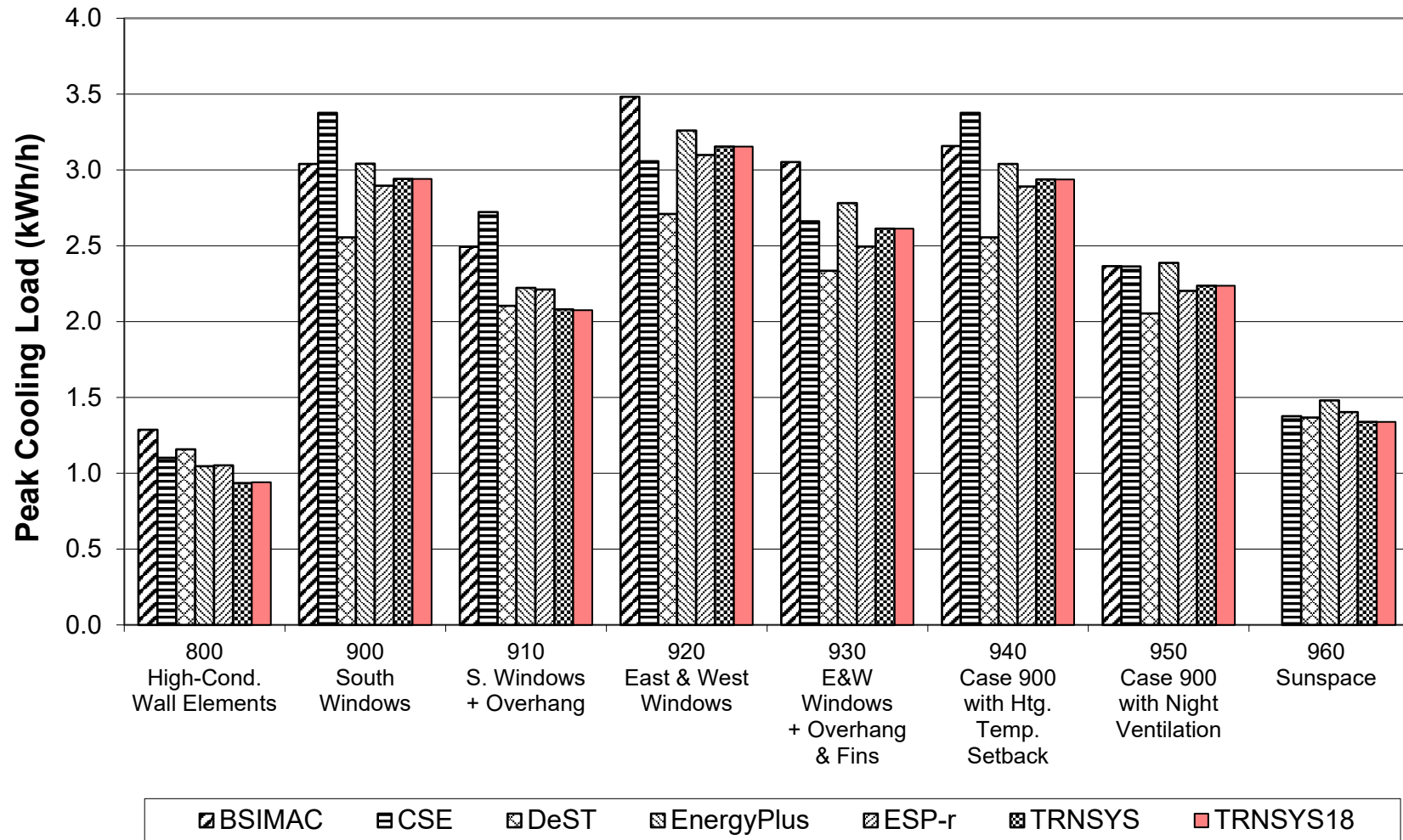
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-13. Basic:  
High Mass Peak Heating**

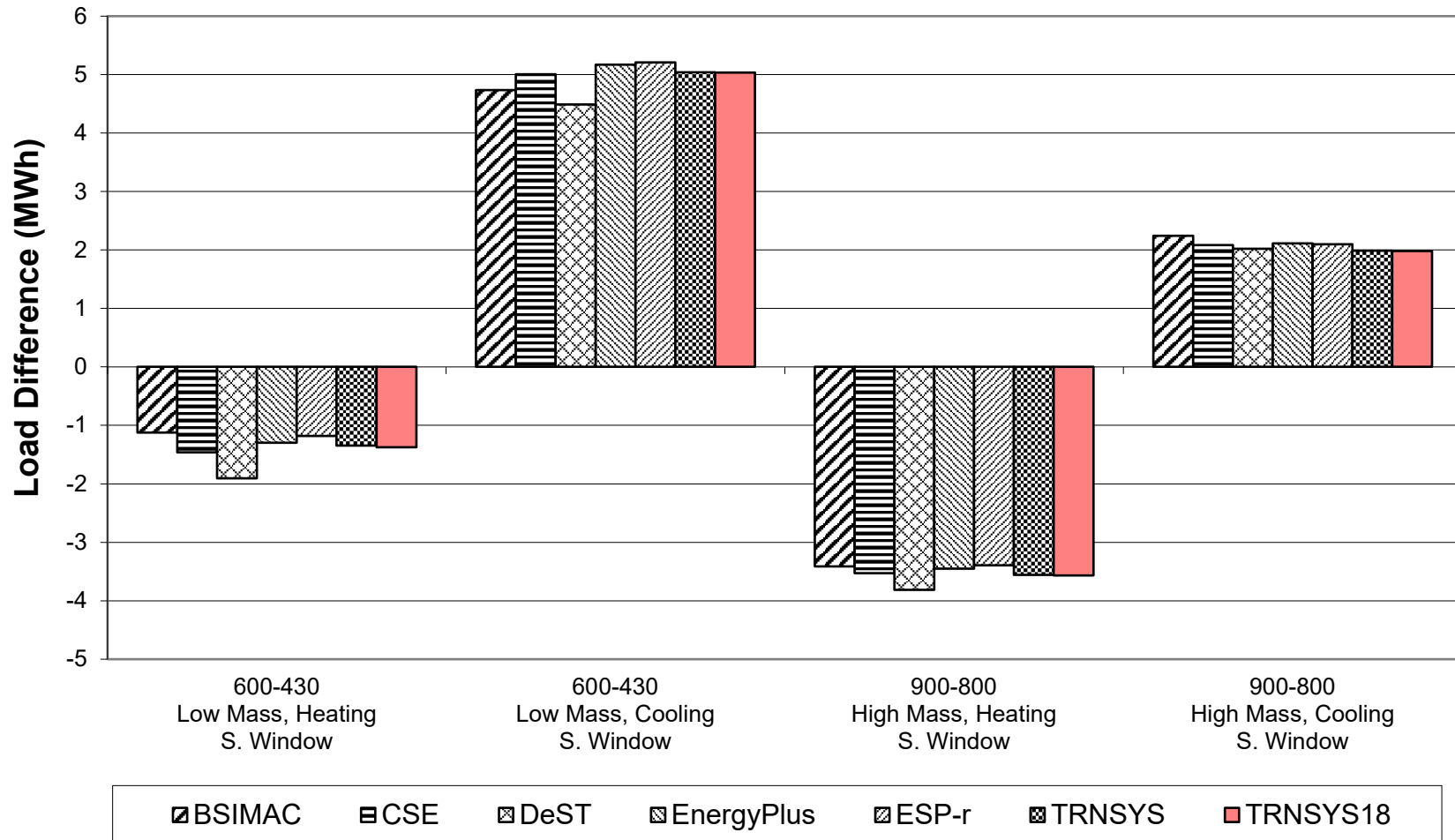


ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-14. Basic:  
High Mass Peak Sensible Cooling**

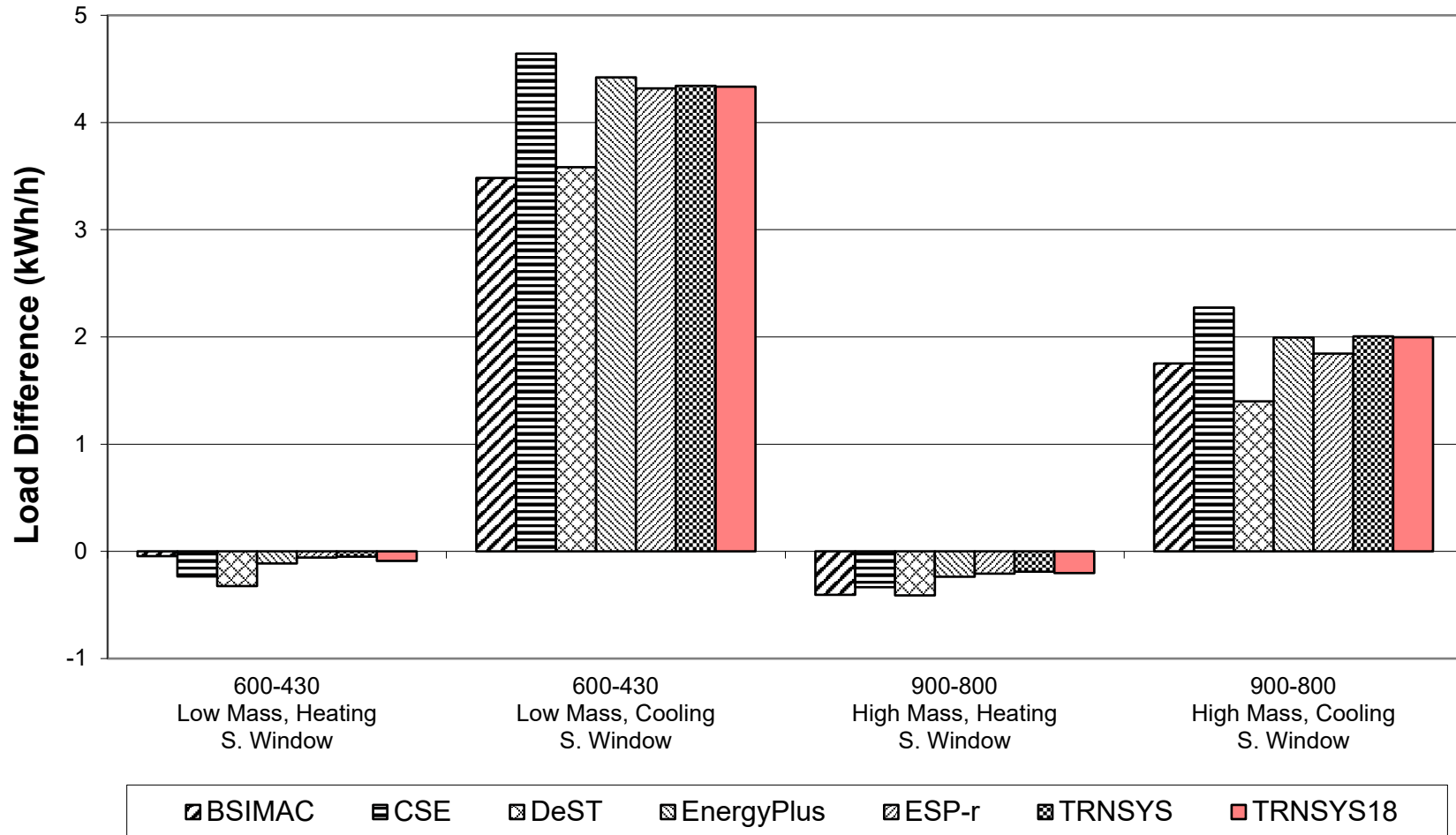


**Figure B8-15. Basic and In-Depth:  
South Window (Delta)  
Annual Heating and Sensible Cooling**

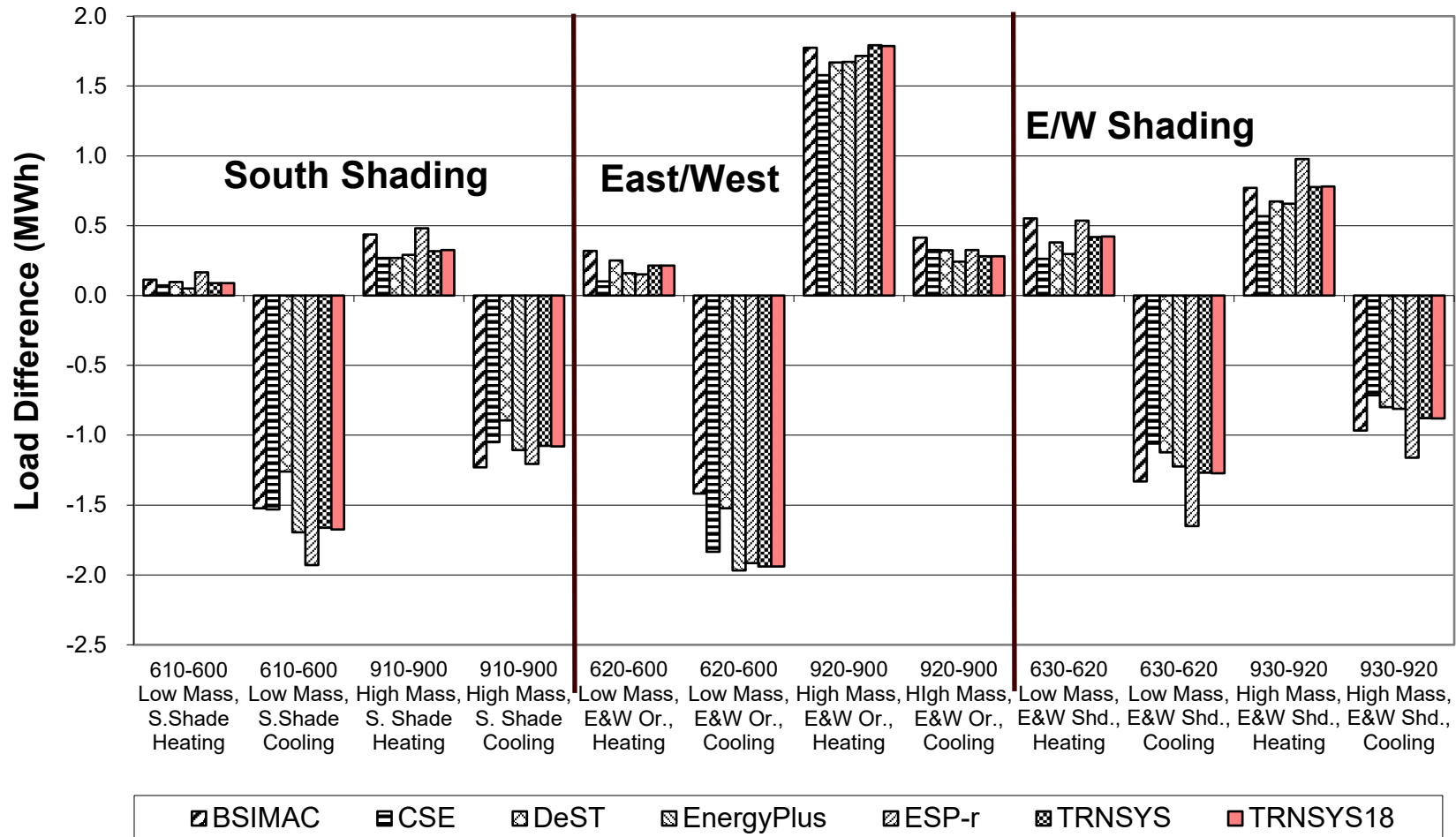




**Figure B8-16. Basic and In-Depth:  
South Window (Delta)  
Peak Heating and Sensible Cooling**

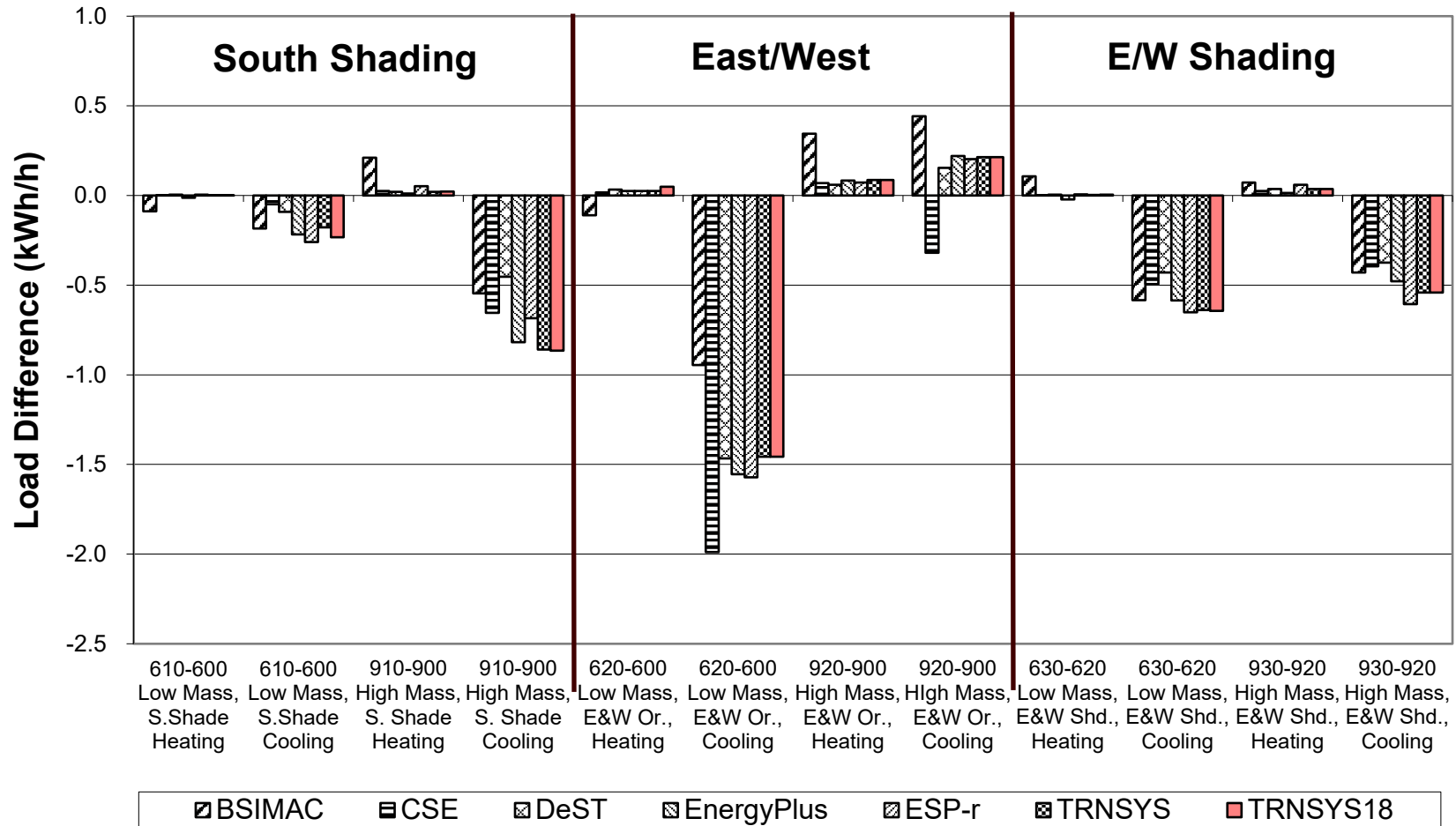


**Figure B8-17. Basic:  
Window Shading and Orientation (Delta)  
Annual Heating and Sensible Cooling**



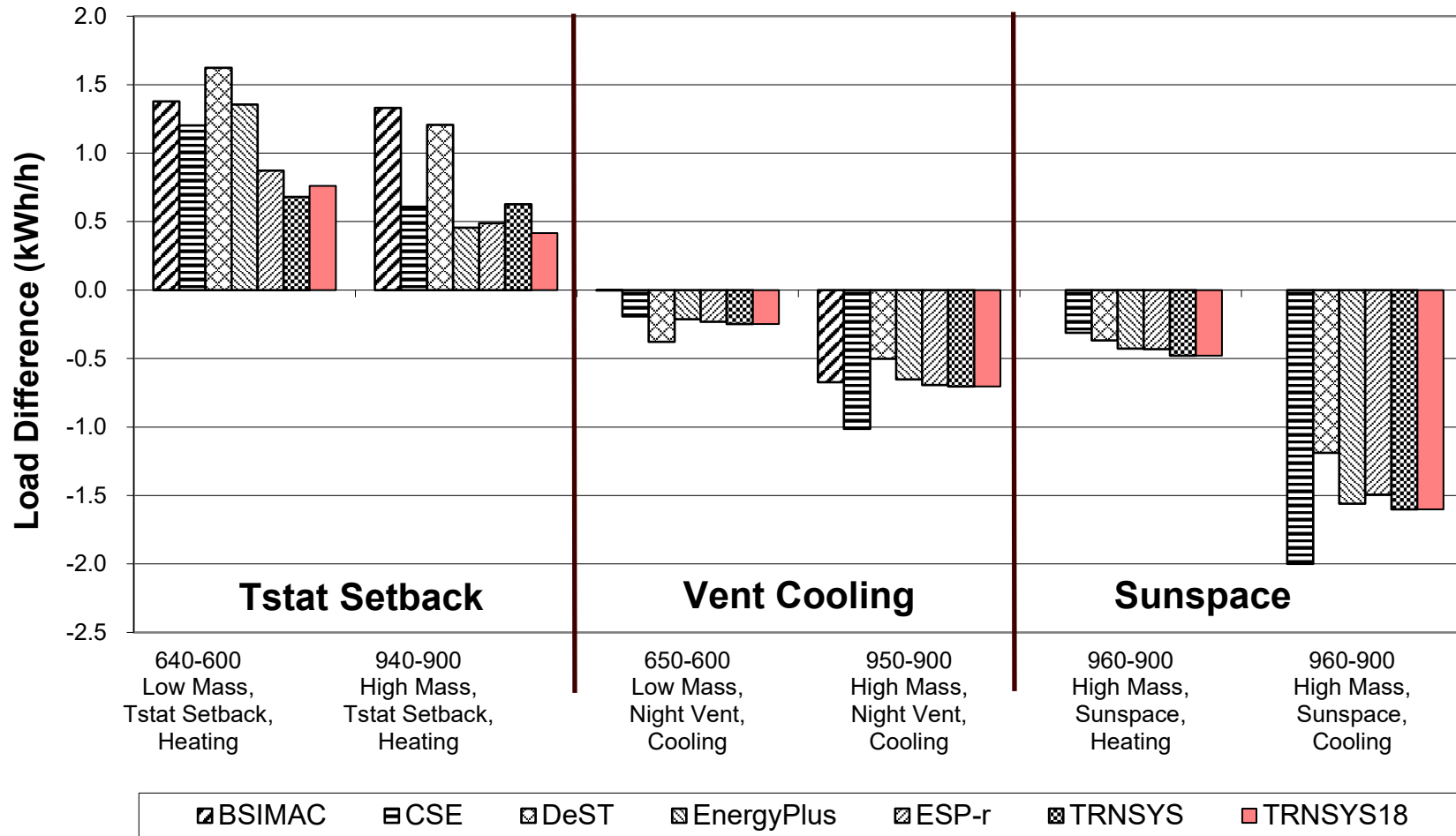
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-18. Basic:  
Window Shading and Orientation (Delta)  
Peak Heating and Sensible Cooling**



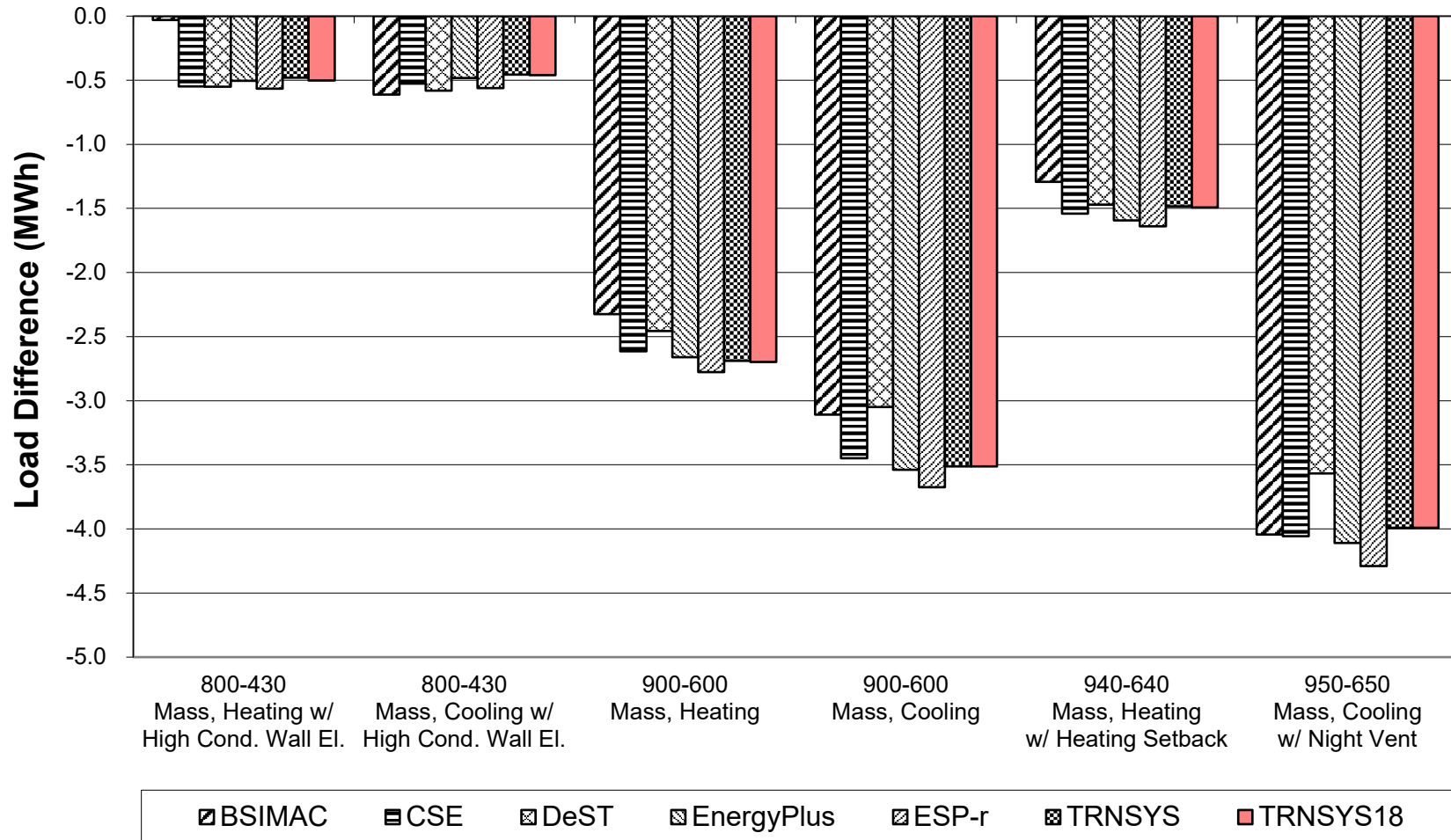


**Figure B8-20. Basic:  
Thermostat Setback, Vent Cooling, and Sunspace (Delta)  
Peak Heating and Sensible Cooling**



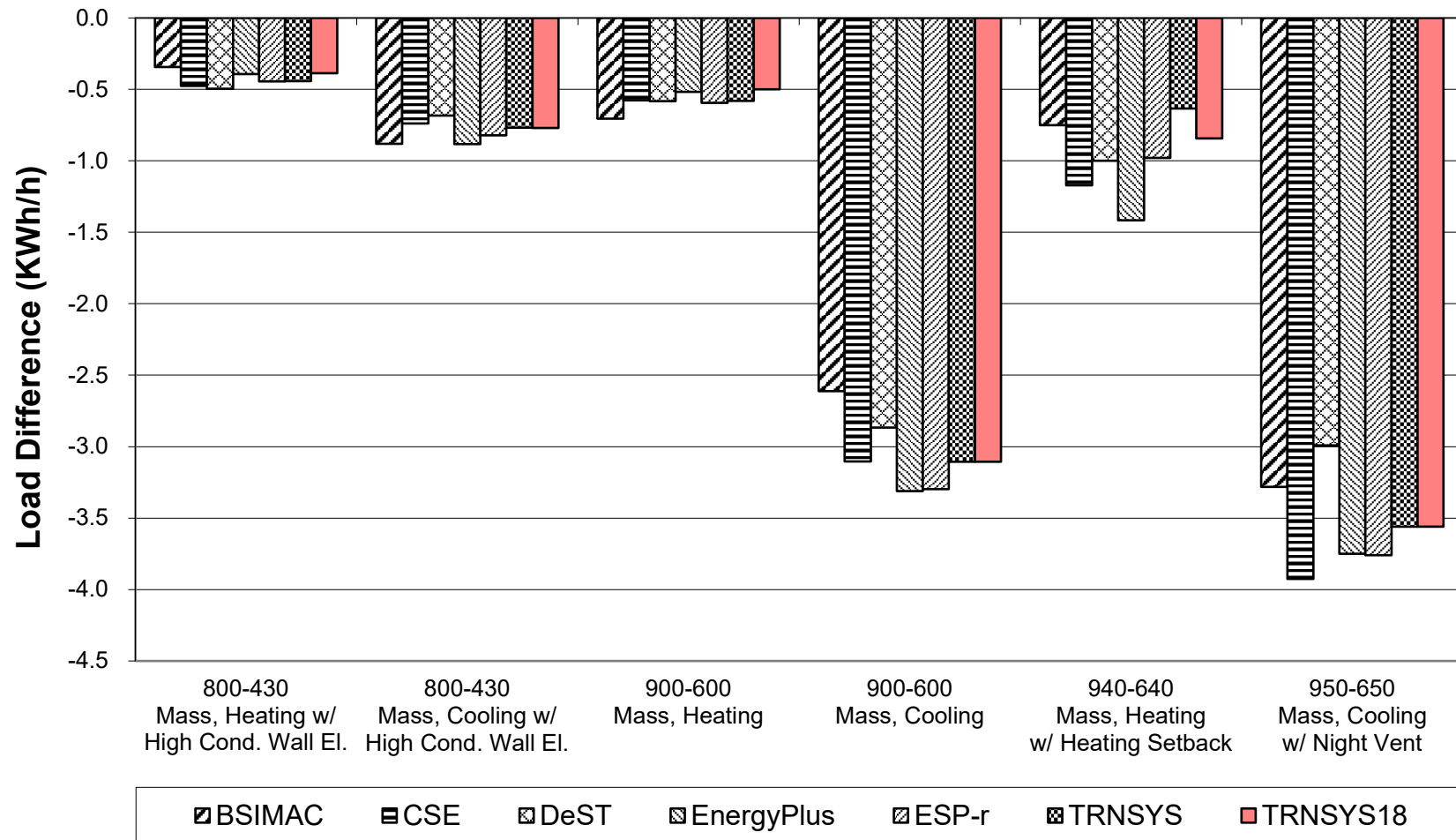
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-21. Basic and In-Depth:  
Mass Effect (Delta)  
Annual Heating and Sensible Cooling**



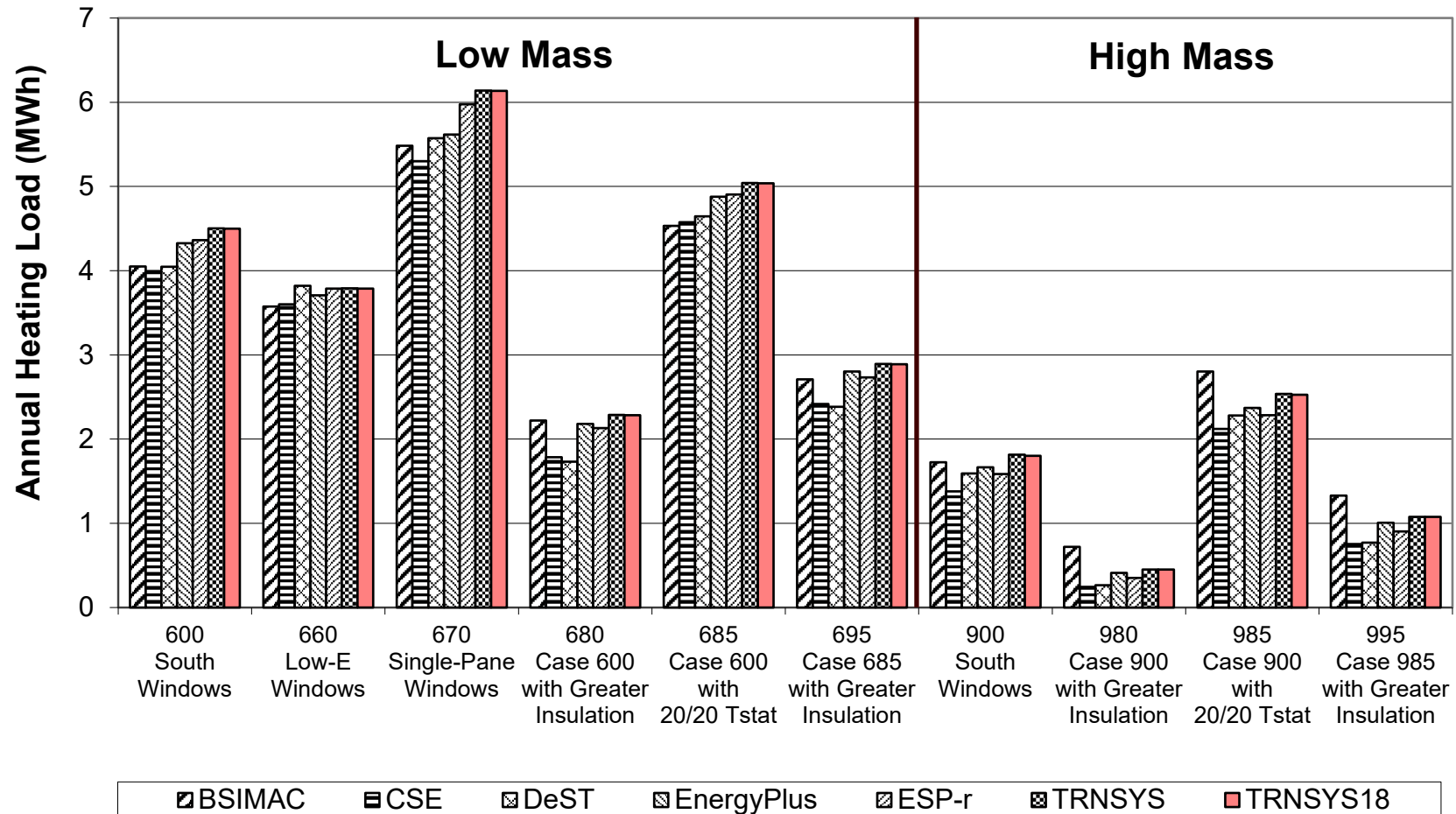
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-22. Basic and In-Depth:  
Mass Effect (Delta)  
Peak Heating and Sensible Cooling**



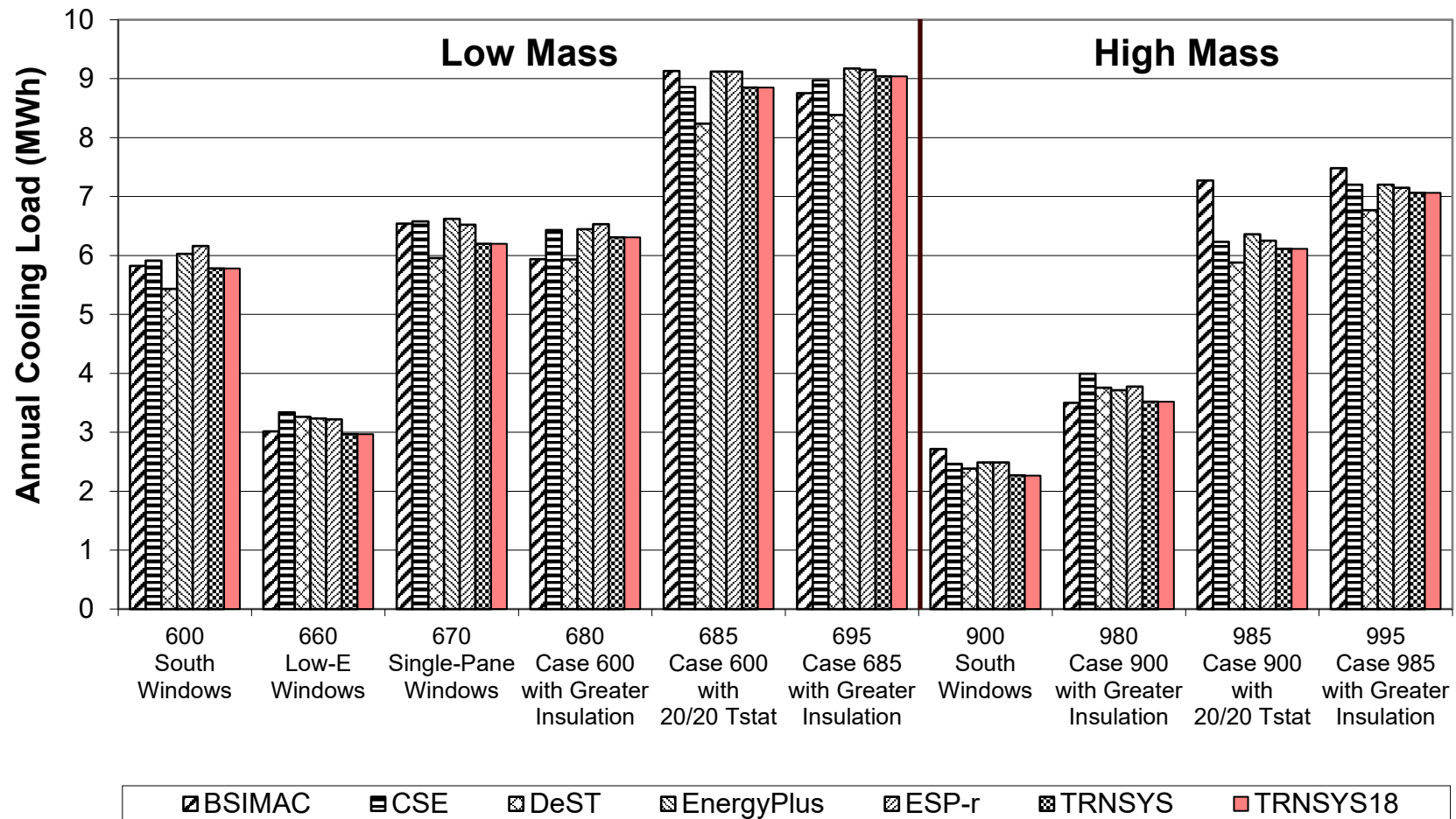
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-23. Basic:  
Cases 660 to 695 and 980 to 995  
Annual Heating**

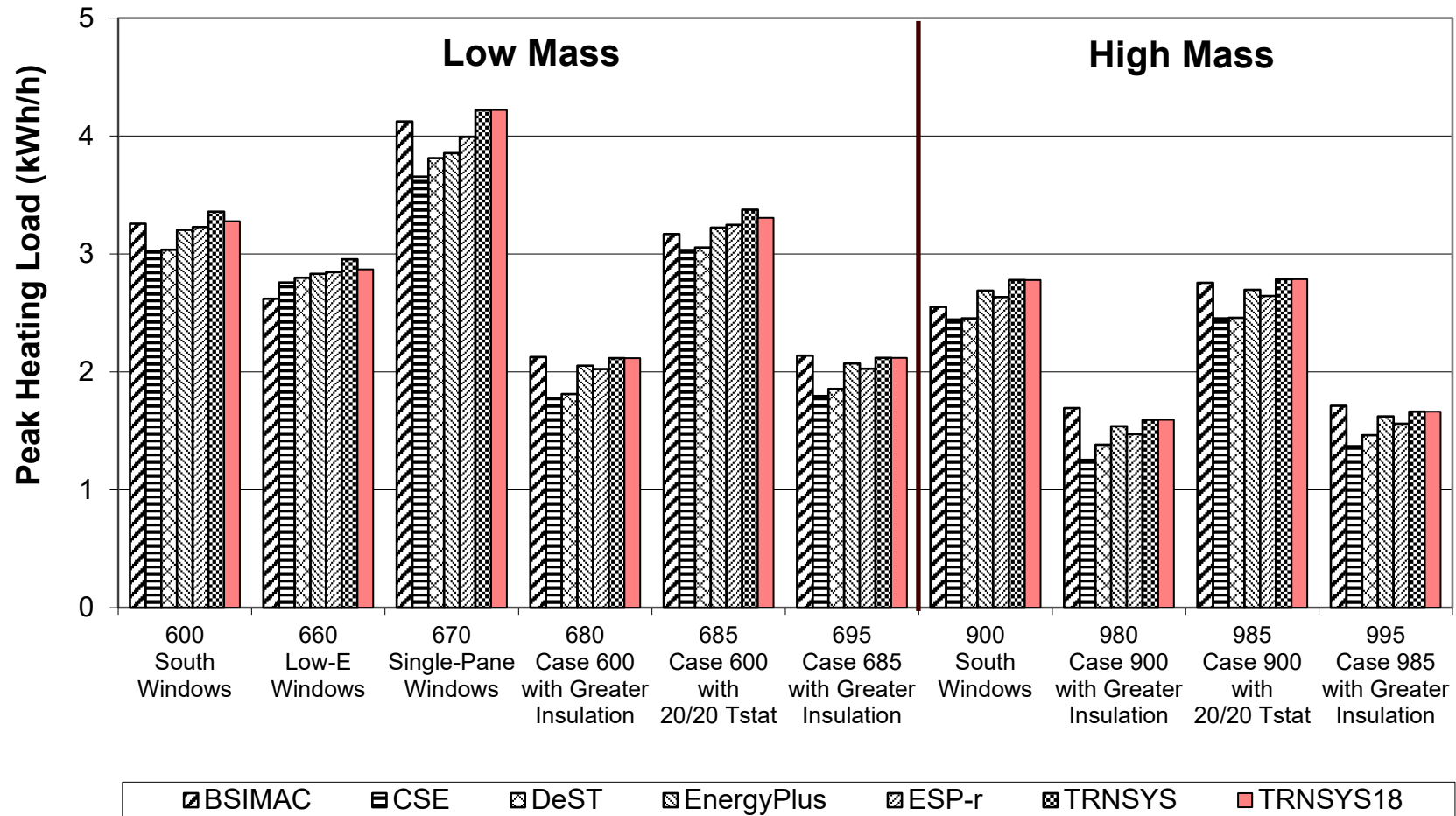




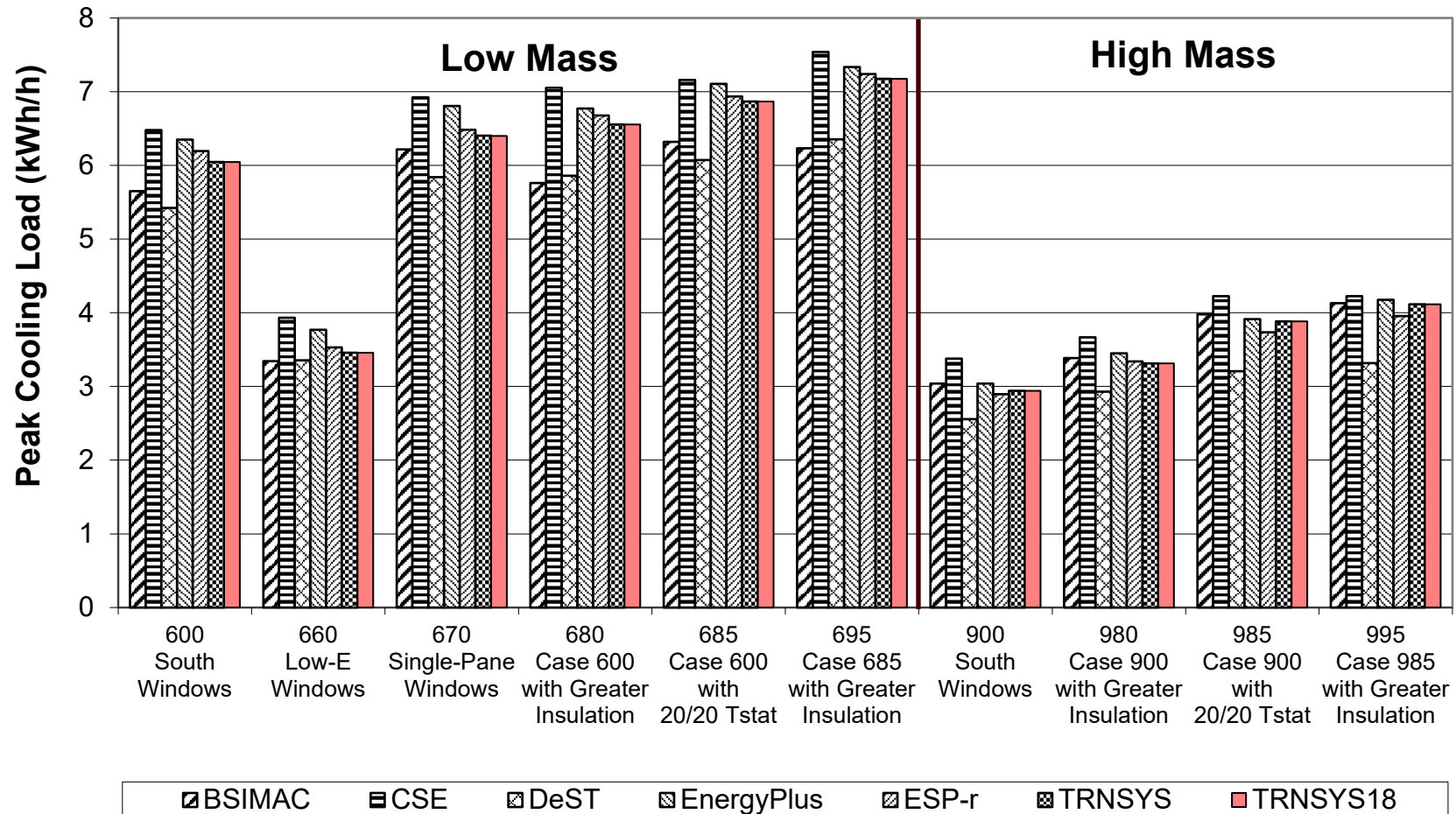
**Figure B8-24. Basic:  
Cases 660 to 695 and 980 to 995  
Annual Cooling**



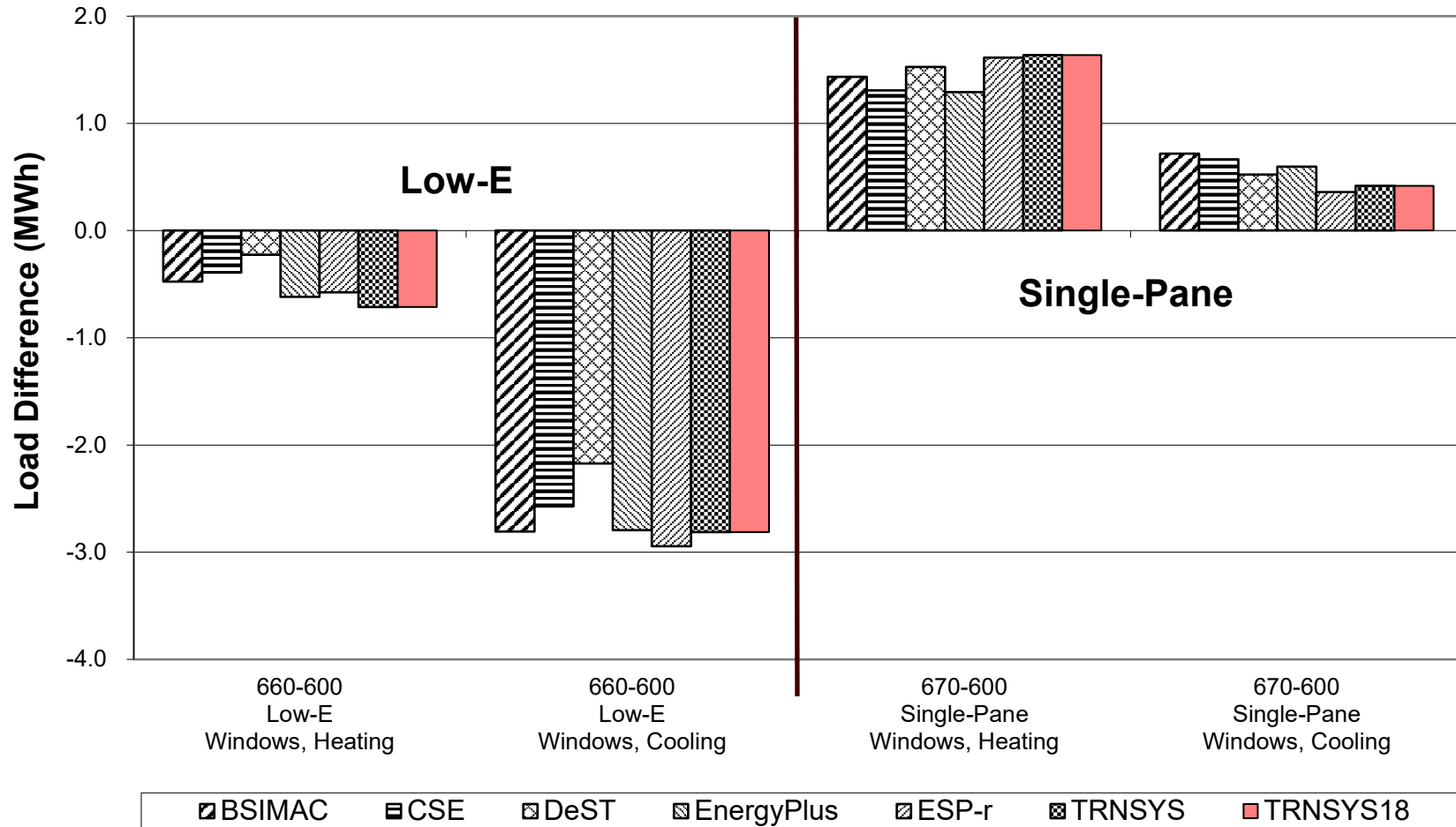
**Figure B8-25. Basic:  
Cases 660 to 695 and 980 to 995  
Peak Heating**



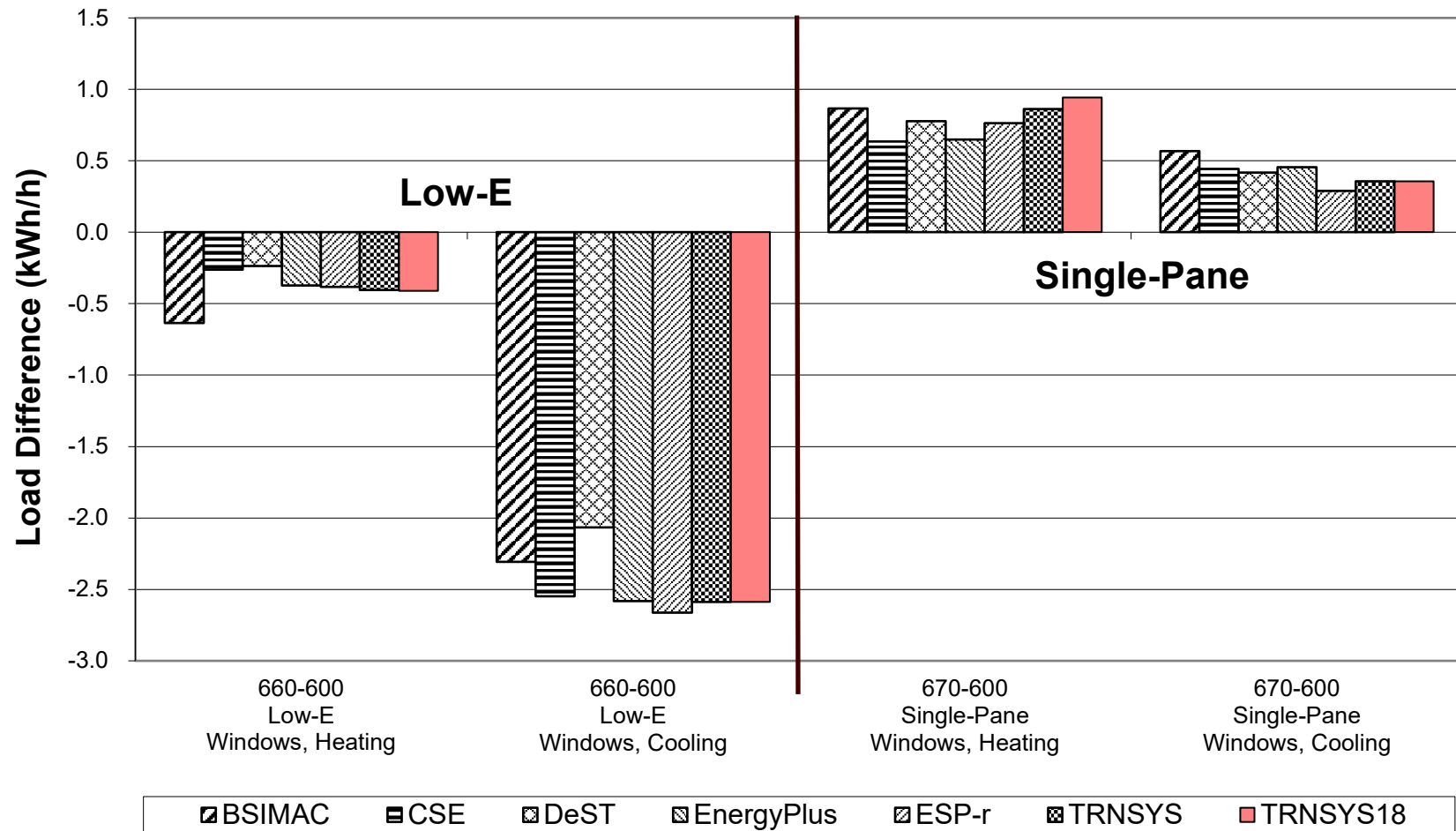
**Figure B8-26. Basic:  
Cases 660 to 695 and 980 to 995  
Peak Cooling**



**Figure B8-27. Basic:  
Window Types (Delta)  
Annual Heating and Sensible Cooling**

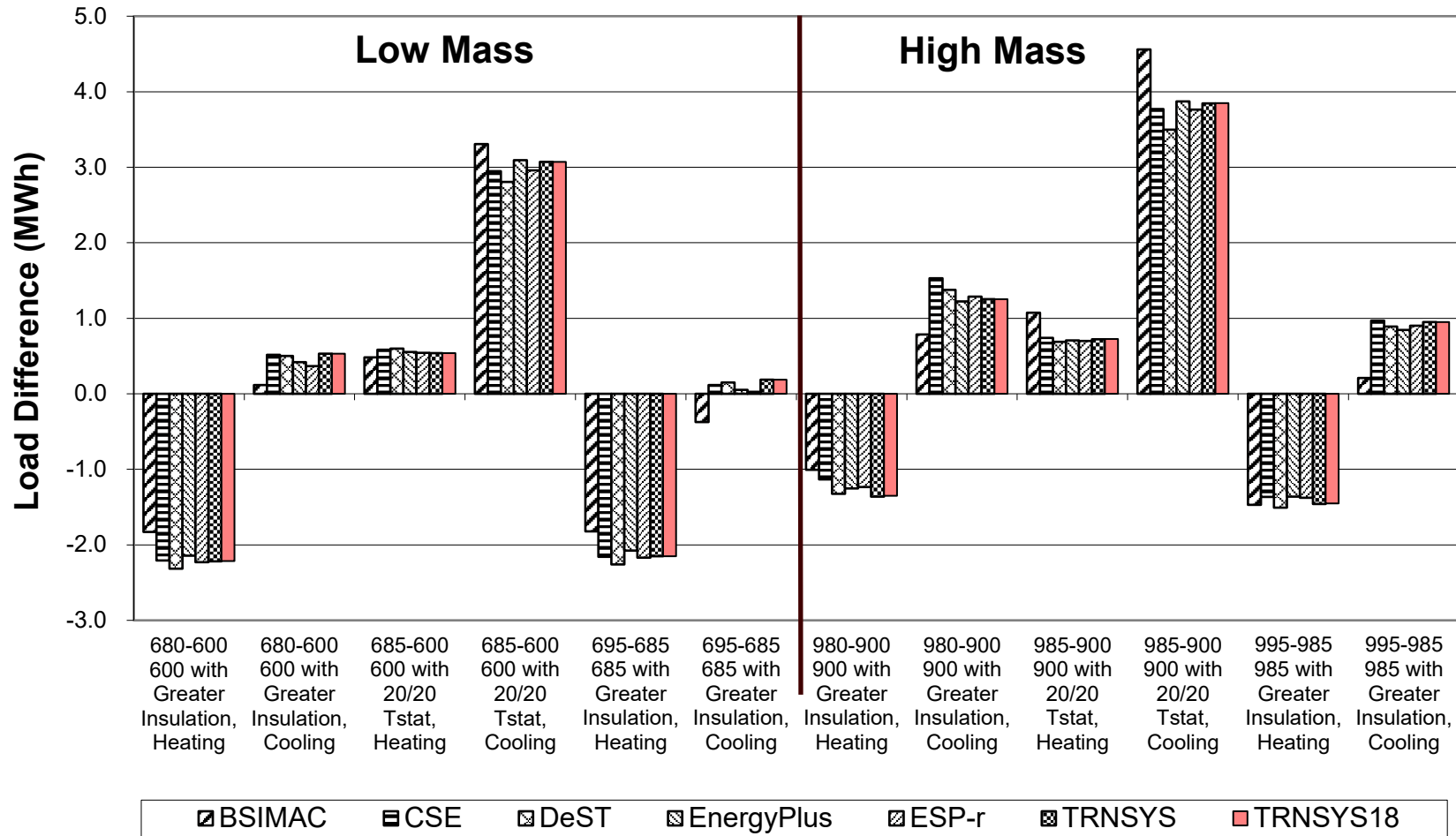


**Figure B8-28. Basic:  
Window Types (Delta)  
Peak Heating and Sensible Cooling**



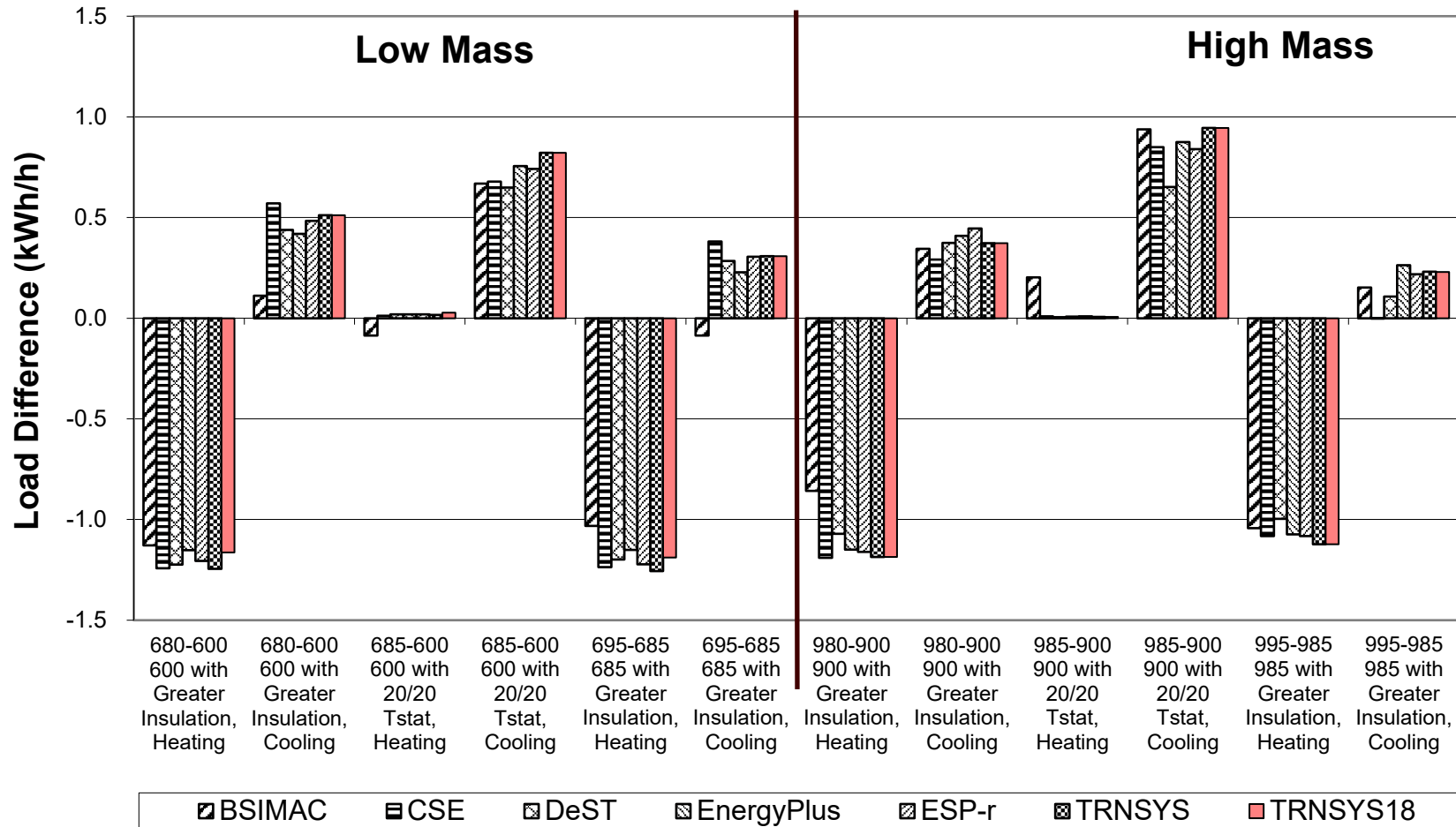
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-29. Basic:  
Insulation (Delta)  
Annual Heating and Sensible Cooling**



ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-30. Basic:  
Insulation (Delta)  
Peak Heating and Sensible Cooling**

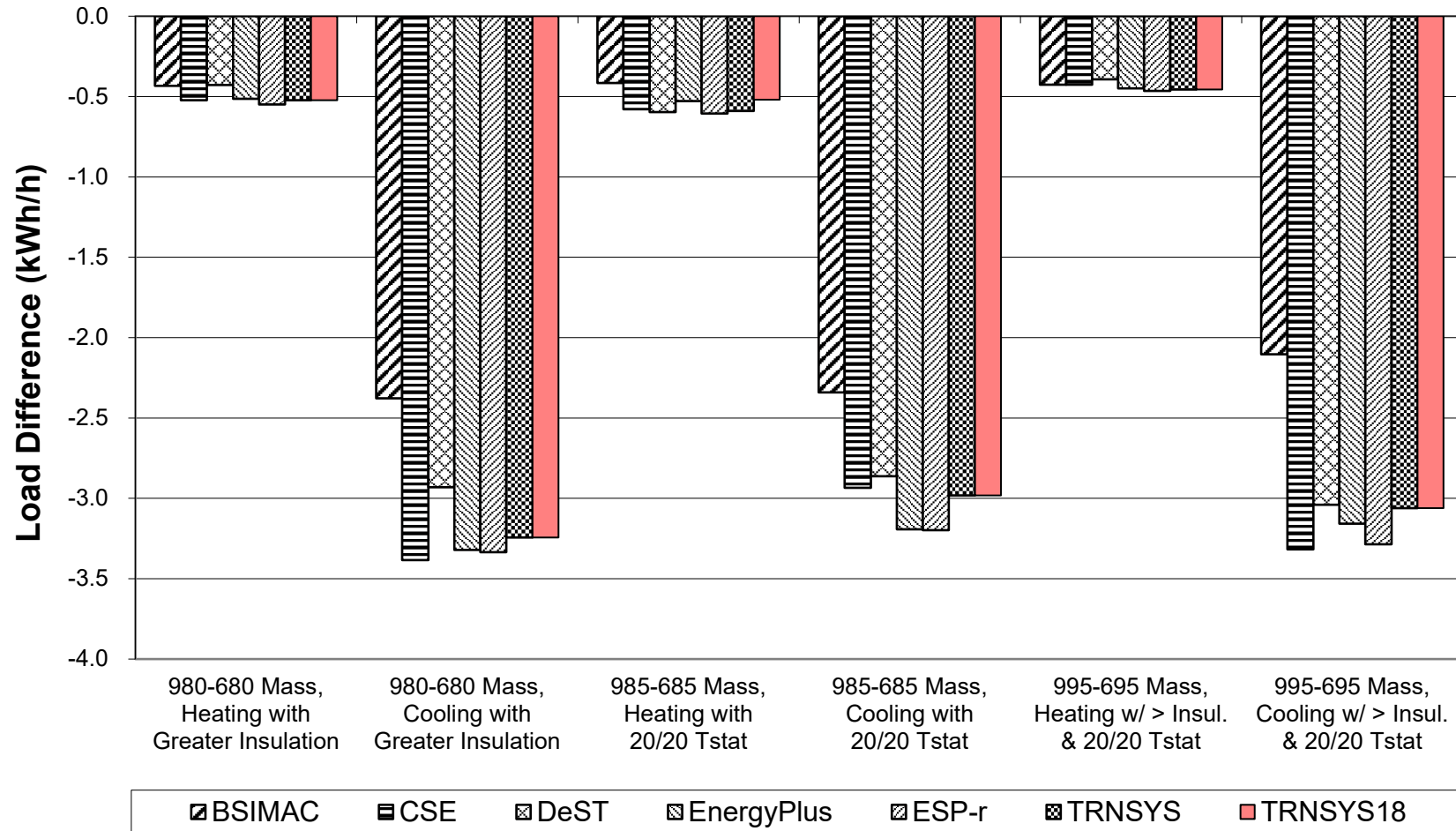




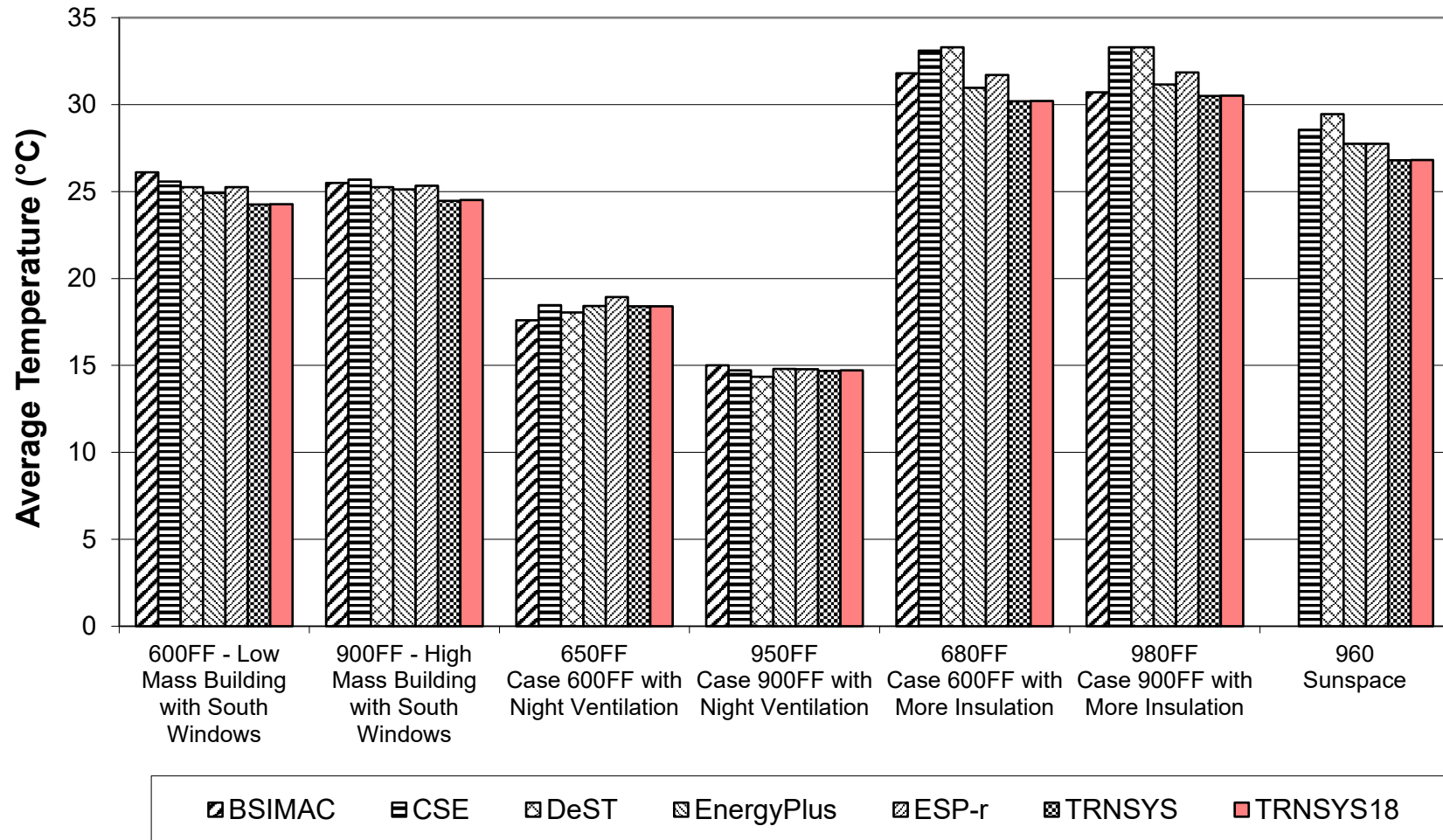


ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

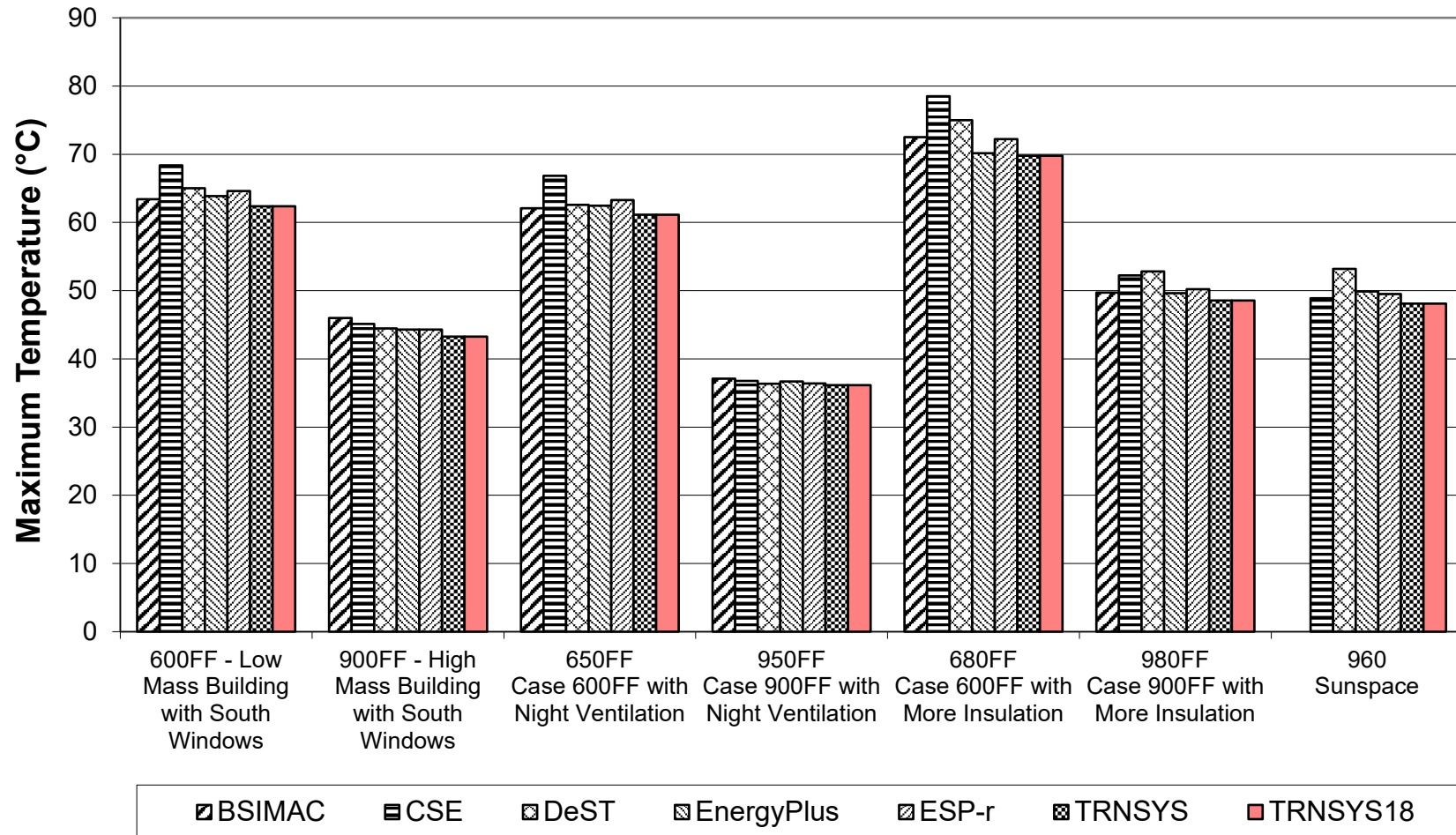
**Figure B8-32. Basic:  
Insulation, Mass Effect (Delta)  
Peak Heating and Sensible Cooling**



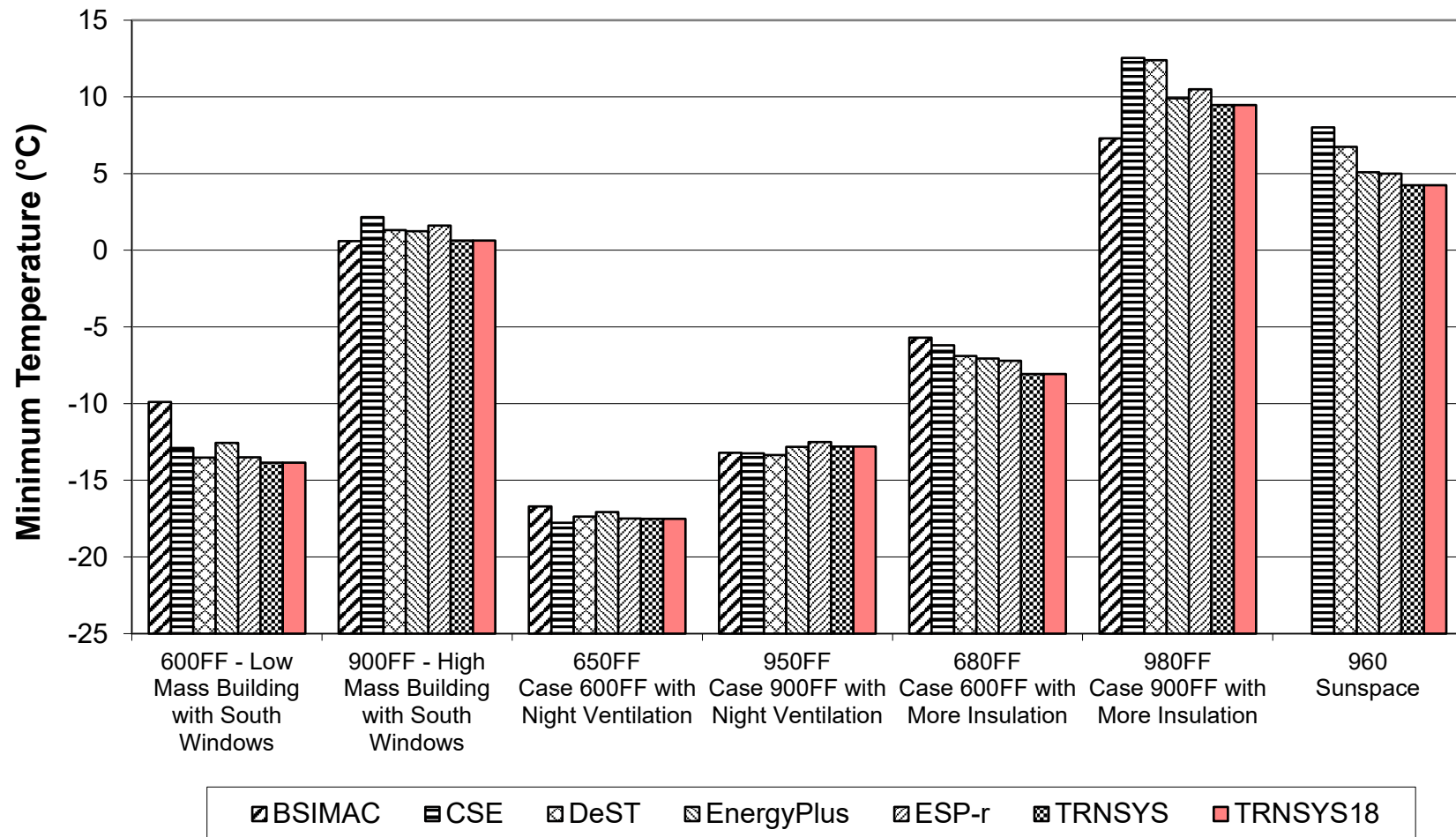
**Figure B8-33. Basic:  
Average Hourly Annual Temperature  
Free-Float Cases**



**Figure B8-34. Basic:  
Maximum Hourly Annual Temperature  
Free-Float Cases**

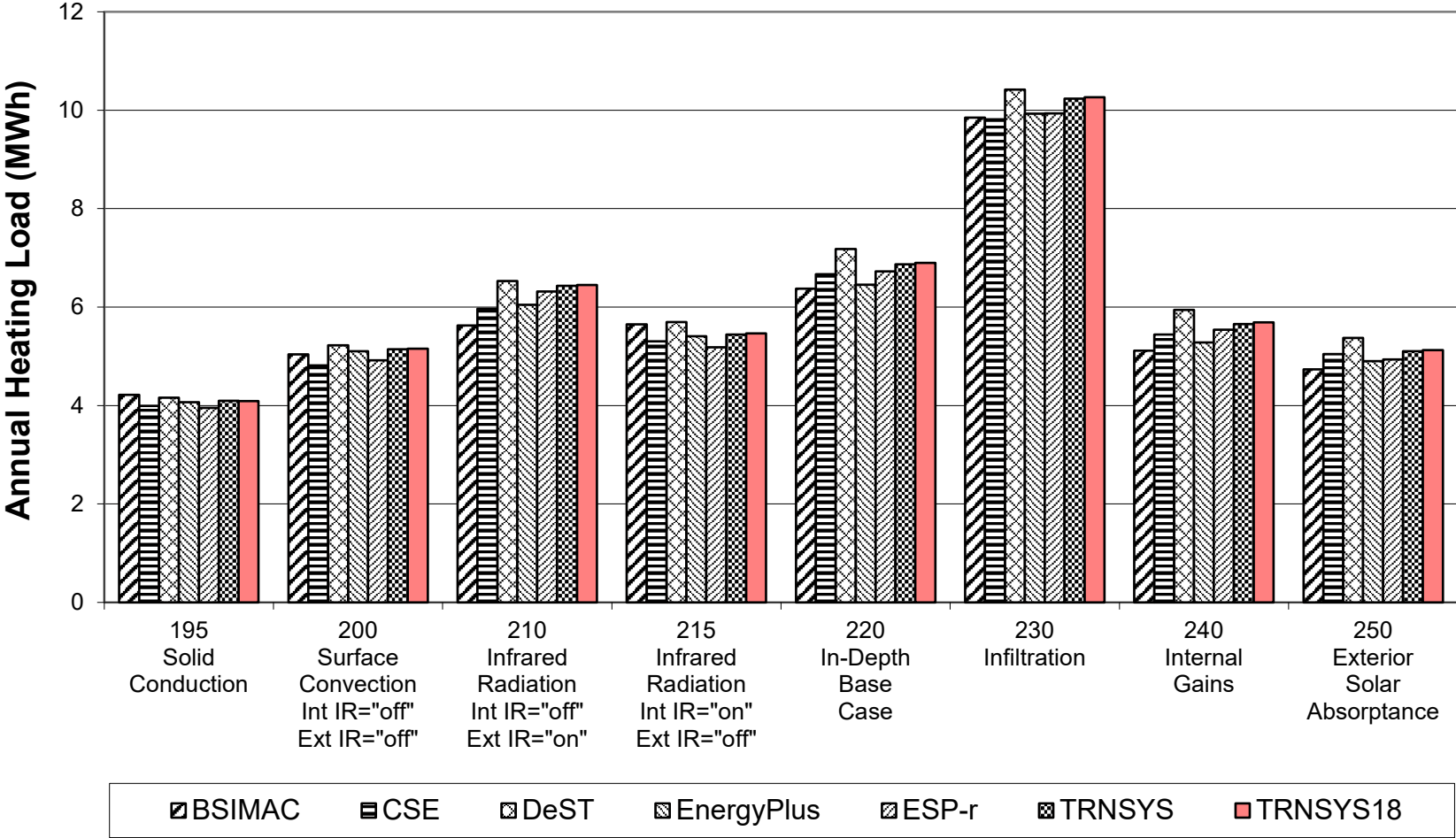


**Figure B8-35. Basic:  
Minimum Hourly Annual Temperature  
Free-Float Cases**



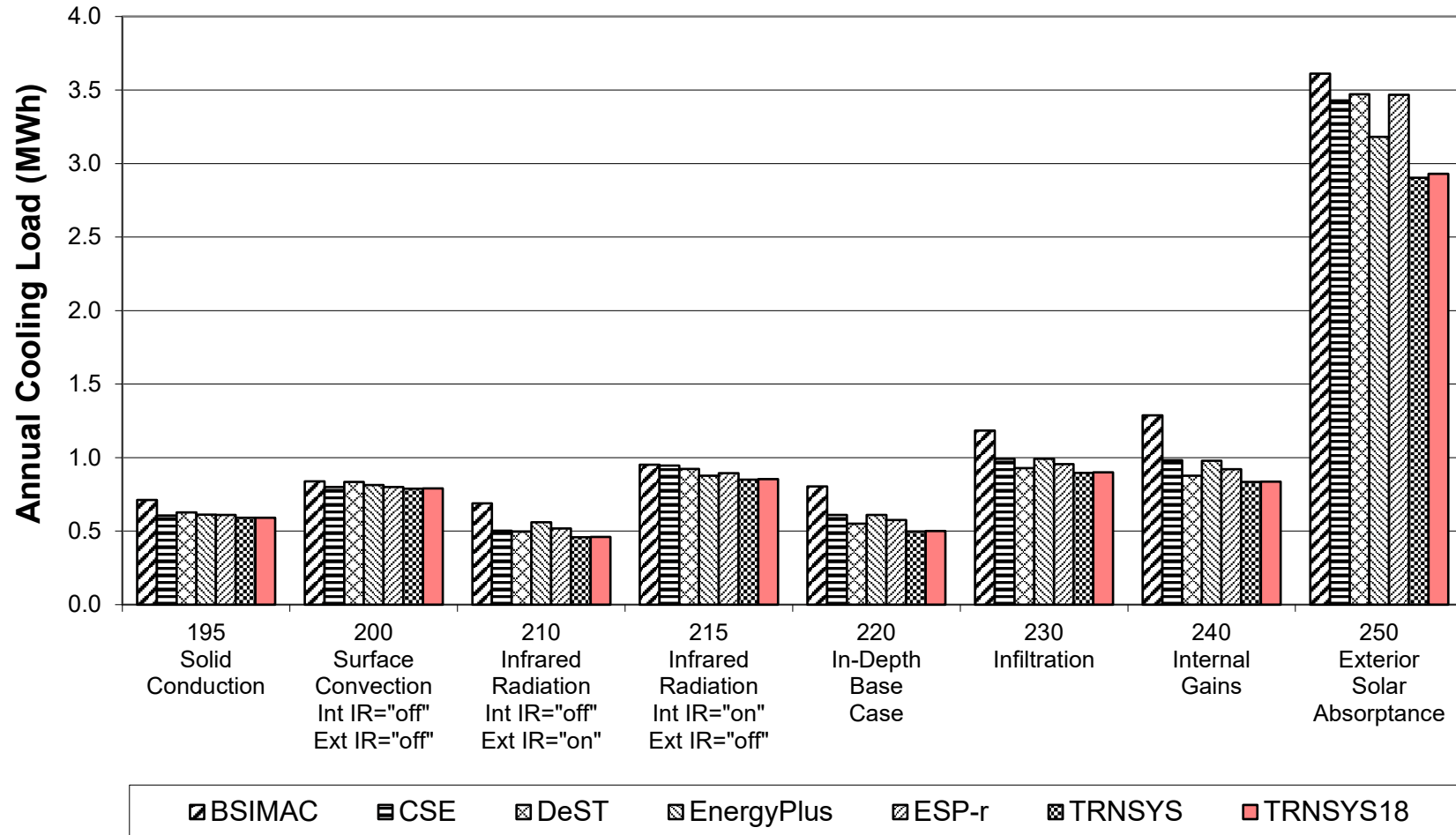
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-36. In-Depth:  
Low Mass Cases 195 to 250  
Annual Heating**

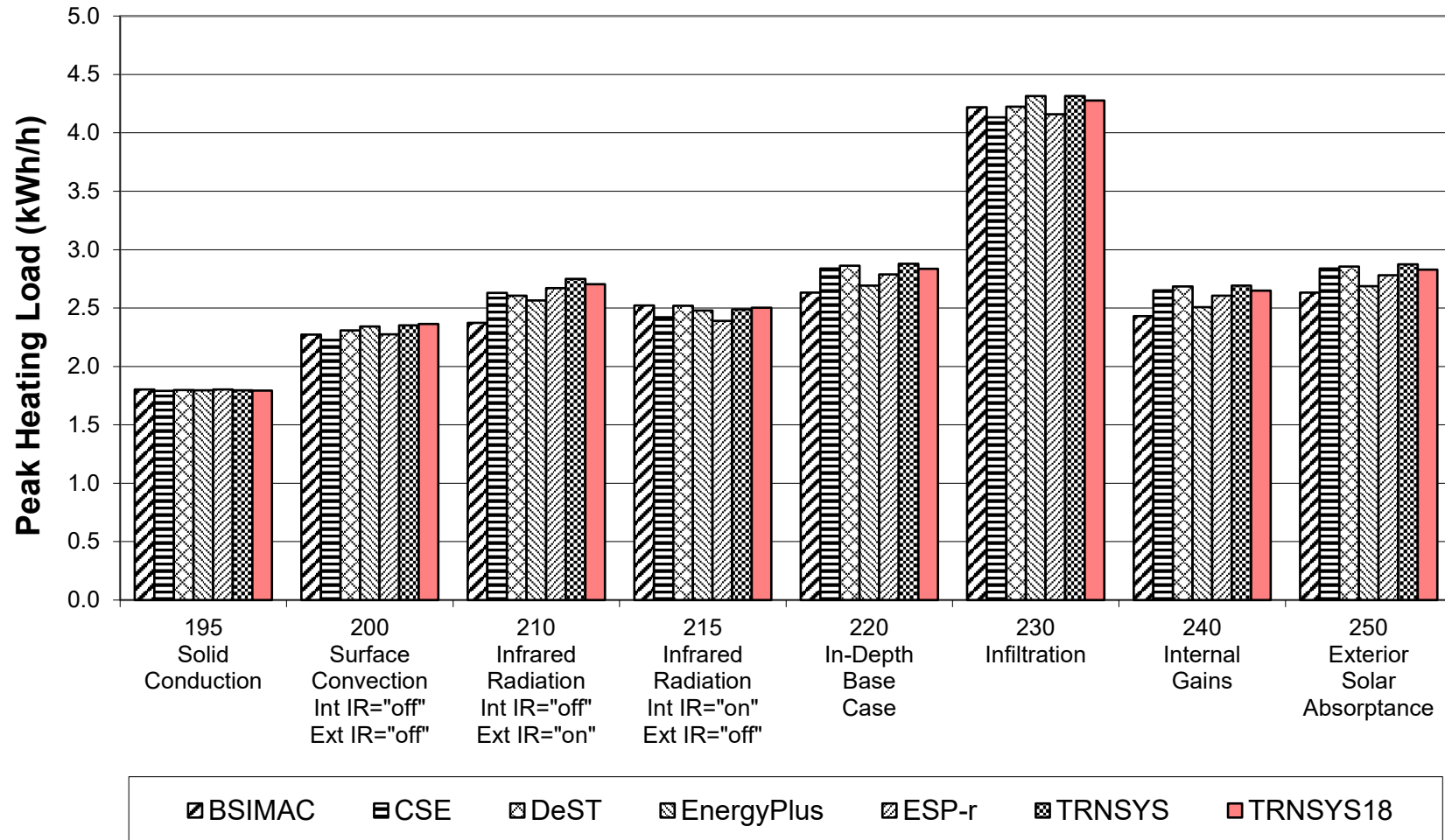


ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

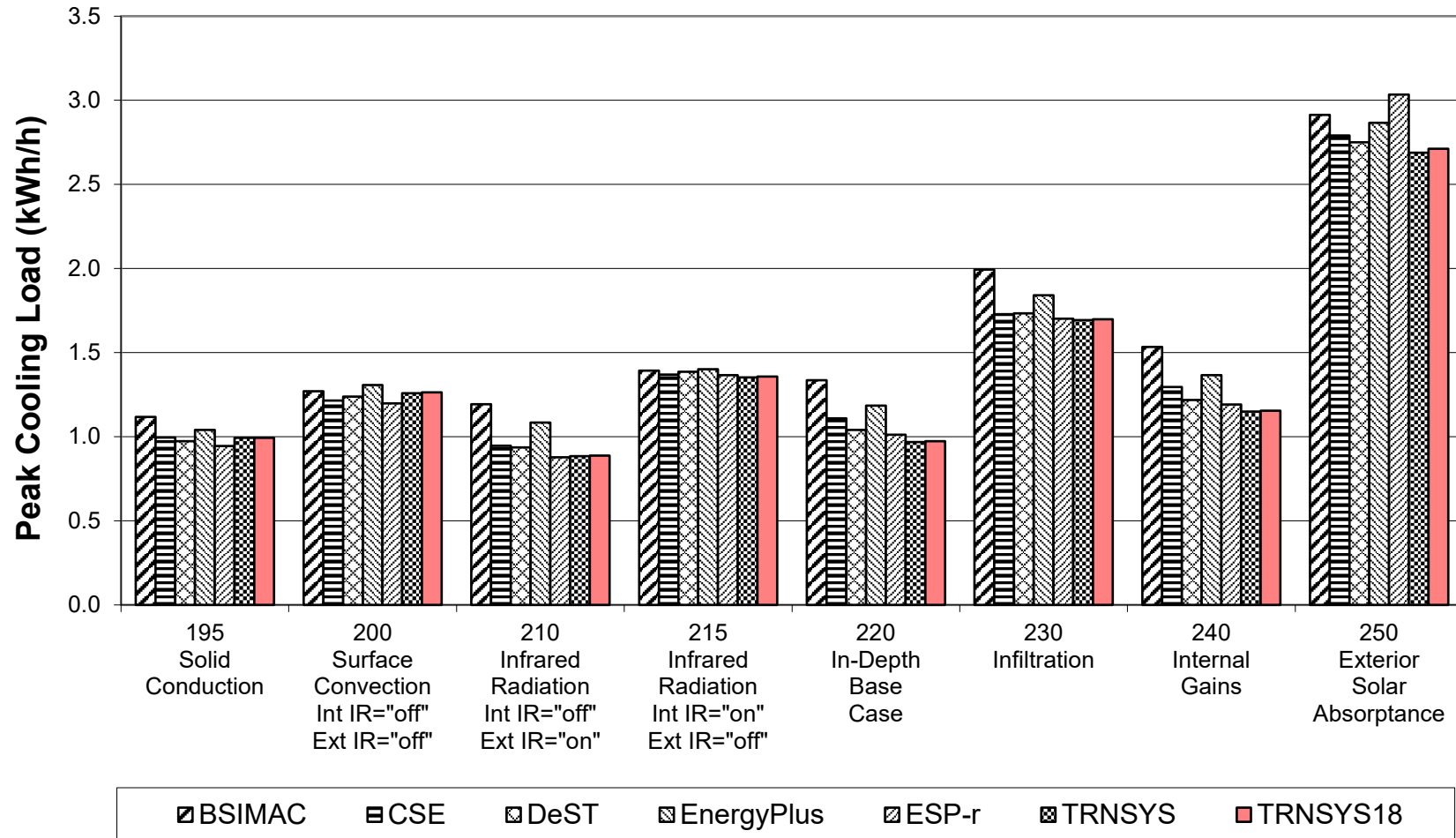
**Figure B8-37. In-Depth:  
Low Mass Cases 195 to 250  
Annual Sensible Cooling**



**Figure B8-38. In-Depth:  
Low Mass Cases 195 to 250  
Peak Heating**

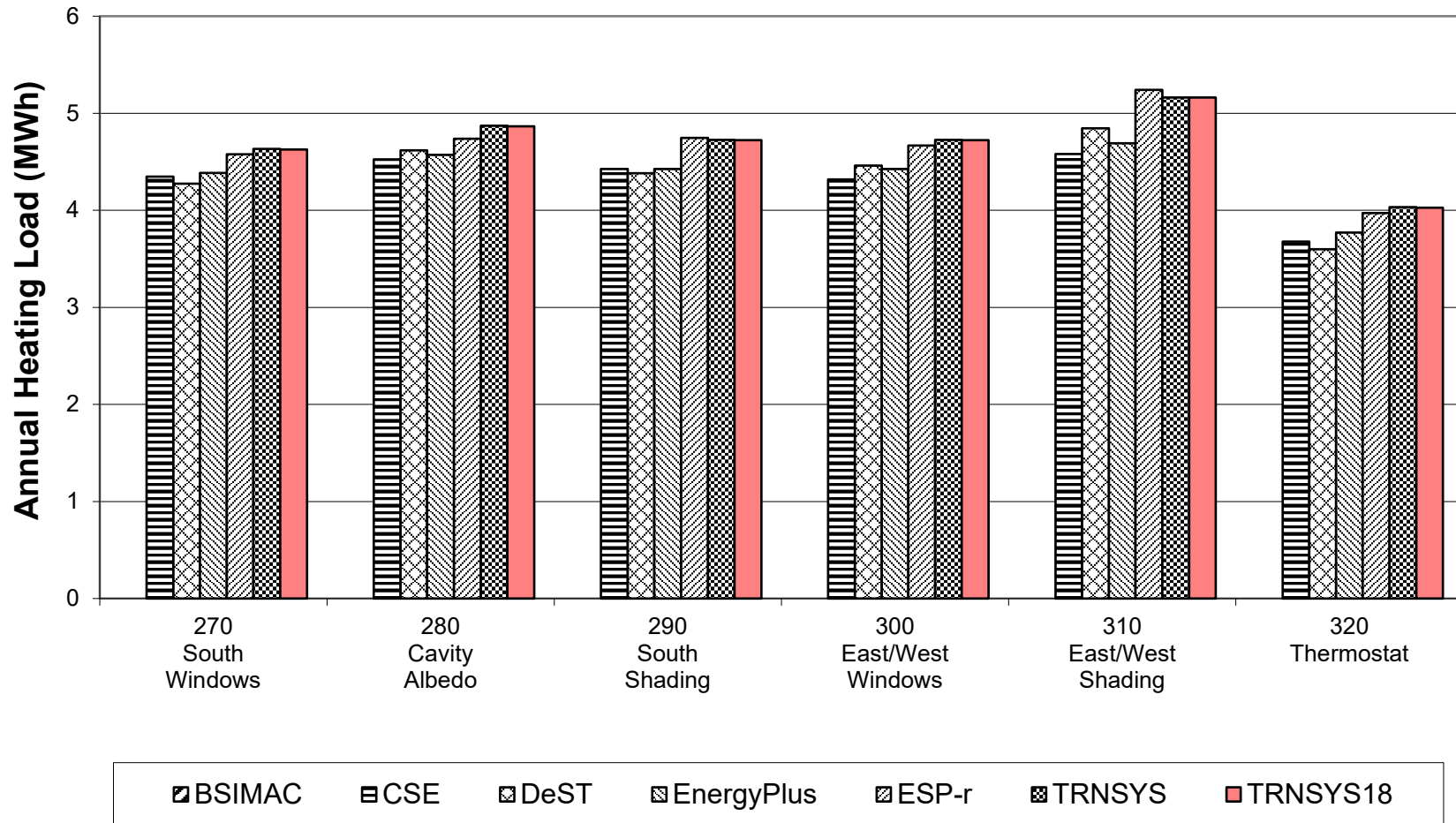


**Figure B8-39. In-Depth:  
Low Mass Cases 195 to 250  
Peak Sensible Cooling**



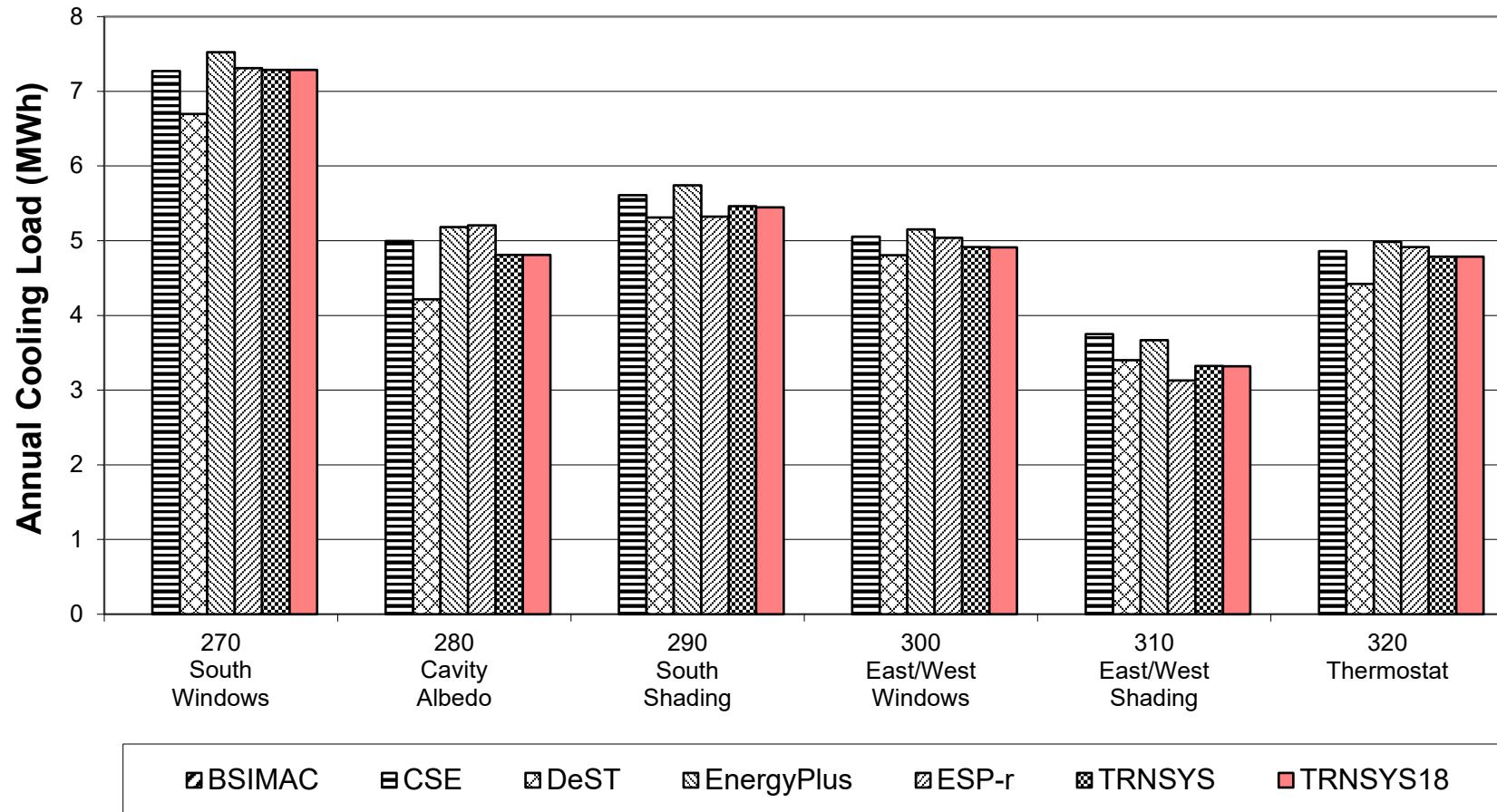


**Figure B8-40. In-Depth:  
Low Mass Cases 270 to 320  
Annual Heating**

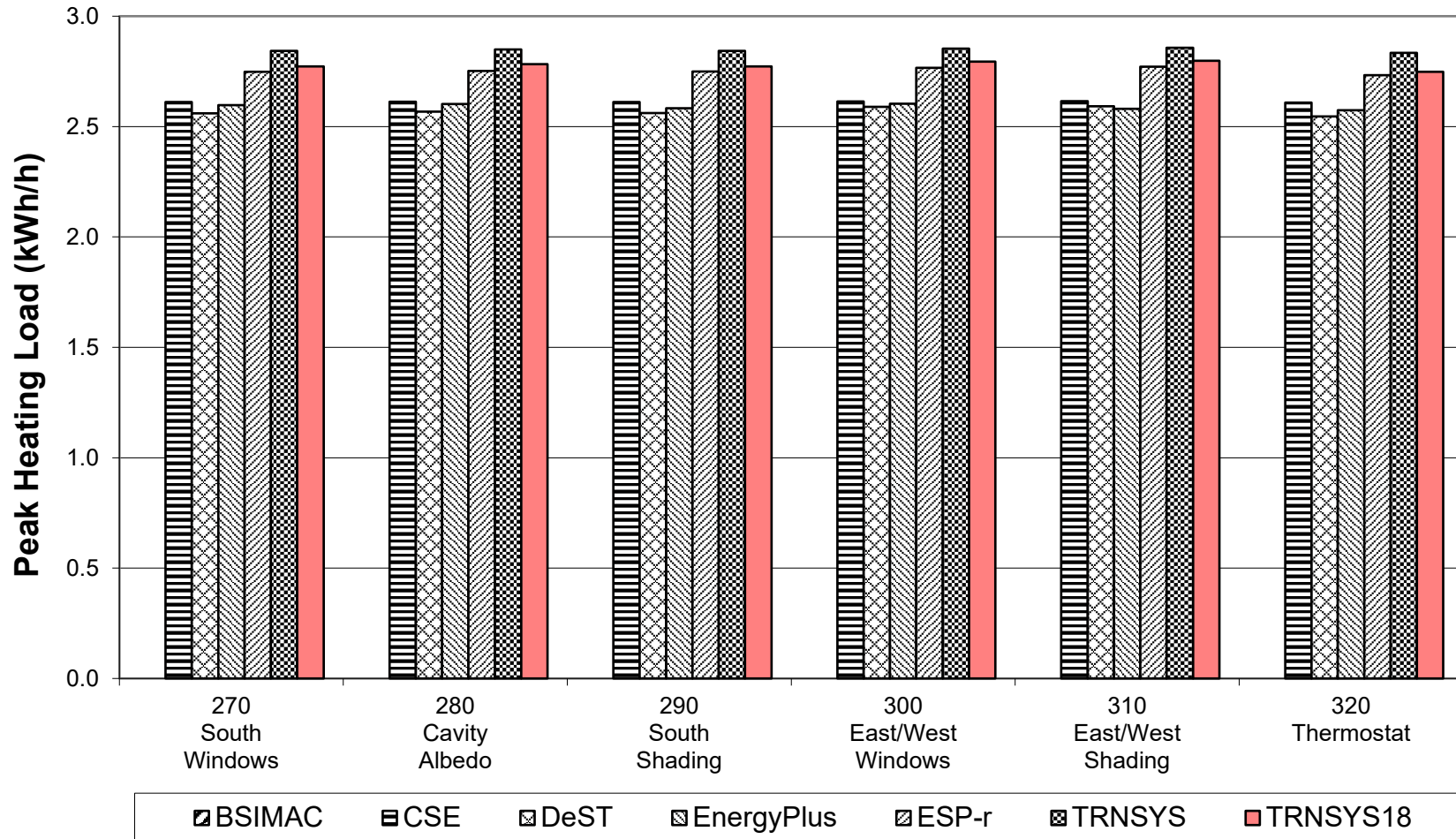


ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

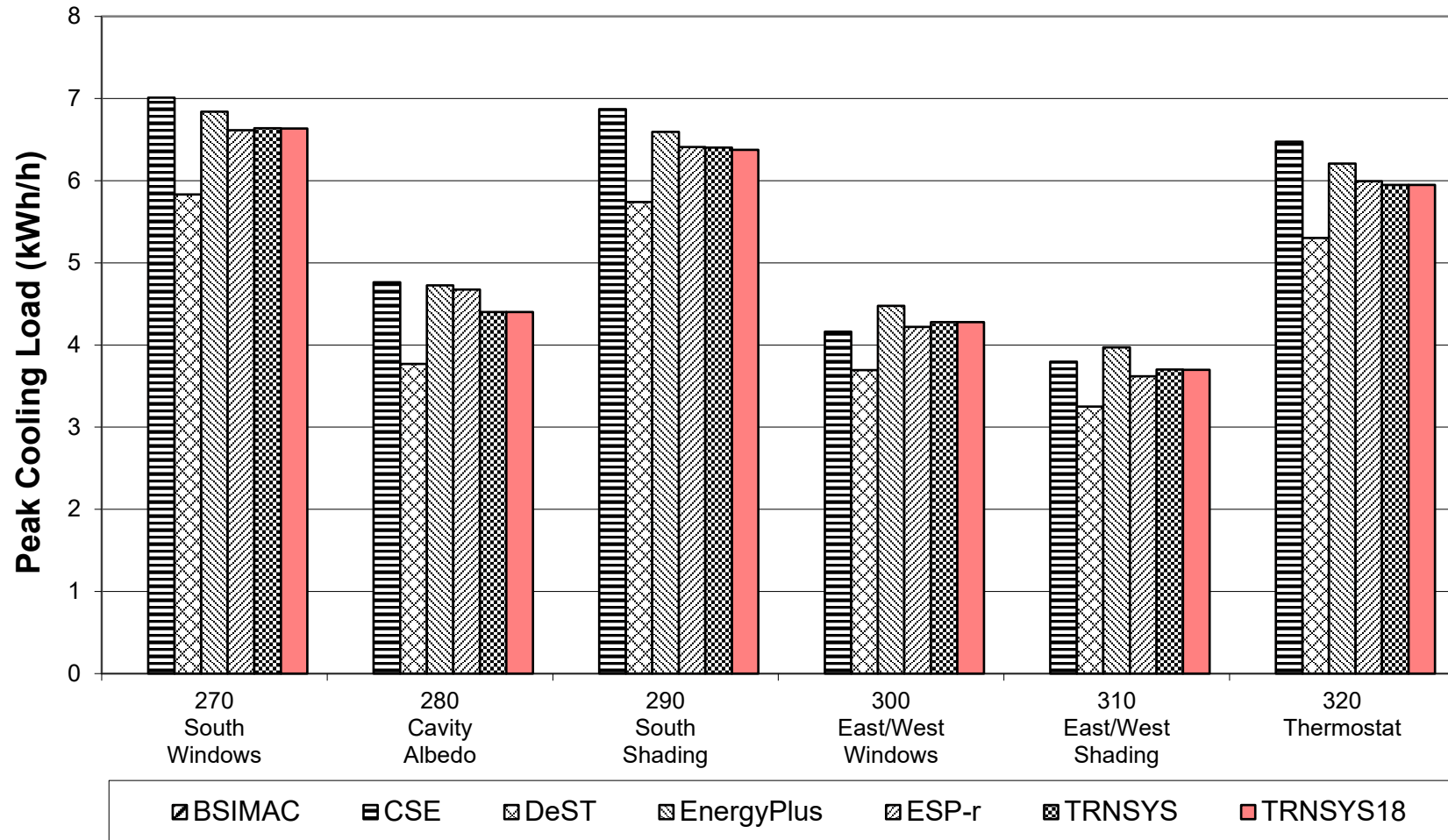
**Figure B8-41. In-Depth:  
Low Mass Cases 270 to 320  
Annual Sensible Cooling**



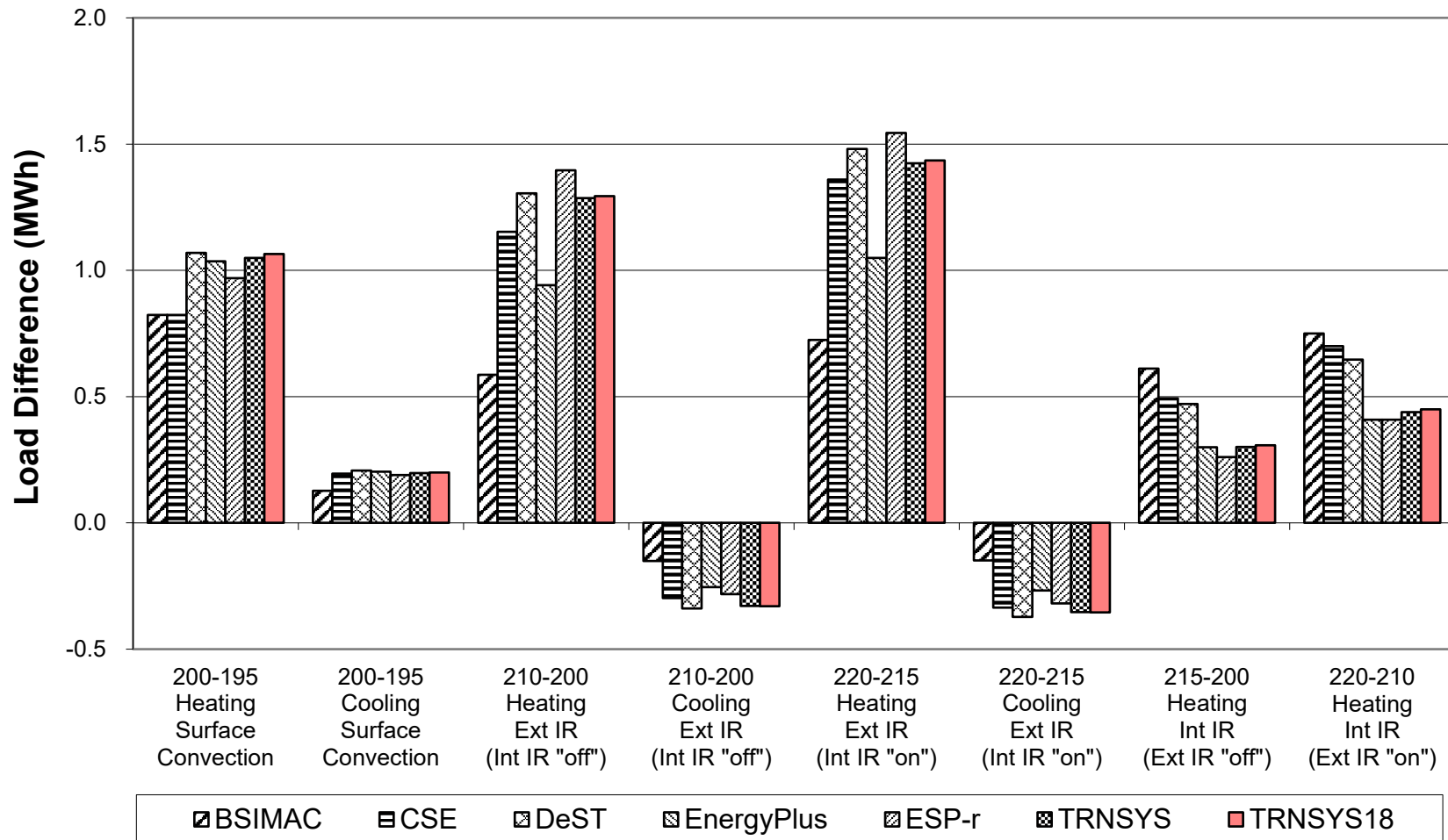
**Figure B8-42. In-Depth:  
Low Mass Cases 270 to 320  
Peak Heating**



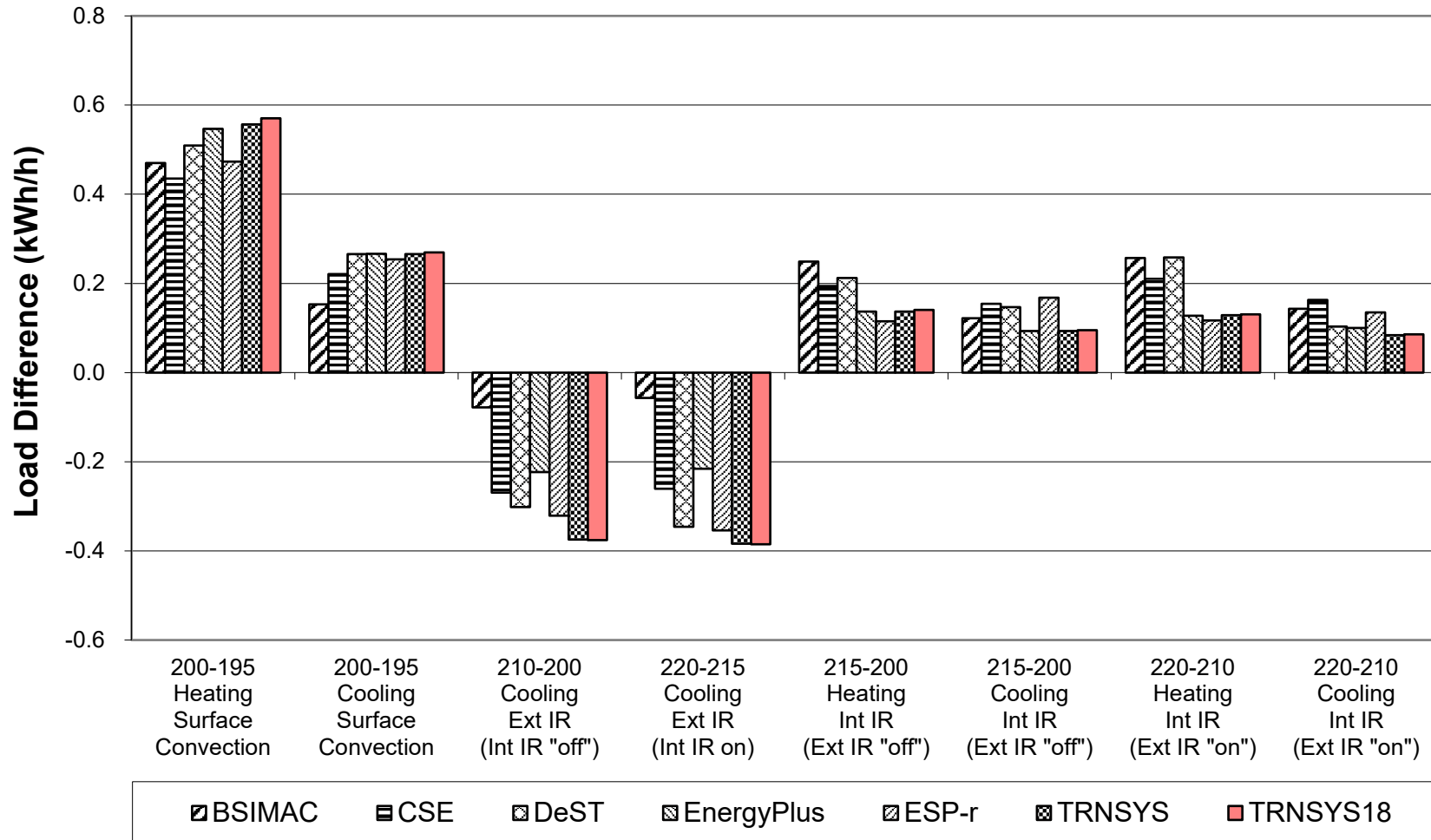
**Figure B8-43. In-Depth:  
Low Mass Cases 270 to 320  
Peak Sensible Cooling**



**Figure B8-44. In-Depth:  
Cases 195 to 220 (Delta)  
Annual Heating and Sensible Cooling**

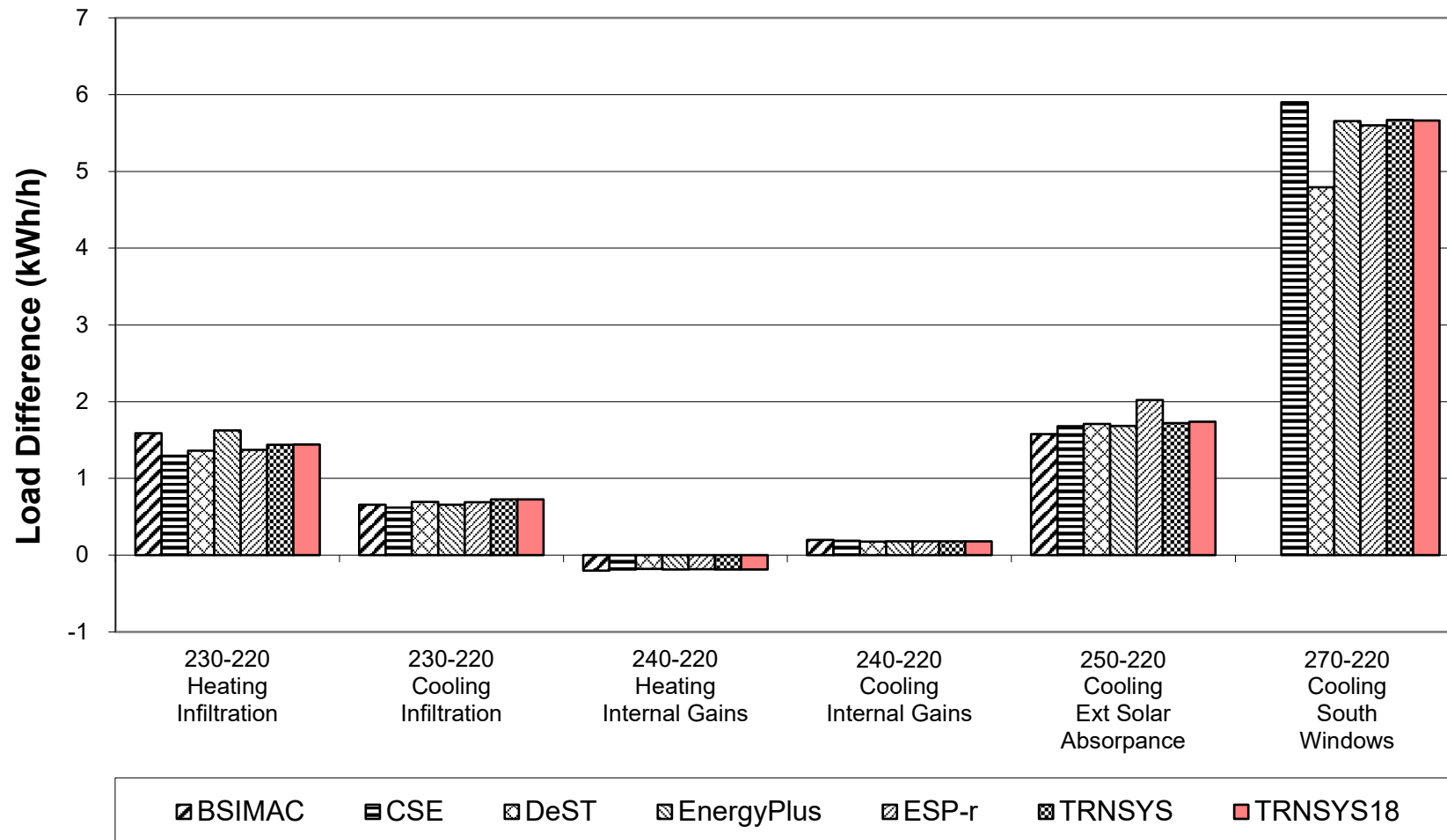


**Figure B8-45. In-Depth:  
Cases 195 to 220 (Delta)  
Peak Heating and Sensible Cooling**





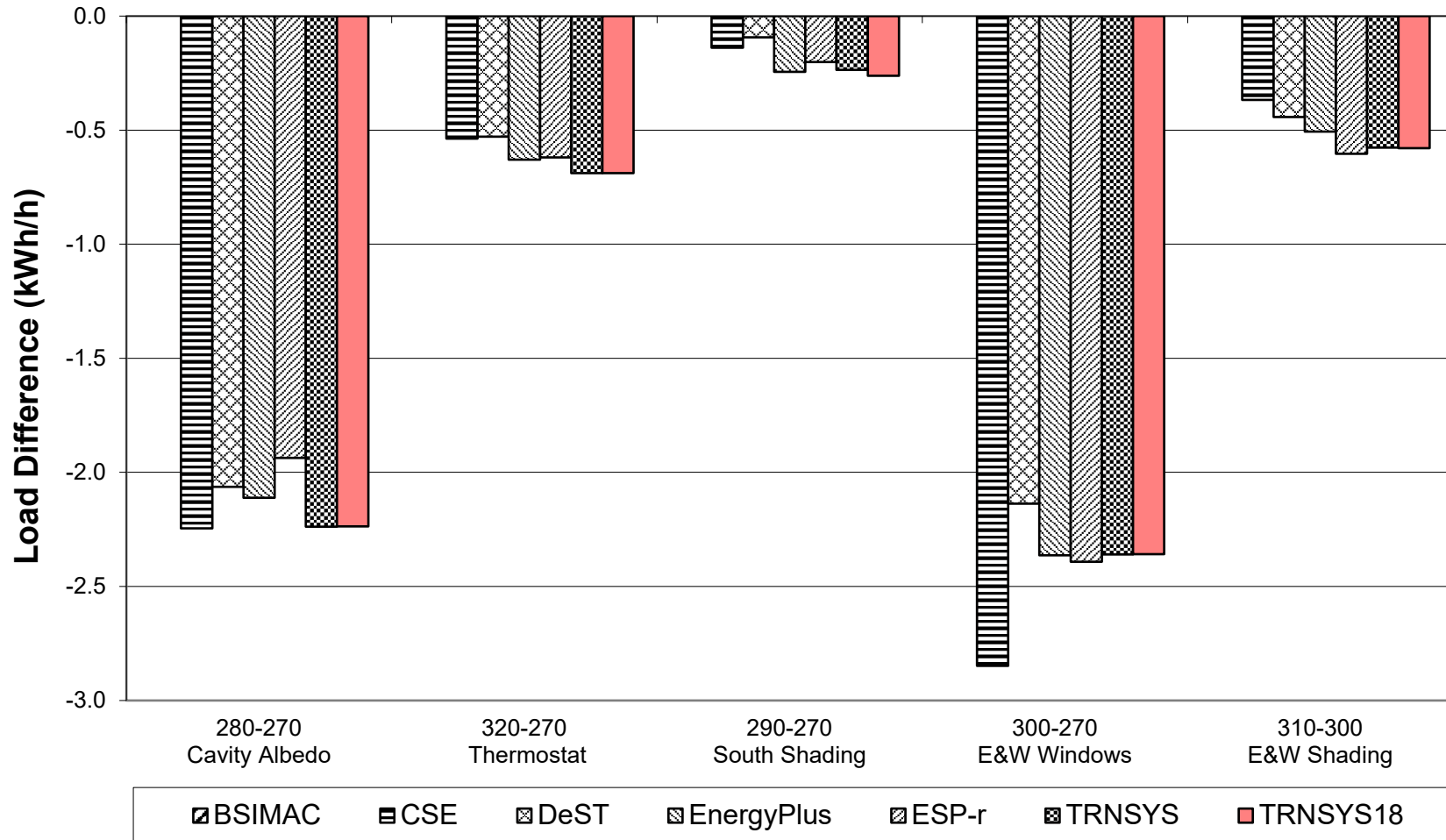
**Figure B8-47. In-Depth:  
Cases 220 to 270 (Delta)  
Peak Heating and Sensible Cooling**





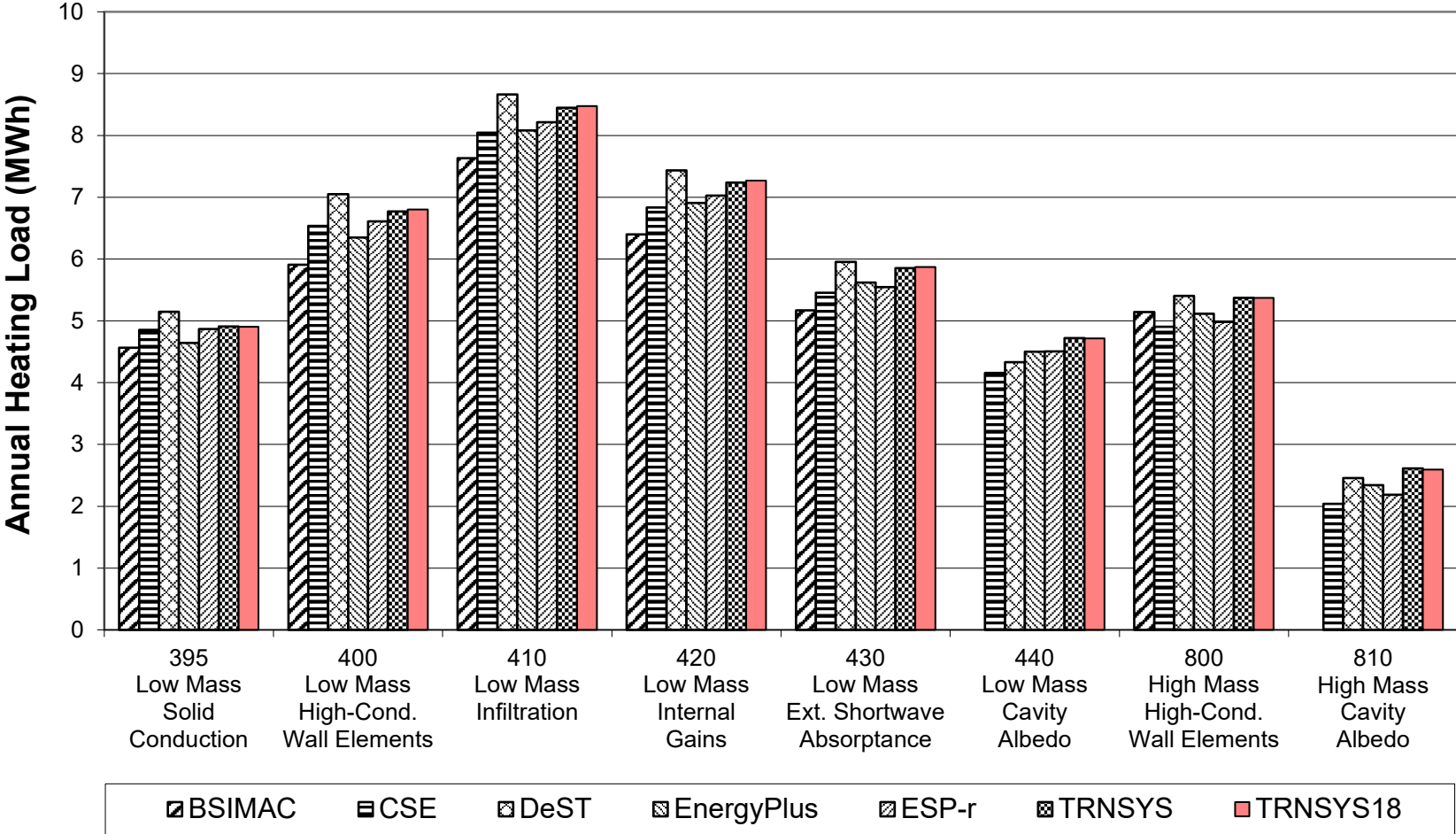


**Figure B8-49. In-Depth:  
Cases 270 to 320 (Delta)  
Peak Sensible Cooling**



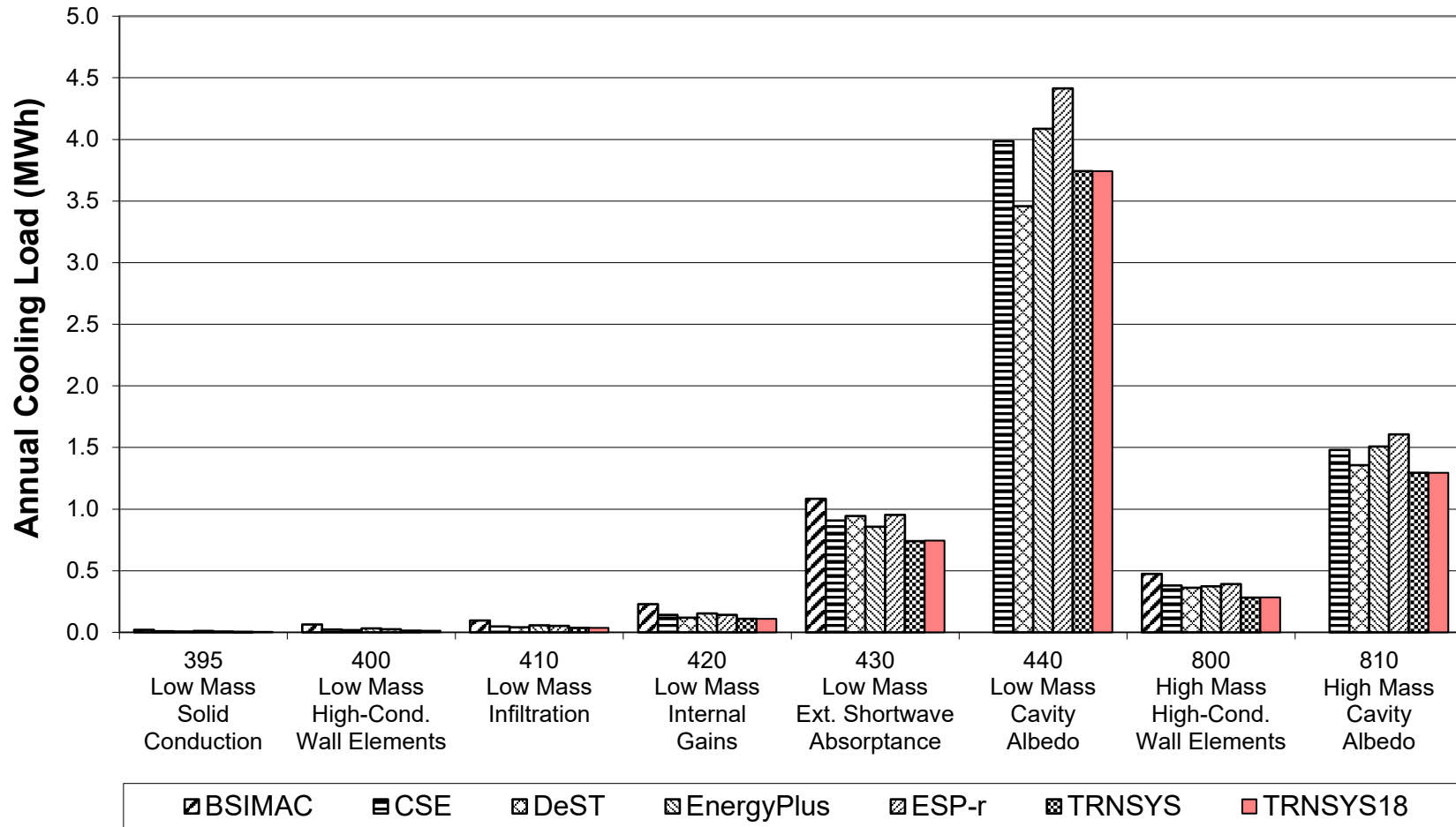
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-50. In-Depth:  
Cases 395 to 440, 800, 810  
Annual Heating**

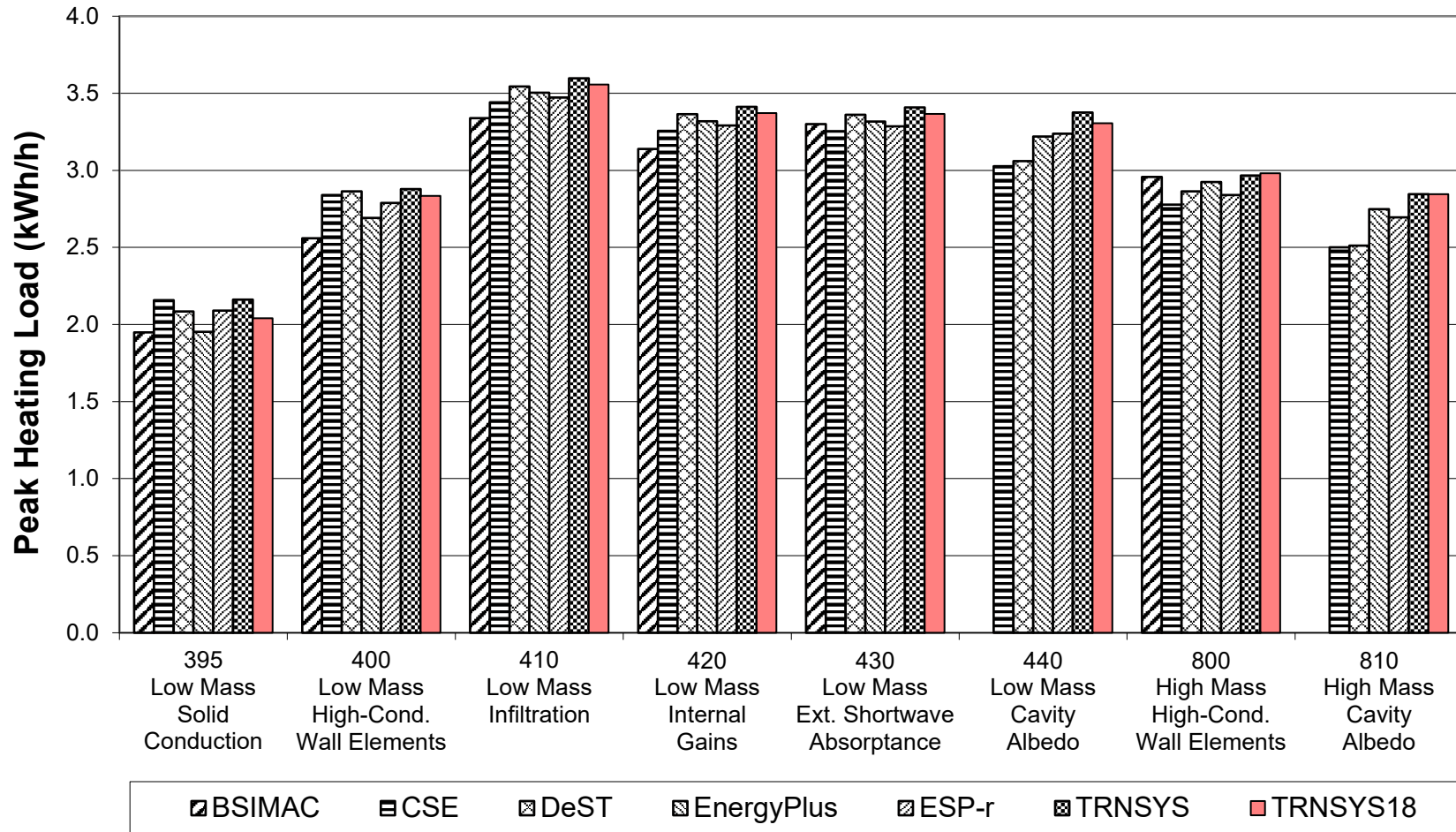


ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-51. In-Depth:  
Cases 395 to 440, 800, 810  
Annual Sensible Cooling**

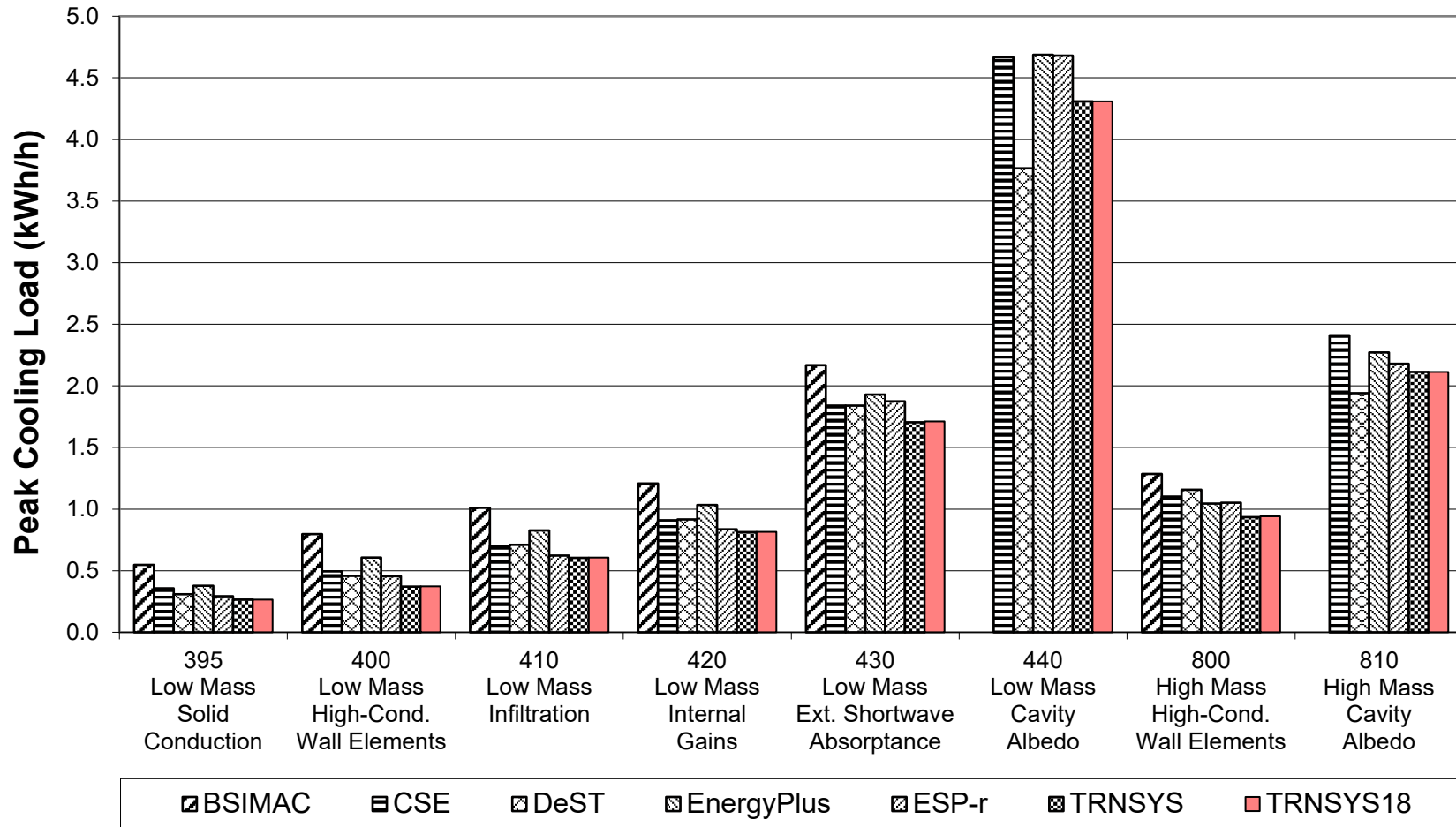


**Figure B8-52. In-Depth:  
Cases 395 to 440, 800, 810  
Peak Heating**



ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-53. In-Depth:  
Cases 395 to 440, 800, 810  
Peak Sensible Cooling**

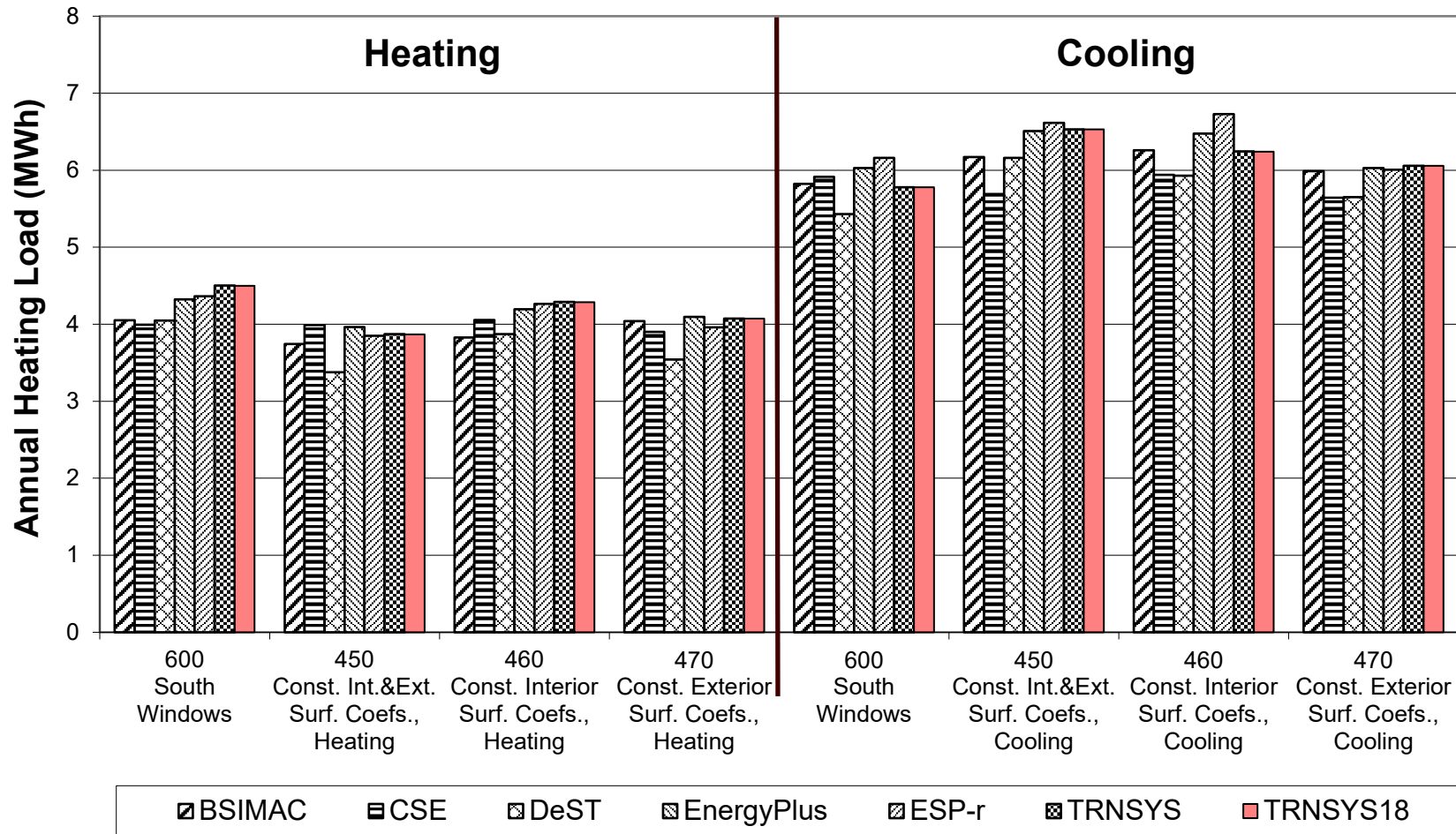




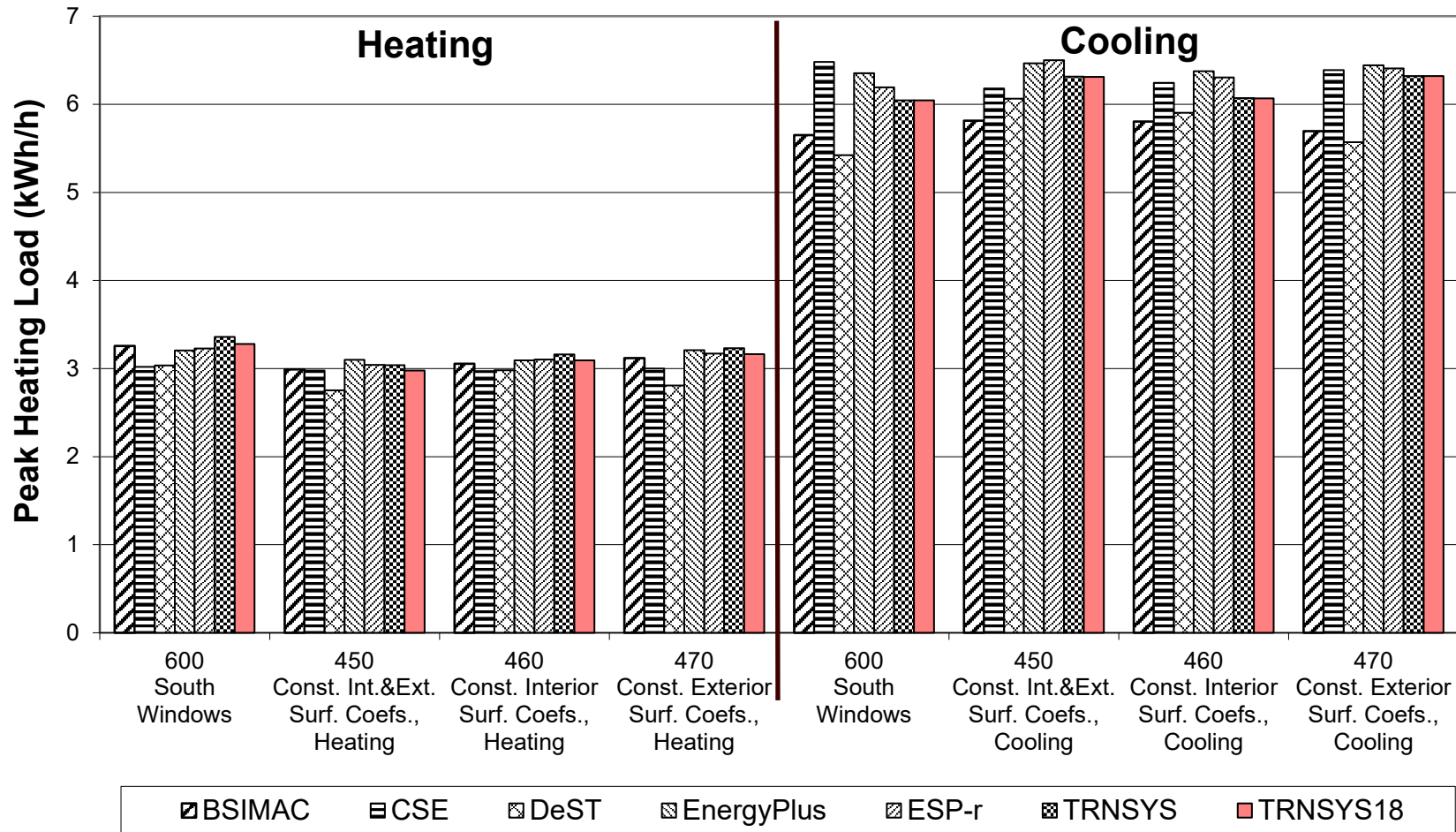




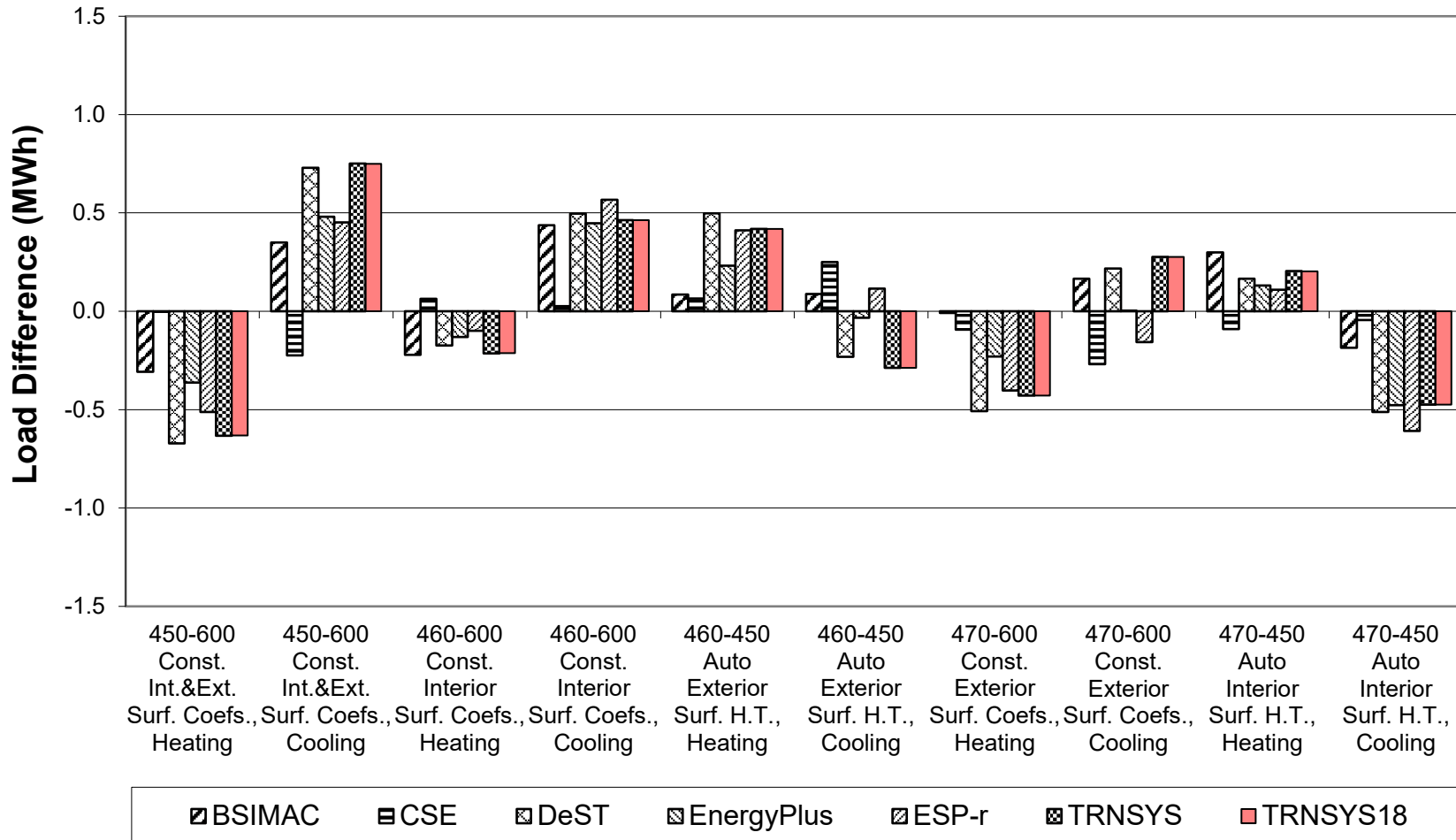
**Figure B8-56. In-Depth: Surface Heat Transfer  
Cases 600, 450, 460, 470  
Annual Heating and Sensible Cooling**



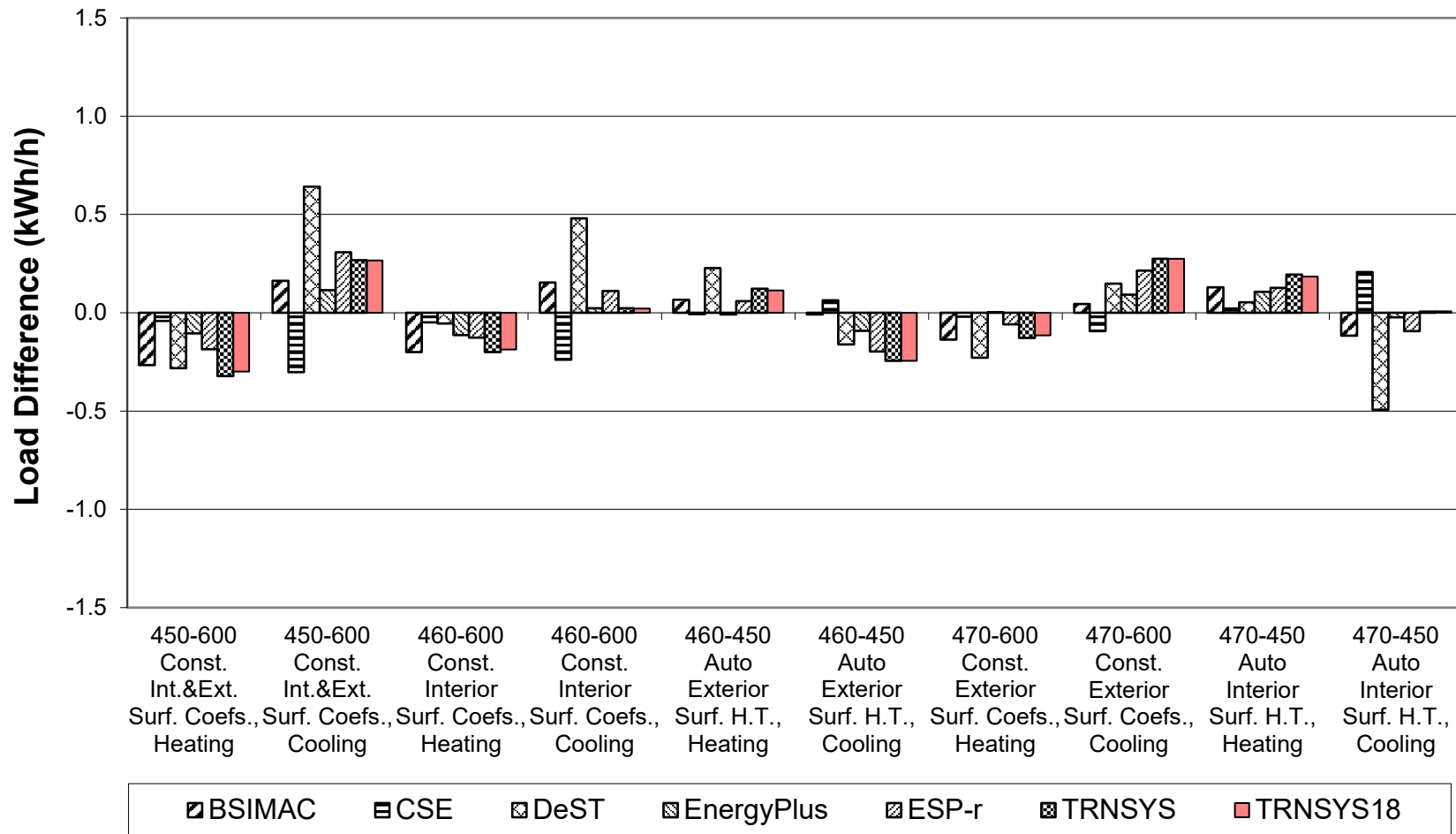
**Figure B8-57. In-Depth: Surface Heat Transfer  
Cases 600, 450, 460, 470  
Peak Heating and Sensible Cooling**



**Figure B8-58. In-Depth: Surface Heat Transfer  
Cases 450 to 600 (Delta)  
Annual Heating and Sensible Cooling**

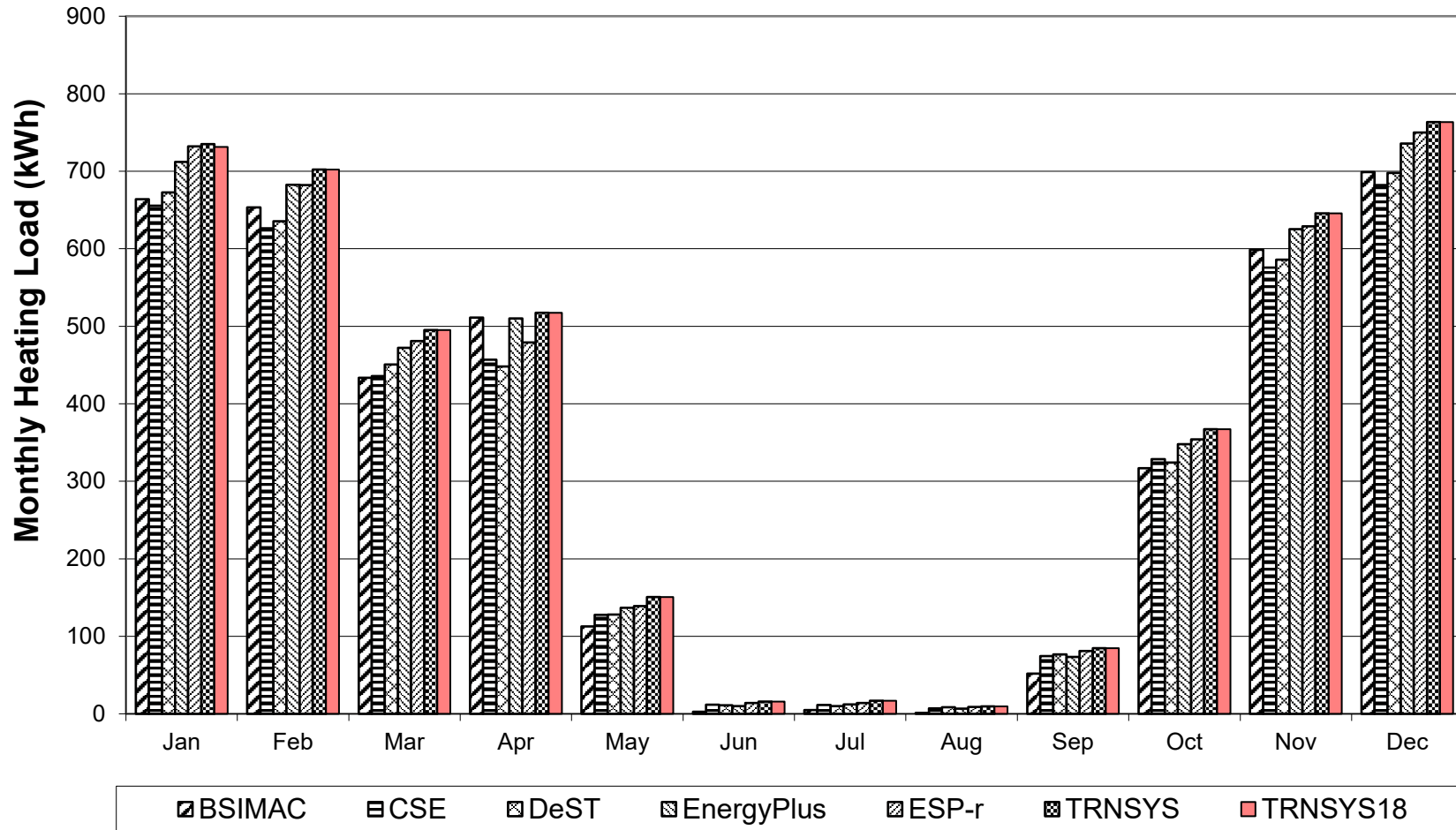


**Figure B8-59. In-Depth: Surface Heat Transfer  
Cases 450 to 600 (Delta)  
Peak Heating and Sensible Cooling**



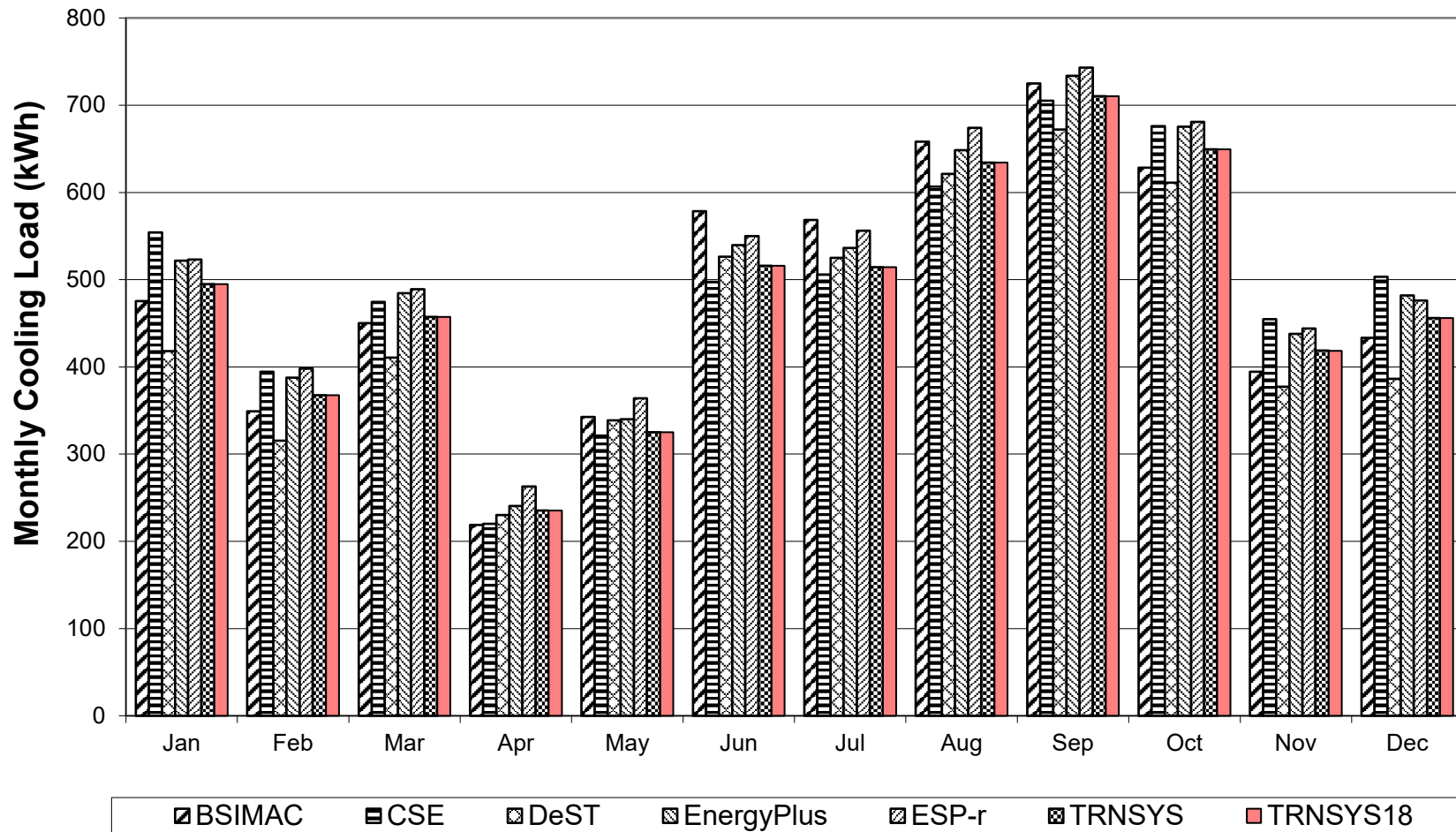
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-M1.  
Monthly Heating  
Case 600**

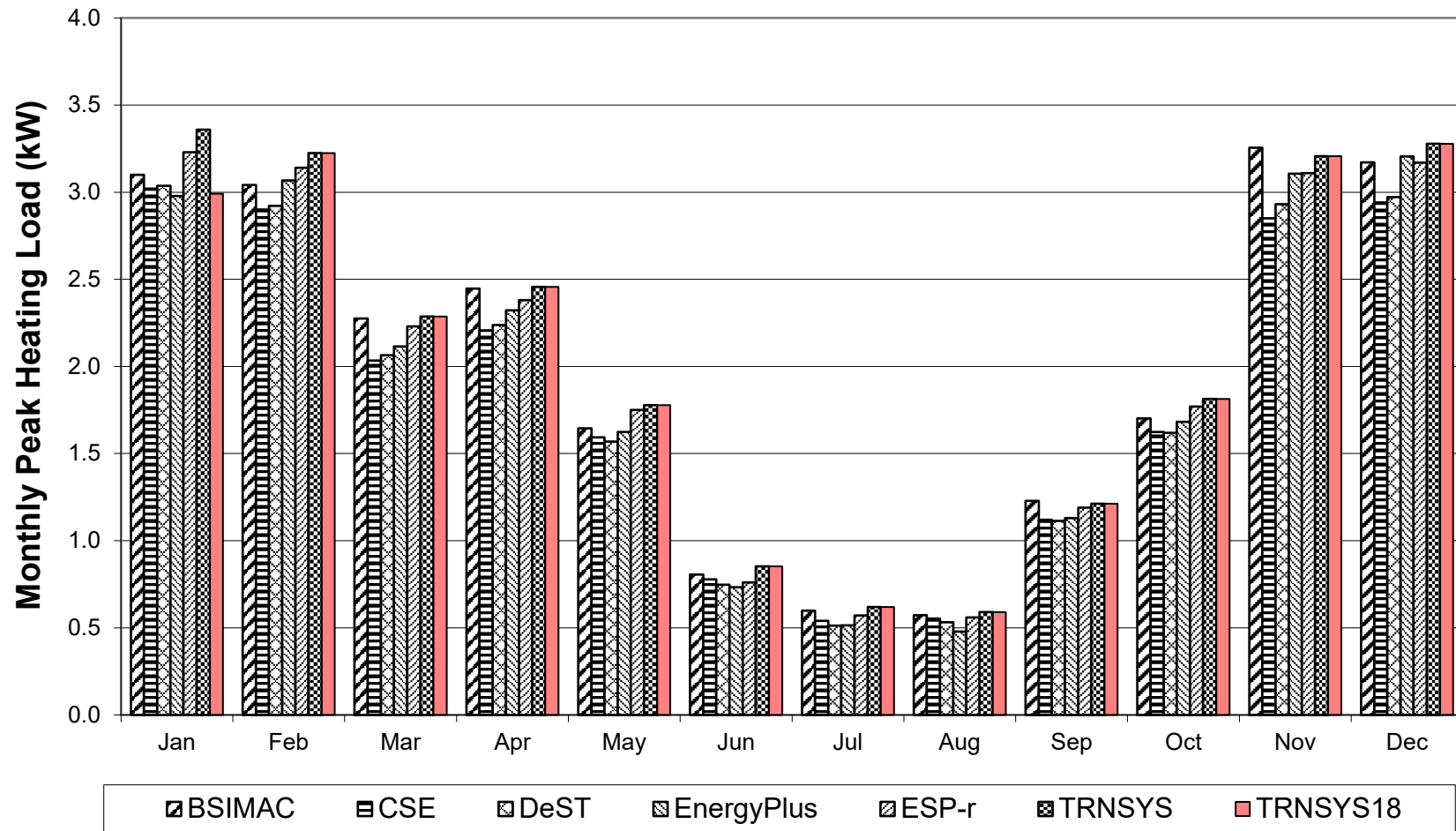


ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-M2.**  
**Monthly Sensible Cooling**  
**Case 600**

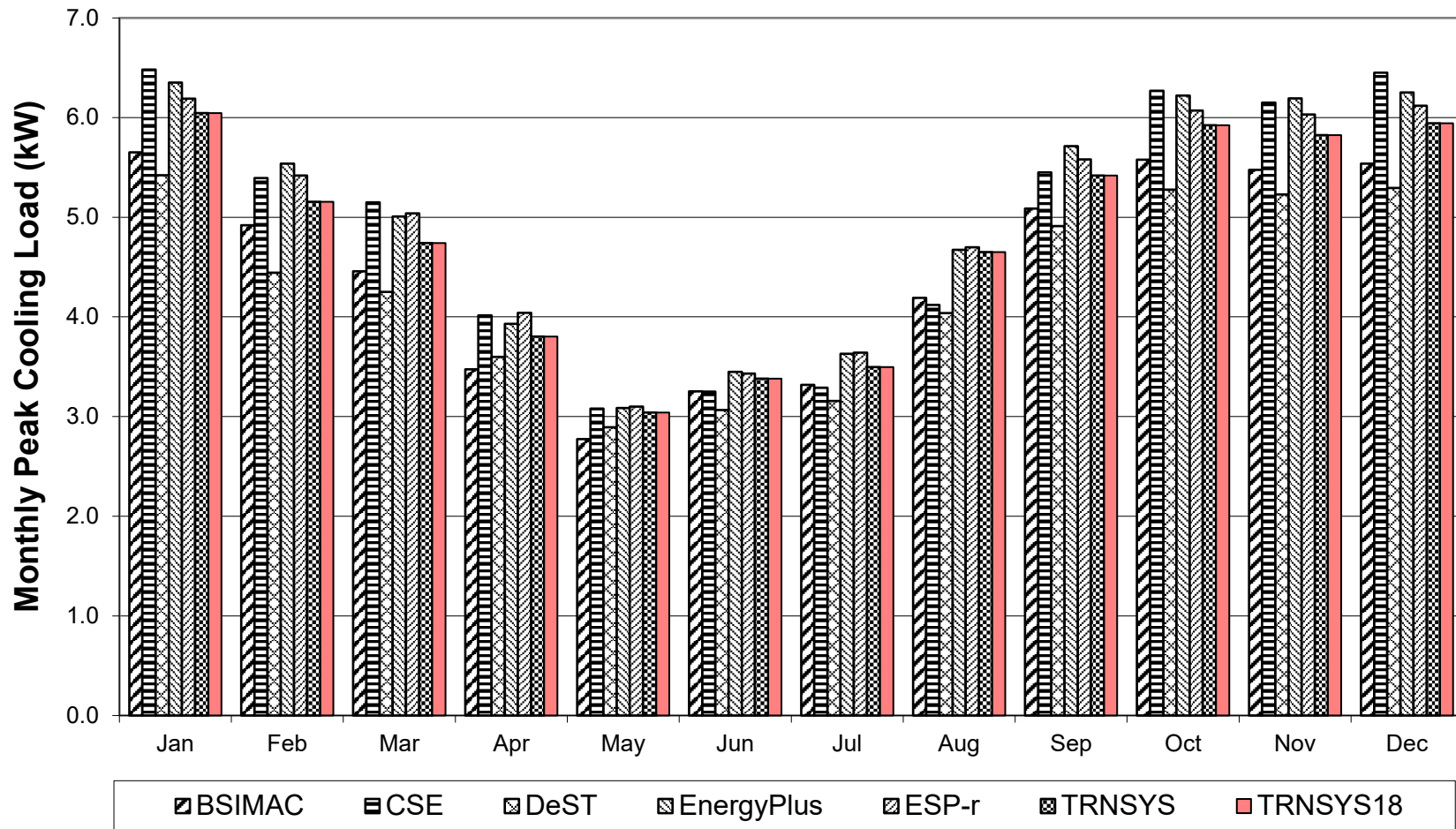


**Figure B8-M3.  
Monthly Peak Heating  
Case 600**



ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

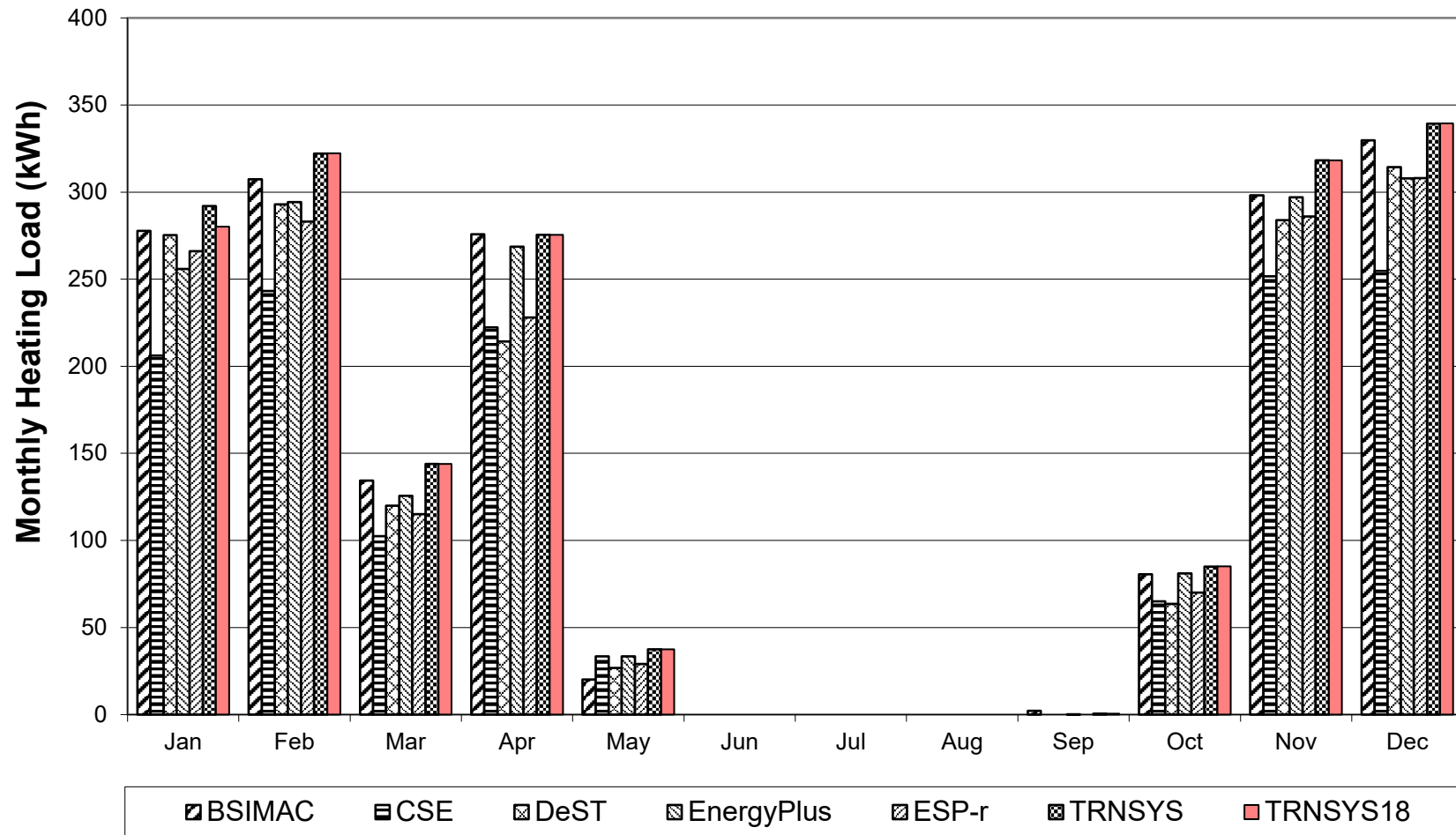
**Figure B8-M4.**  
**Monthly Peak Sensible Cooling**  
**Case 600**





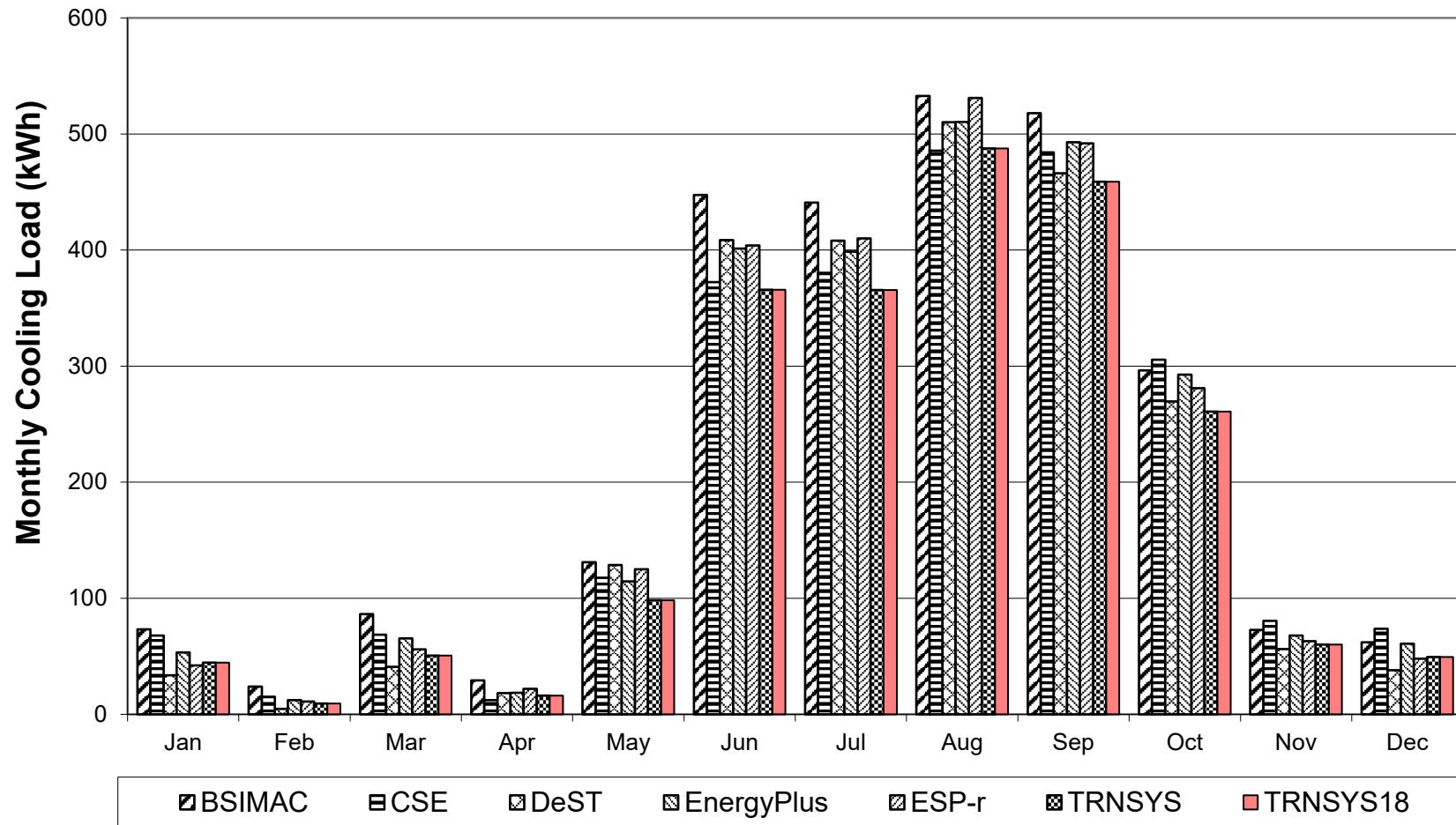
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-M5.  
Monthly Heating  
Case 900**



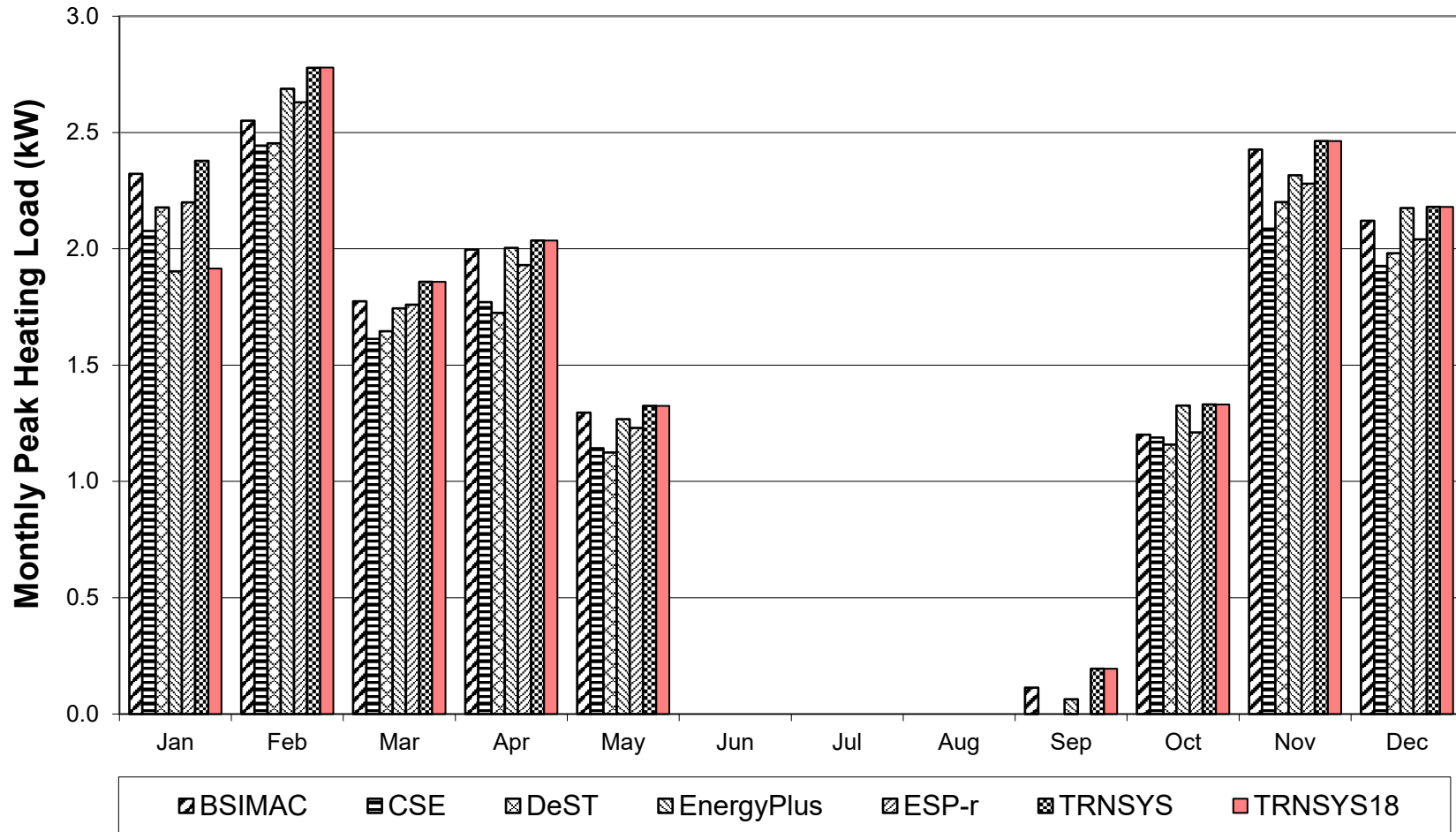
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-M6.**  
**Monthly Sensible Cooling**  
**Case 900**



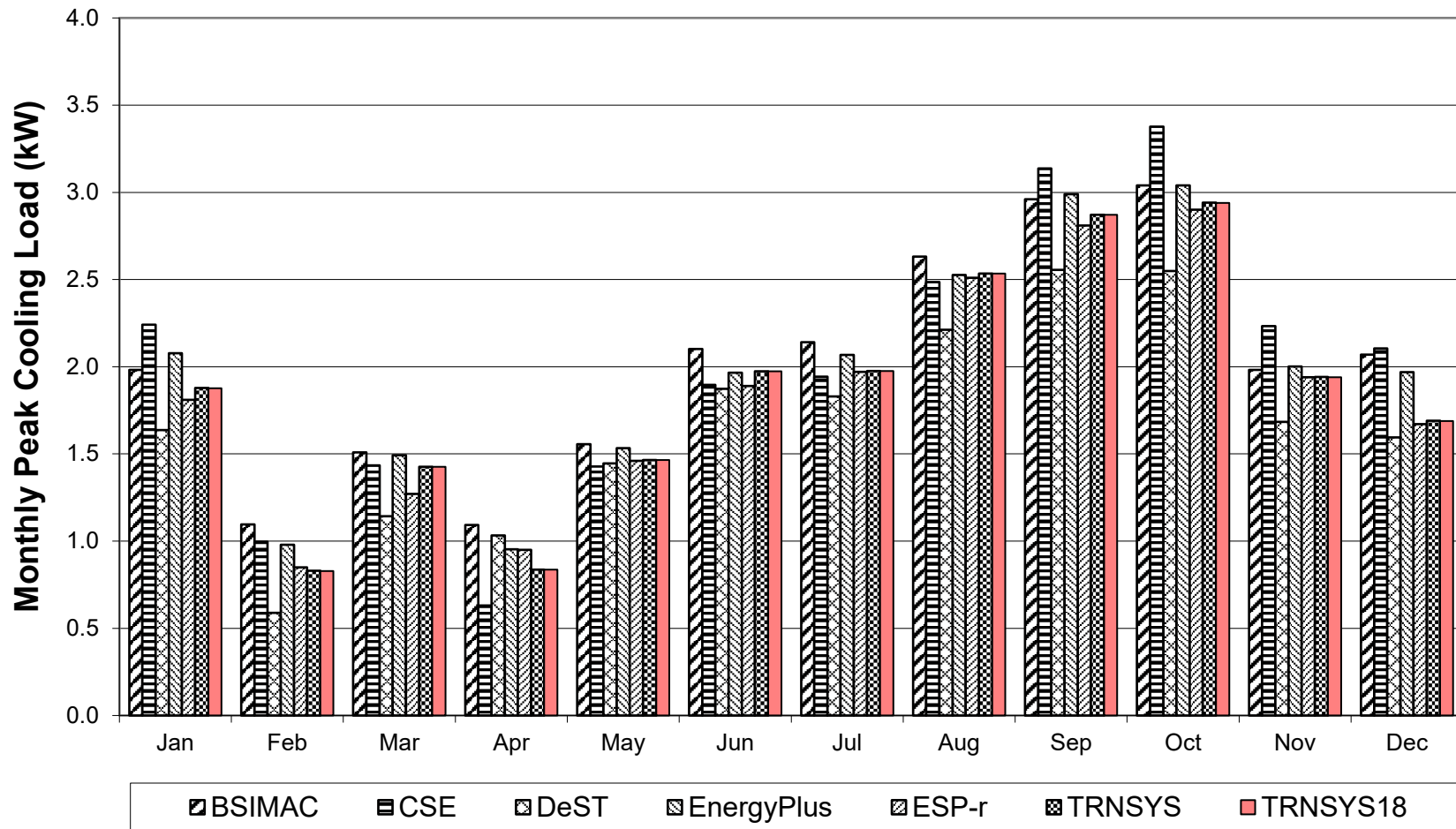
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-M7.**  
**Monthly Peak Heating**  
**Case 900**



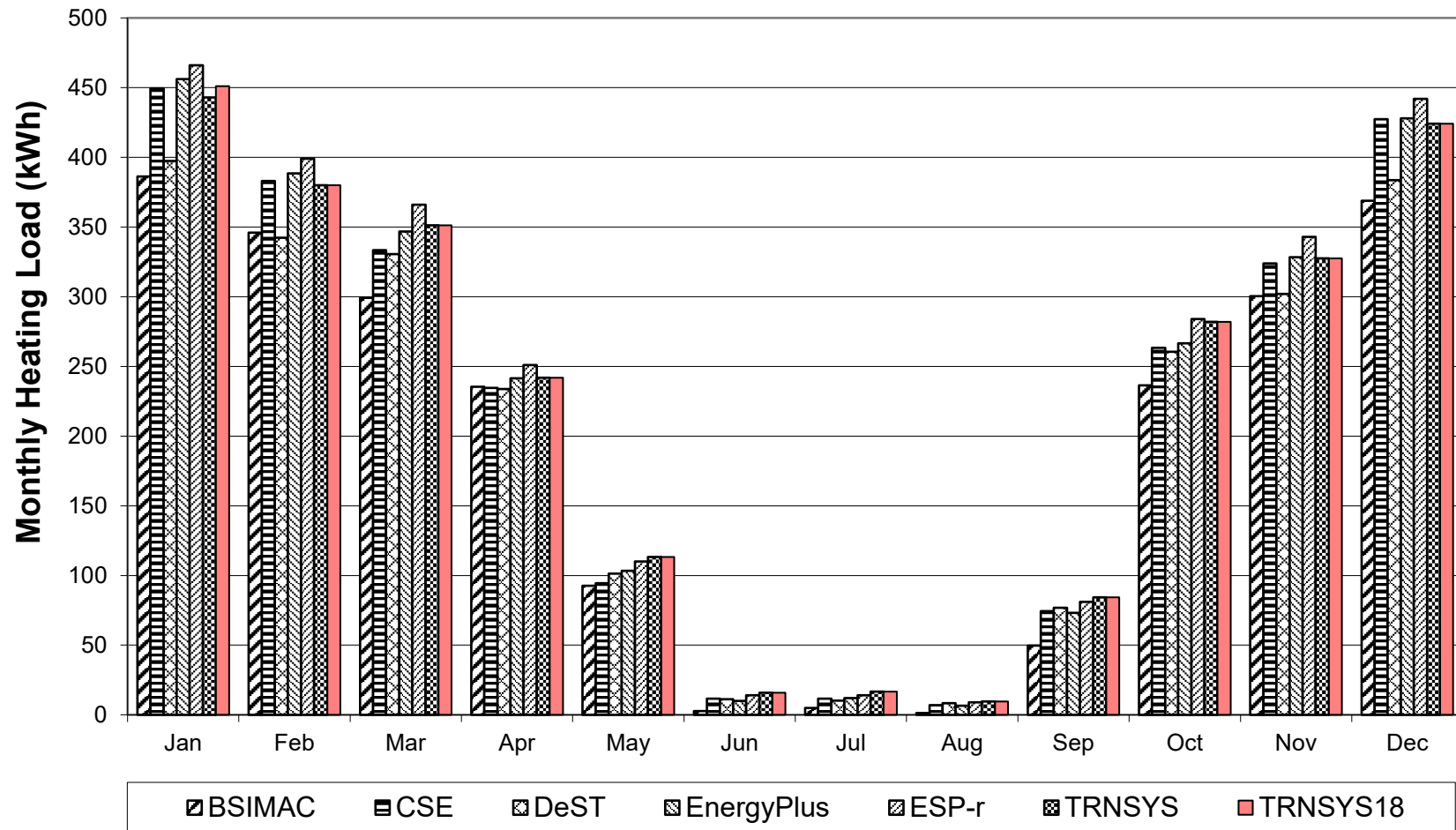
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-M8.**  
**Monthly Peak Sensible Cooling**  
**Case 900**



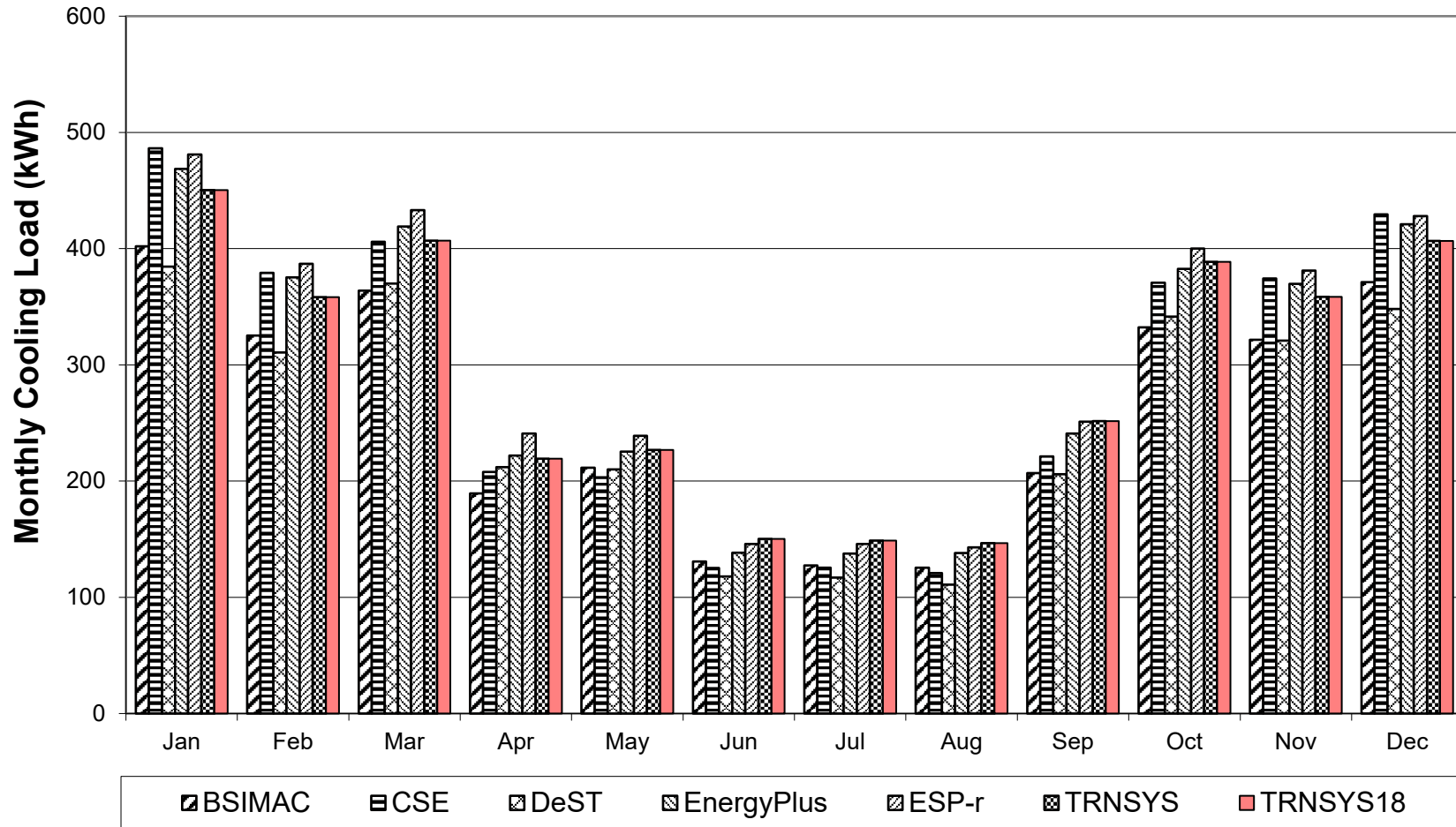
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-M9.**  
**Monthly Heating Sensitivity (Delta)**  
**Case 600-900**



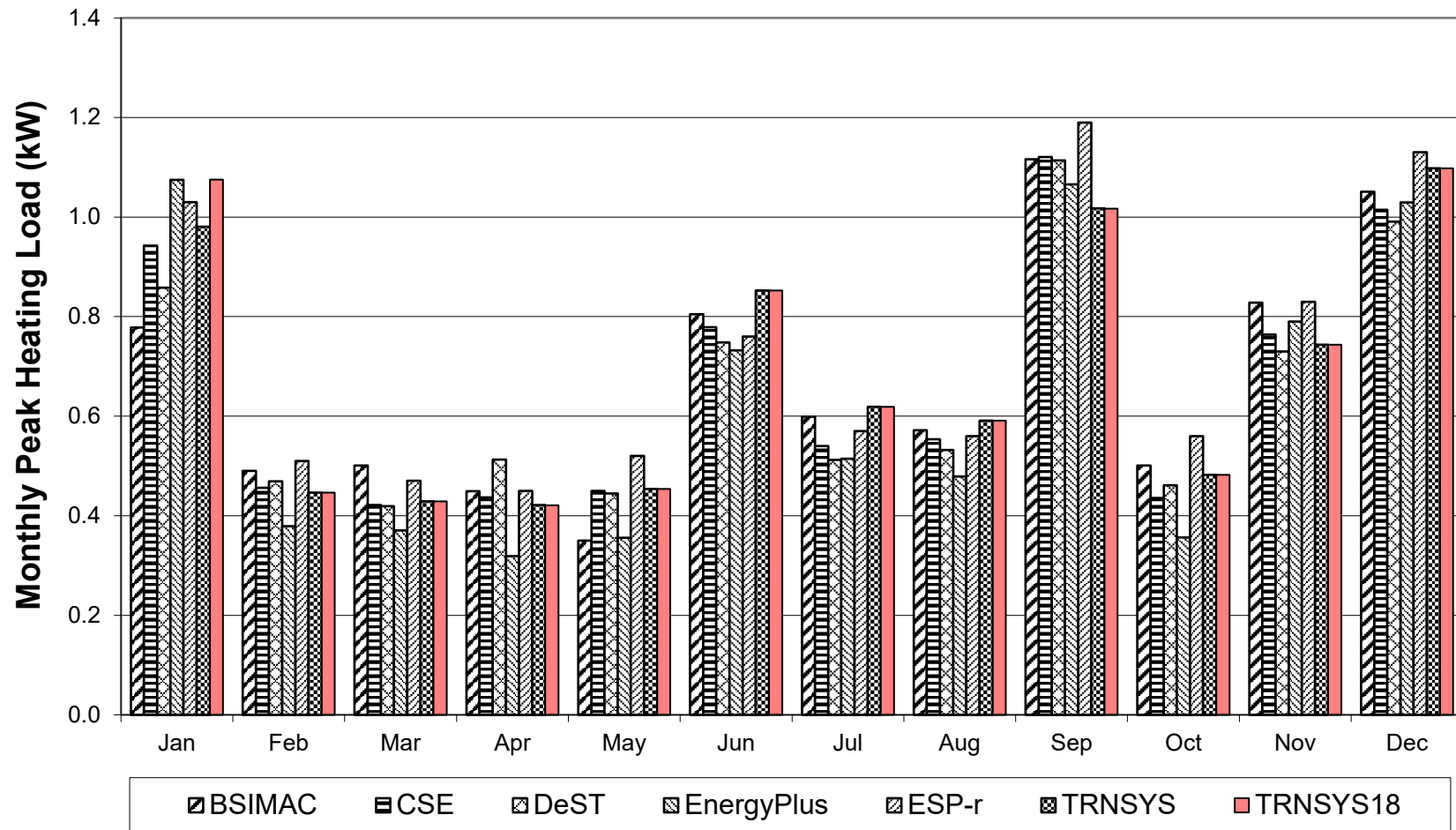
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-M10.**  
**Monthly Cooling Sensitivity (Delta)**  
**Case 600-900**



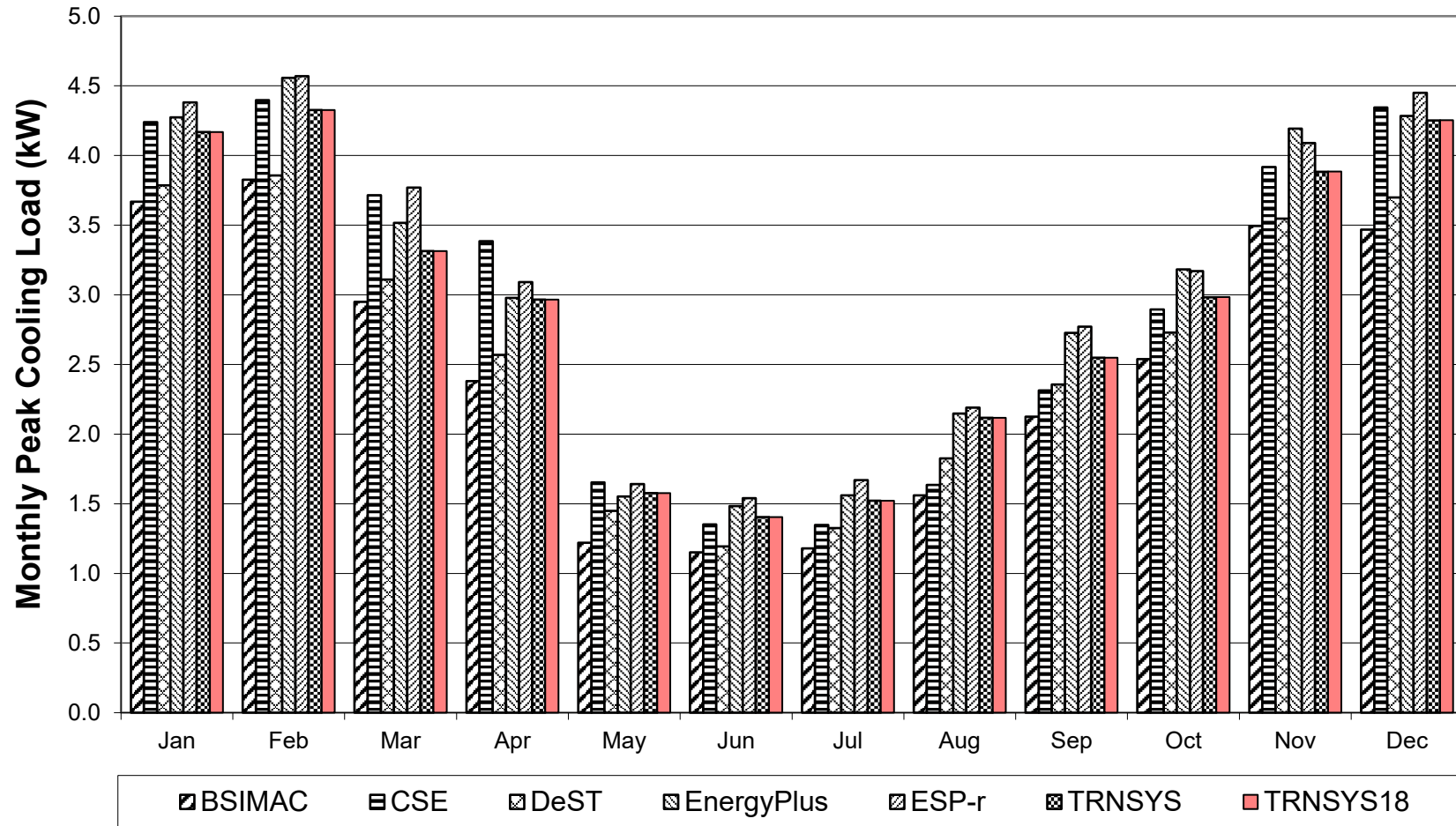
ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

**Figure B8-M11.**  
**Monthly Peak Heating Sensitivity (Delta)**  
**Case 600-900**



ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

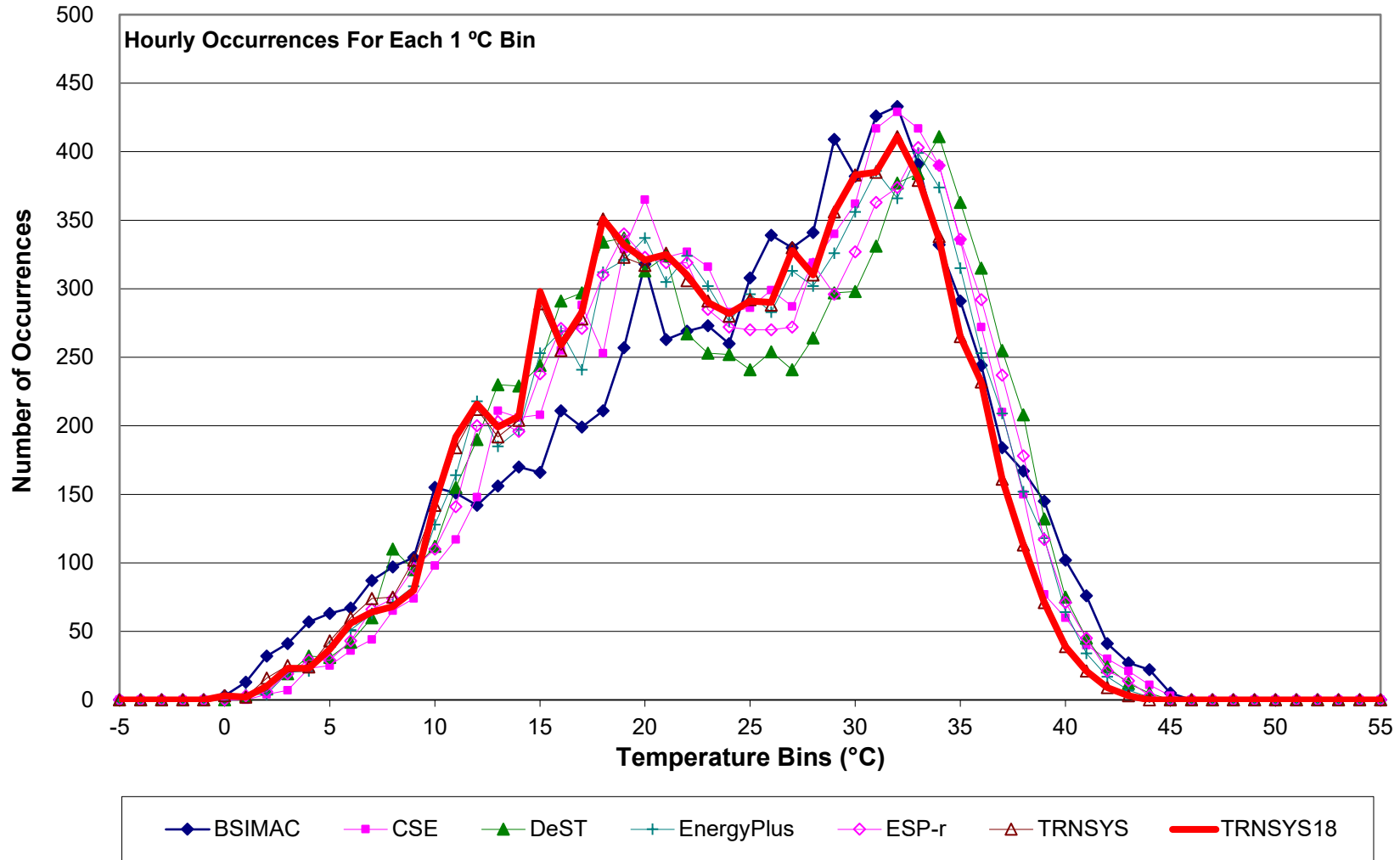
**Figure B8-M12.**  
**Monthly Peak Cooling Sensitivity (Delta)**  
**Case 600-900**



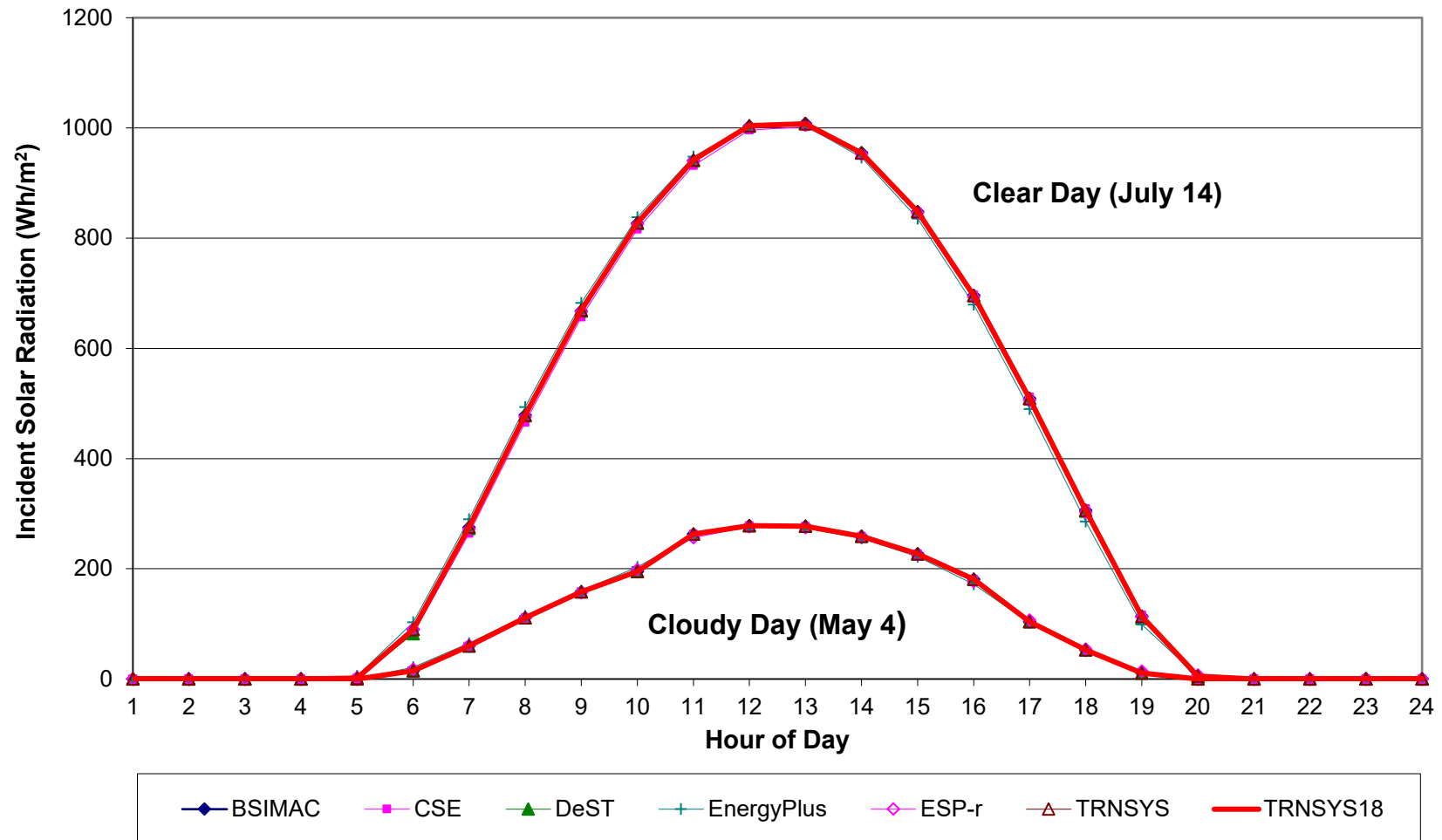


ASHRAE Standard 140-2020, Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Cases 195-995 & 600FF-980FF (TRNSYS18) vs. Annex B8, Section B8.1 Example Results, by Thermal Energy System Specialists, LLC (TESS), 22-Mar-2023

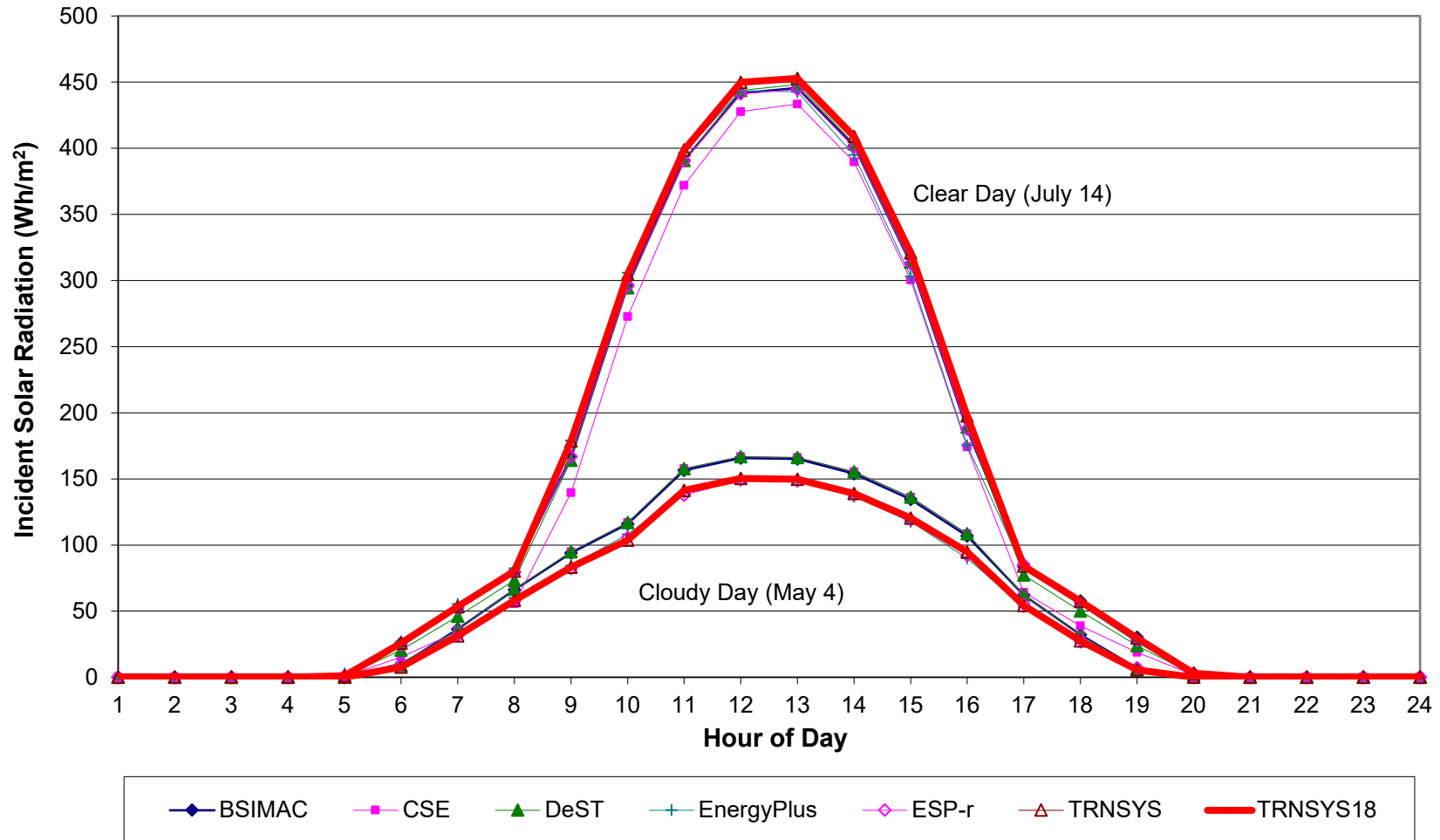
**Figure B8-H1. Case 900FF**  
**Annual Hourly Zone Air Temperature Frequency**



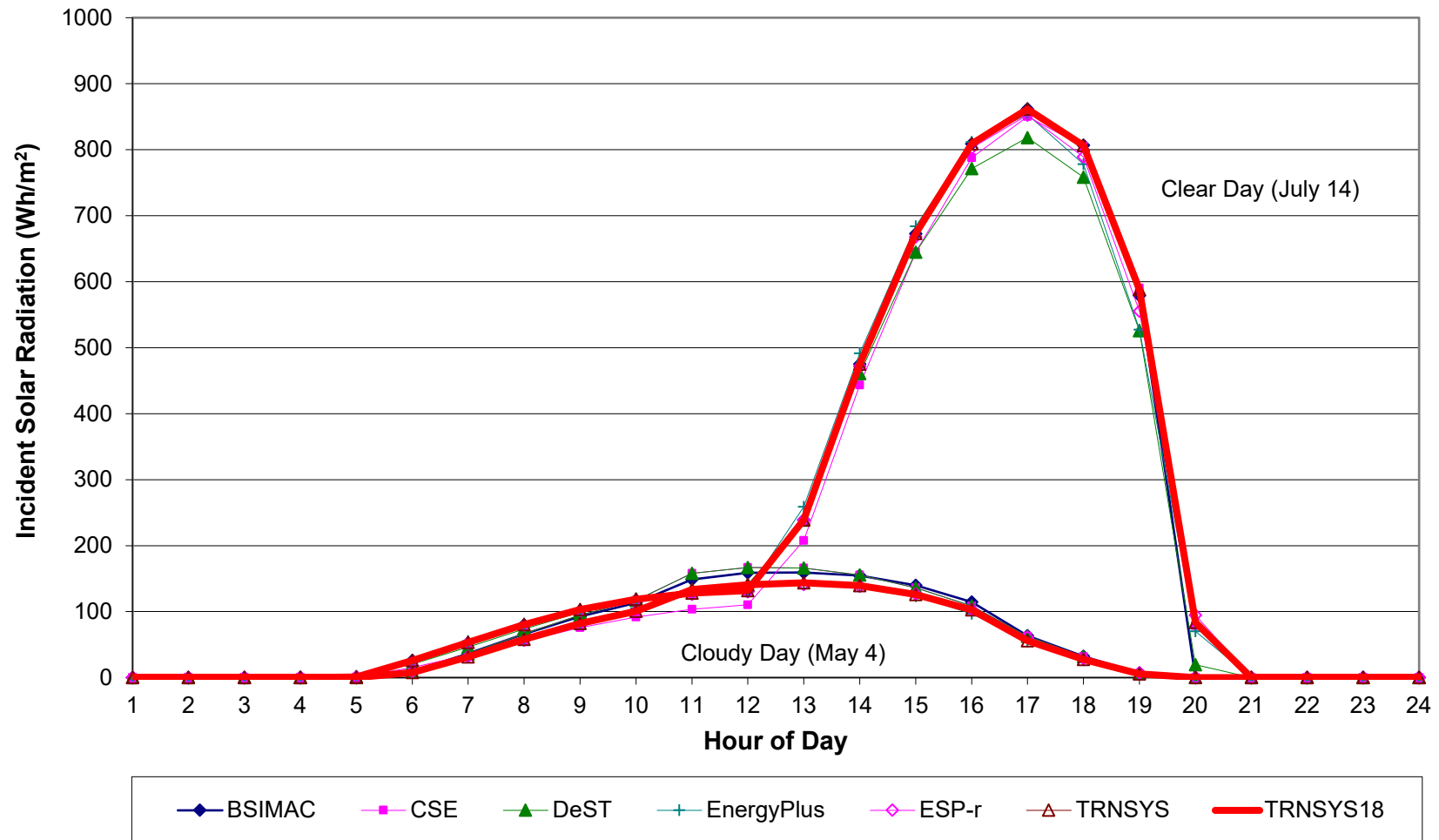
**Figure B8-H2. Case 600**  
**Cloudy & Clear Day Hourly Incident Solar**  
**Horizontal (Upward) Facing Surface**



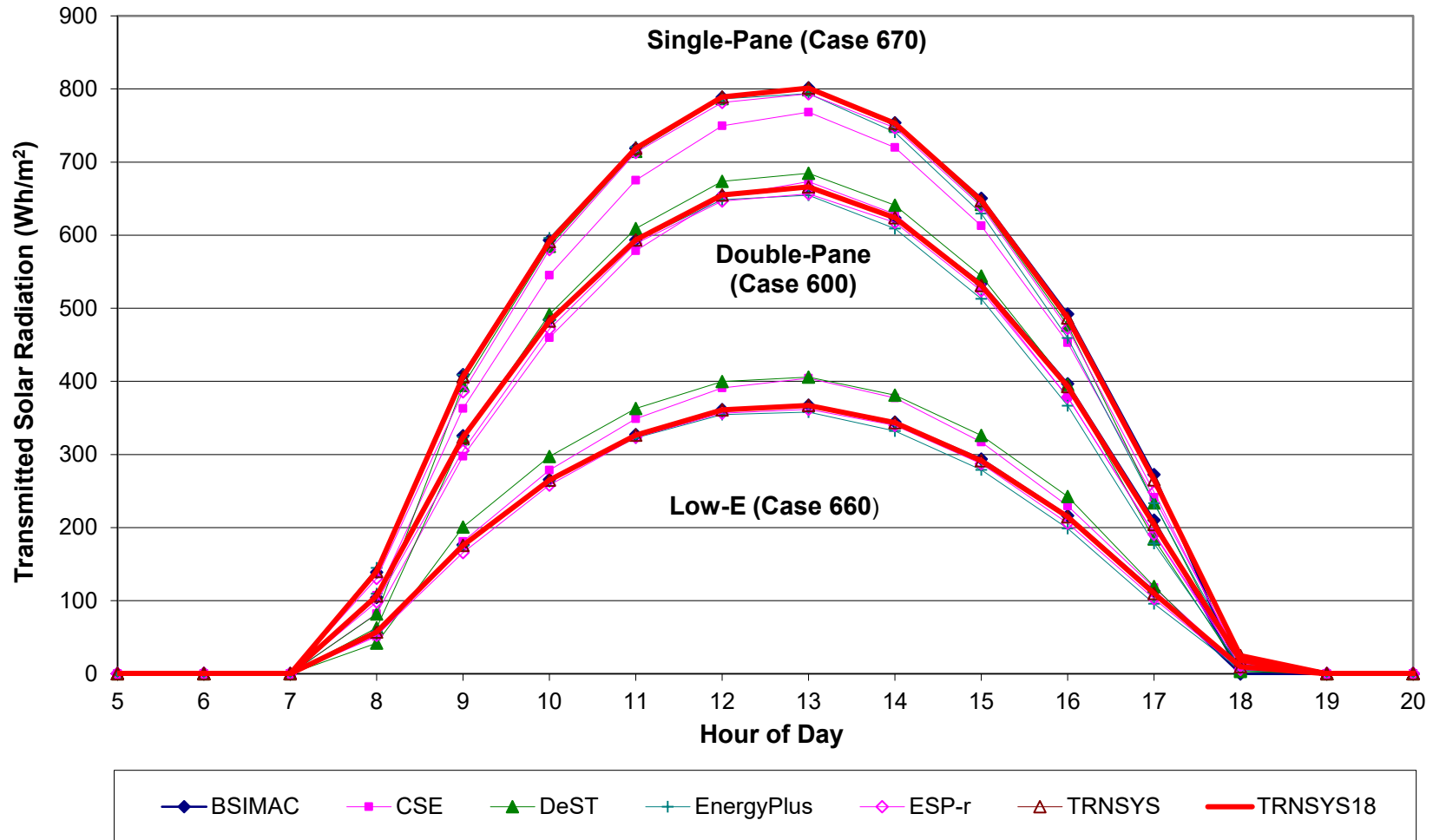
**Figure B8-H3. Case 600**  
**Cloudy & Clear Day Hourly Incident Solar**  
**South Facing Surface**



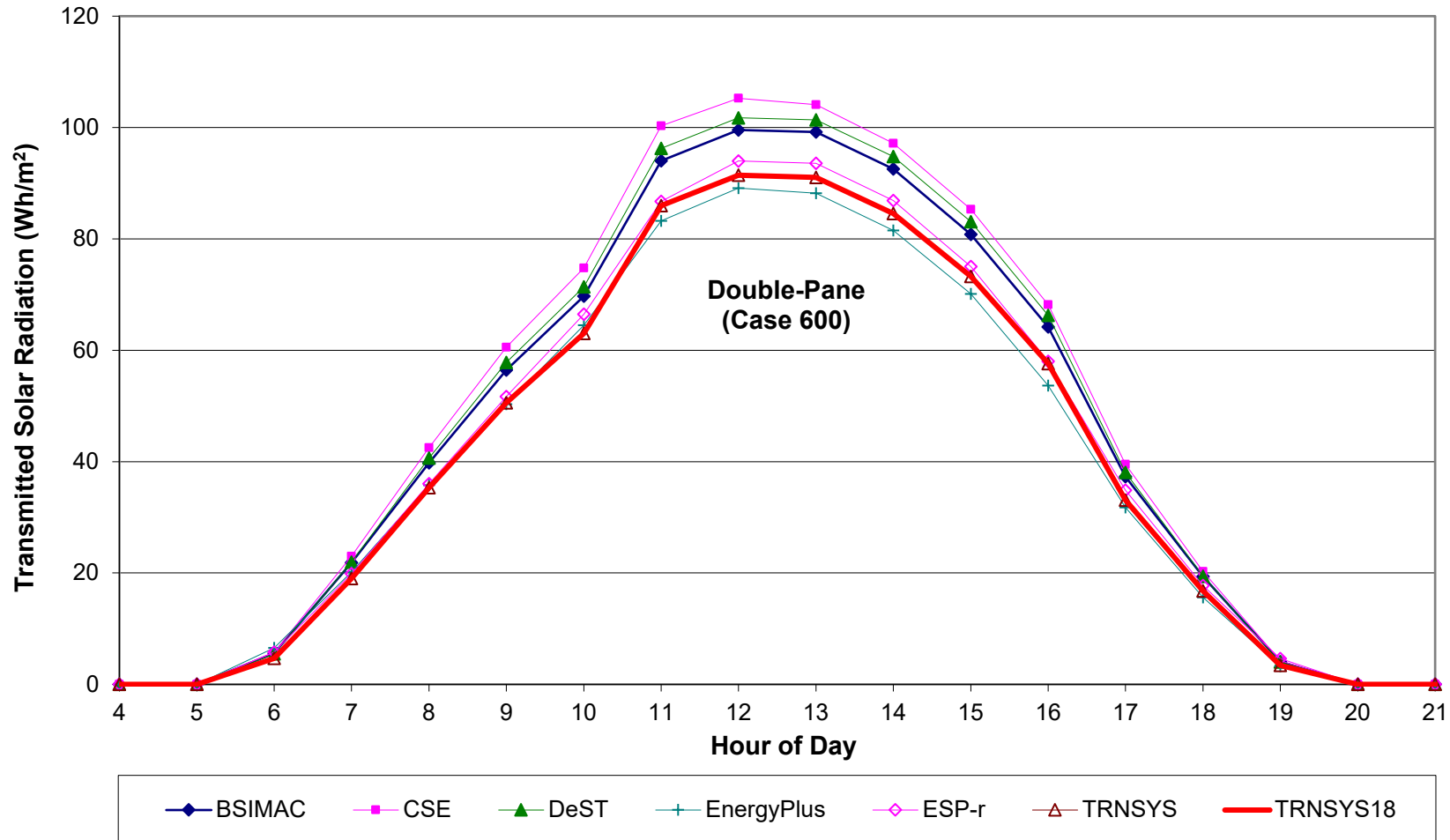
**Figure B8-H4. Case 600**  
**Cloudy & Clear Day Hourly Incident Solar**  
**West Facing Surface**



**Figure B8-H5. Cases 600, 660, 670**  
**Hourly Transmitted Solar, Clear/Cold Day (Feb 1)**  
**Double-Pane, Low-E, Single-Pane Windows**

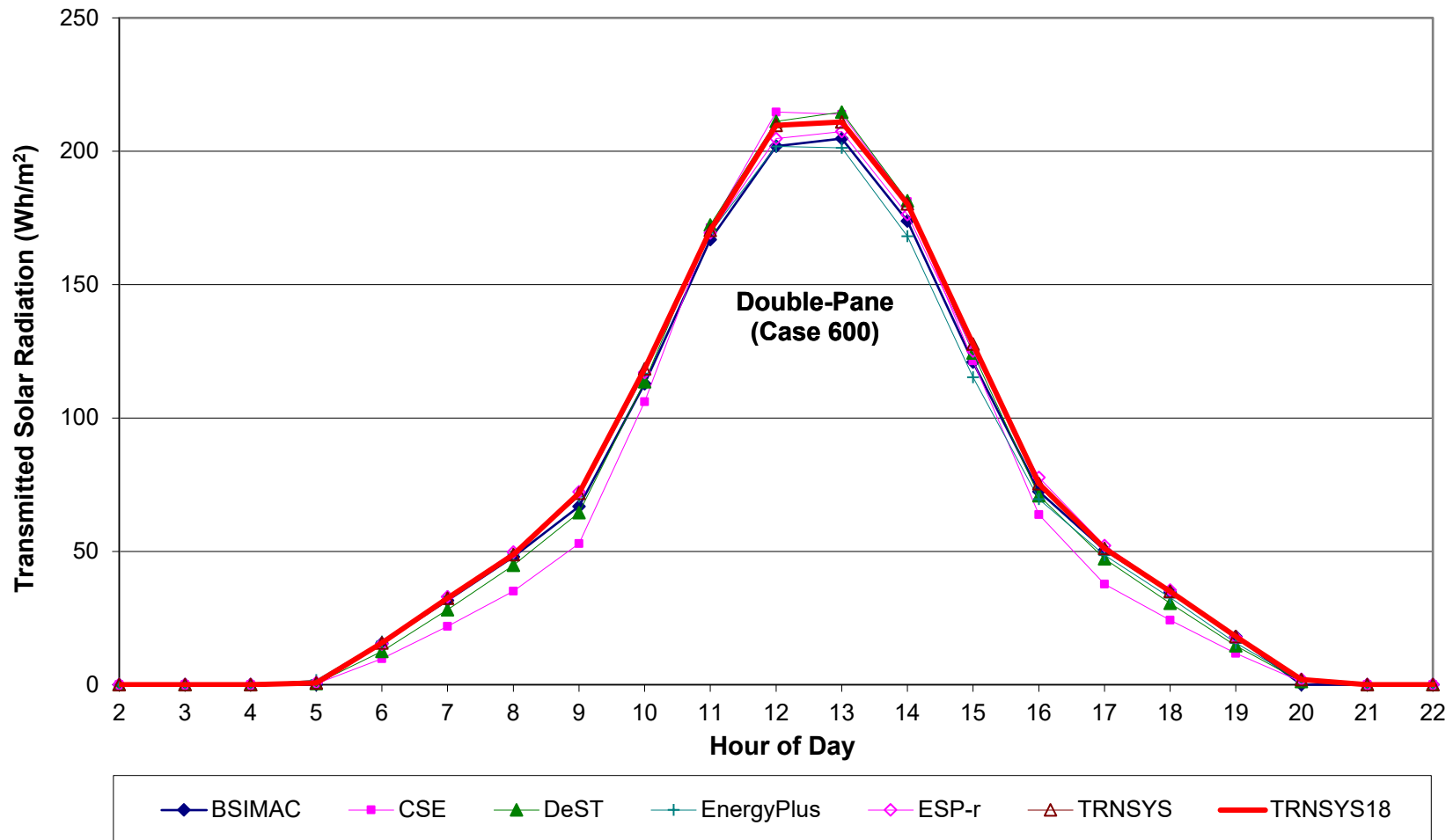


**Figure B8-H6. Case 600**  
**Hourly Transmitted Solar, Cloudy Day (May 4)**  
**Double-Pane Windows**



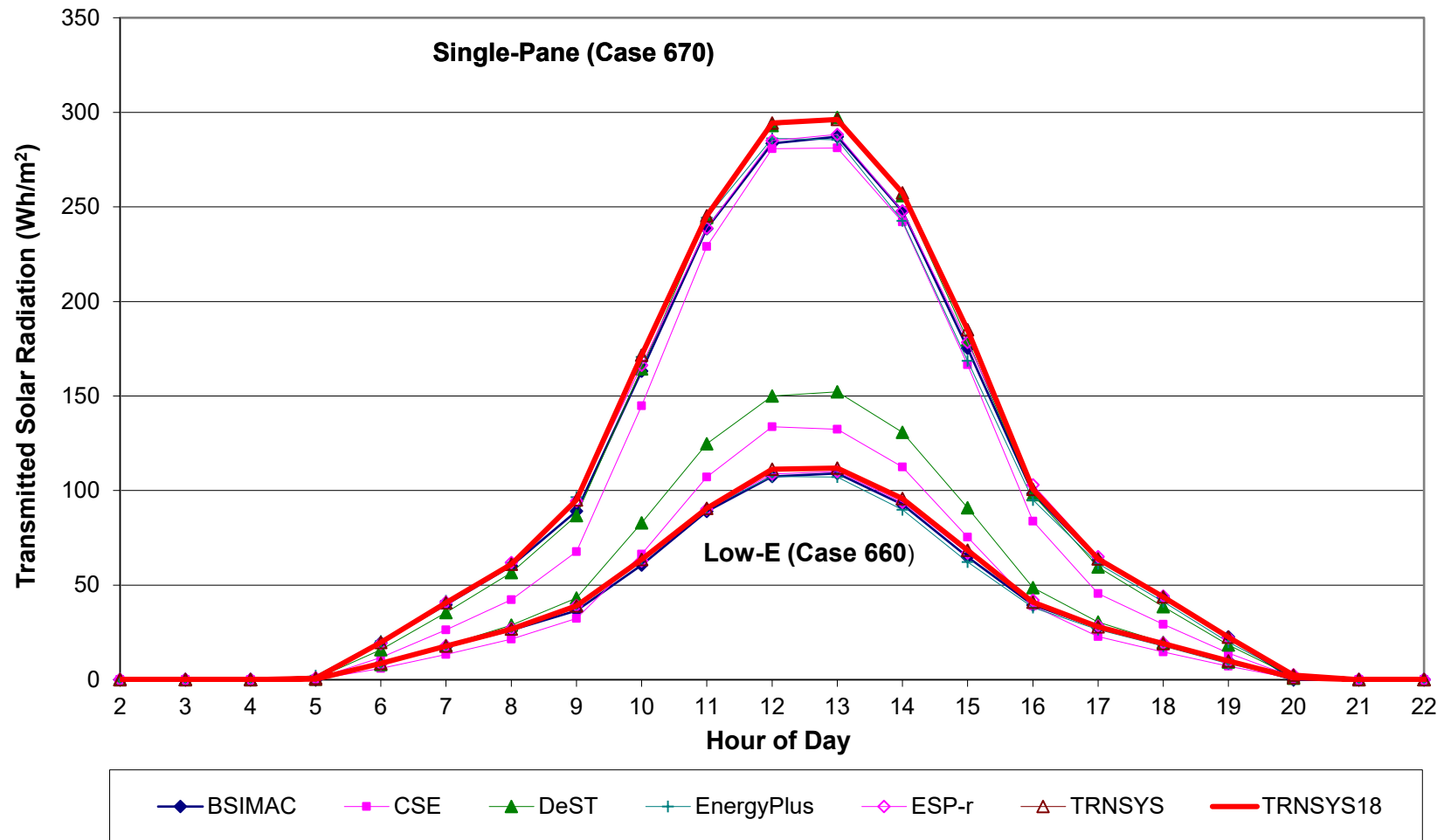


**Figure B8-H8. Case 600**  
**Hourly Transmitted Solar, Clear/Hot Day (Jul 14)**  
**Double-Pane Windows**

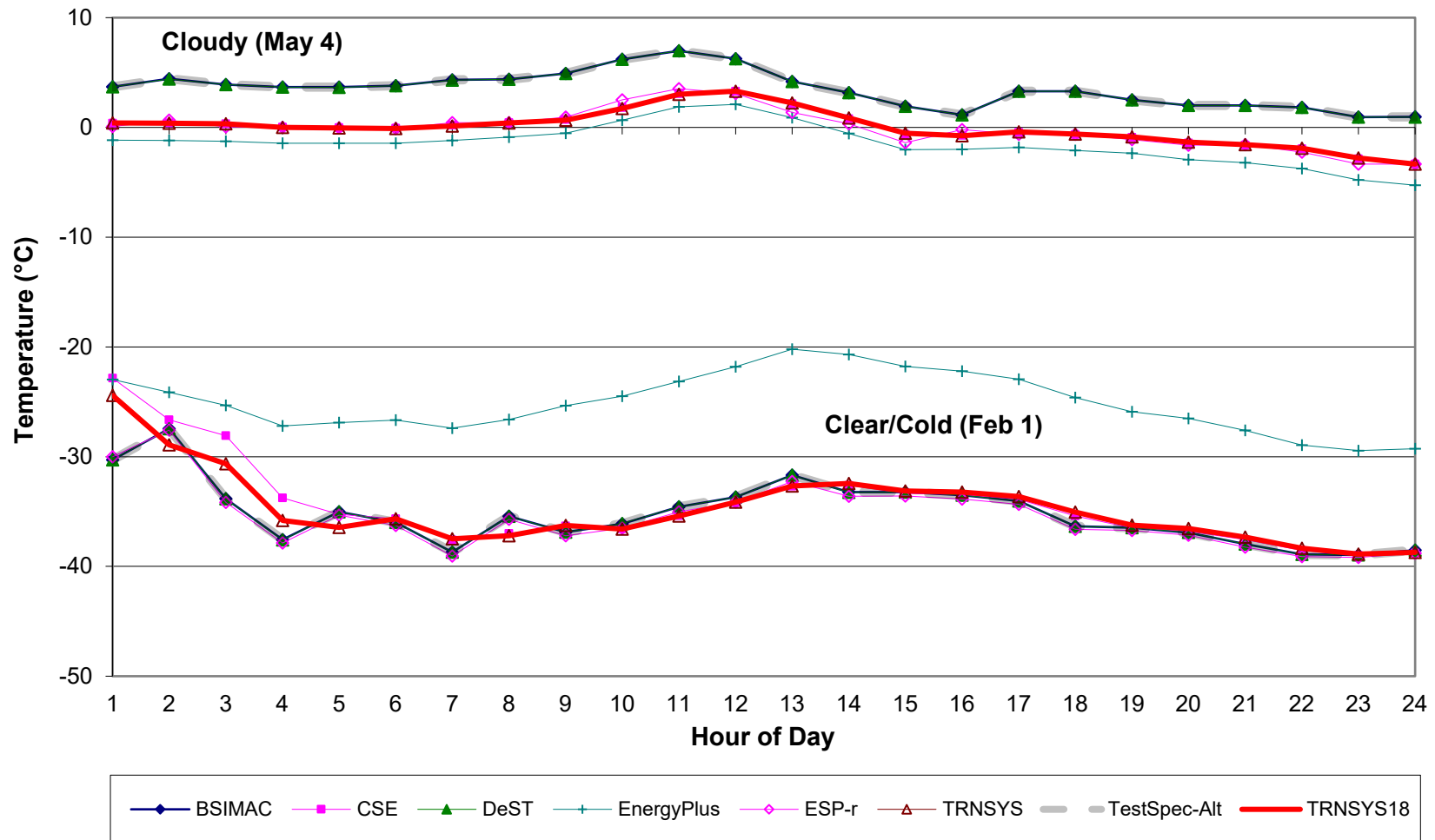




**Figure B8-H9. Cases 660, 670**  
**Hourly Transmitted Solar, Clear/Hot Day (Jul 14)**  
**Low-E and Single-Pane Windows**

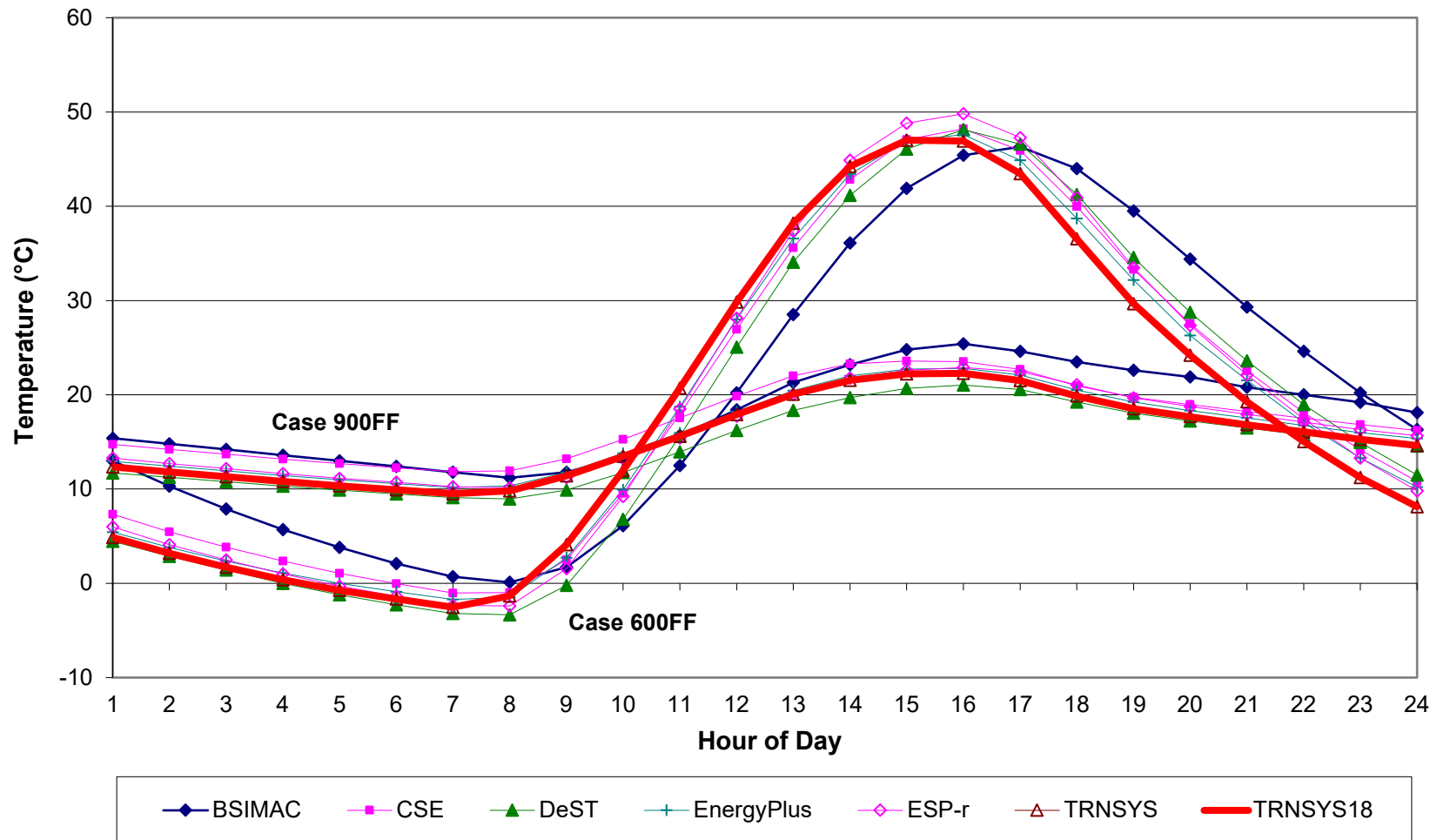


**Figure B8-H10.**  
**Hourly Sky Temperatures**  
**Case 600: Clear/Cold, Cloudy Days**

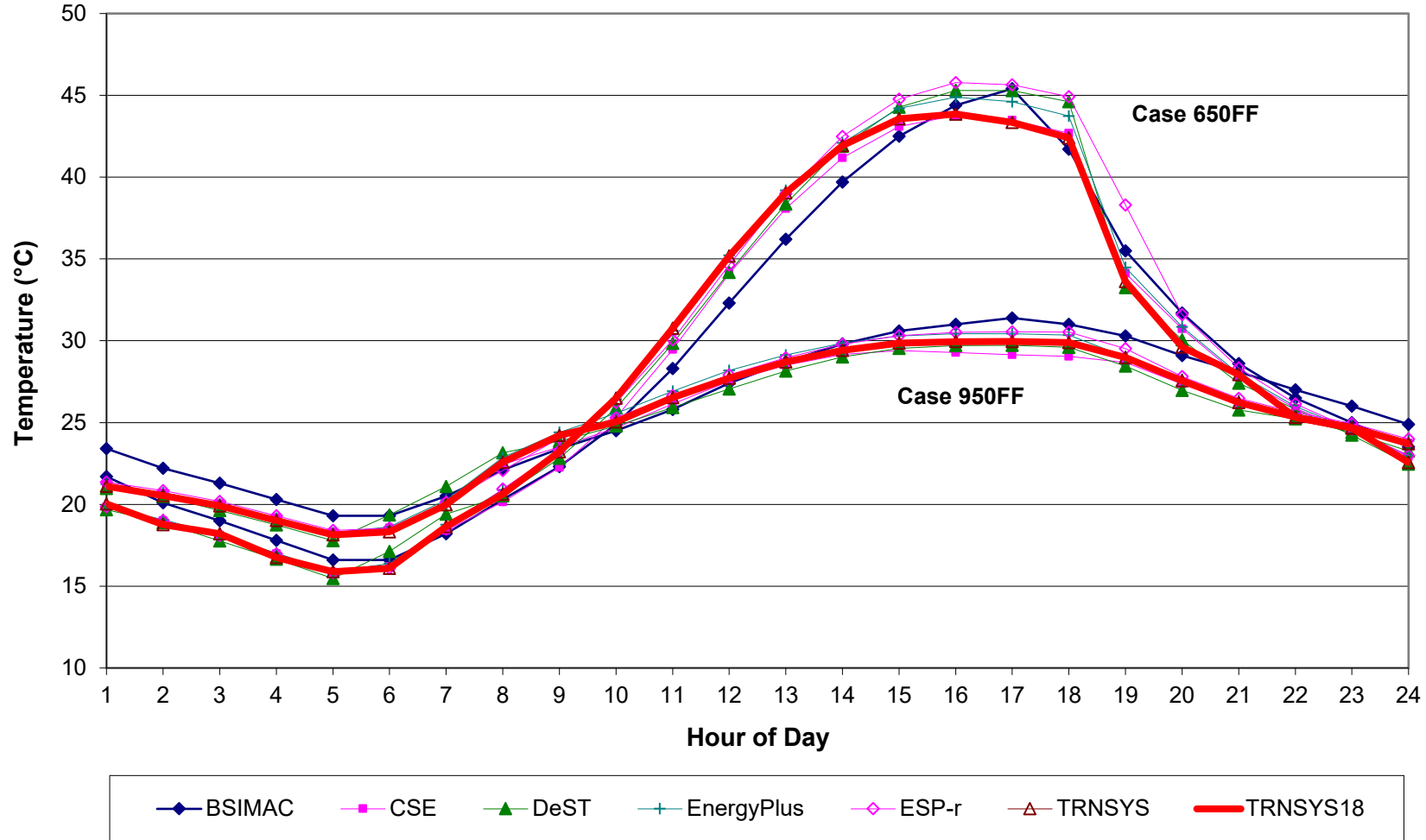




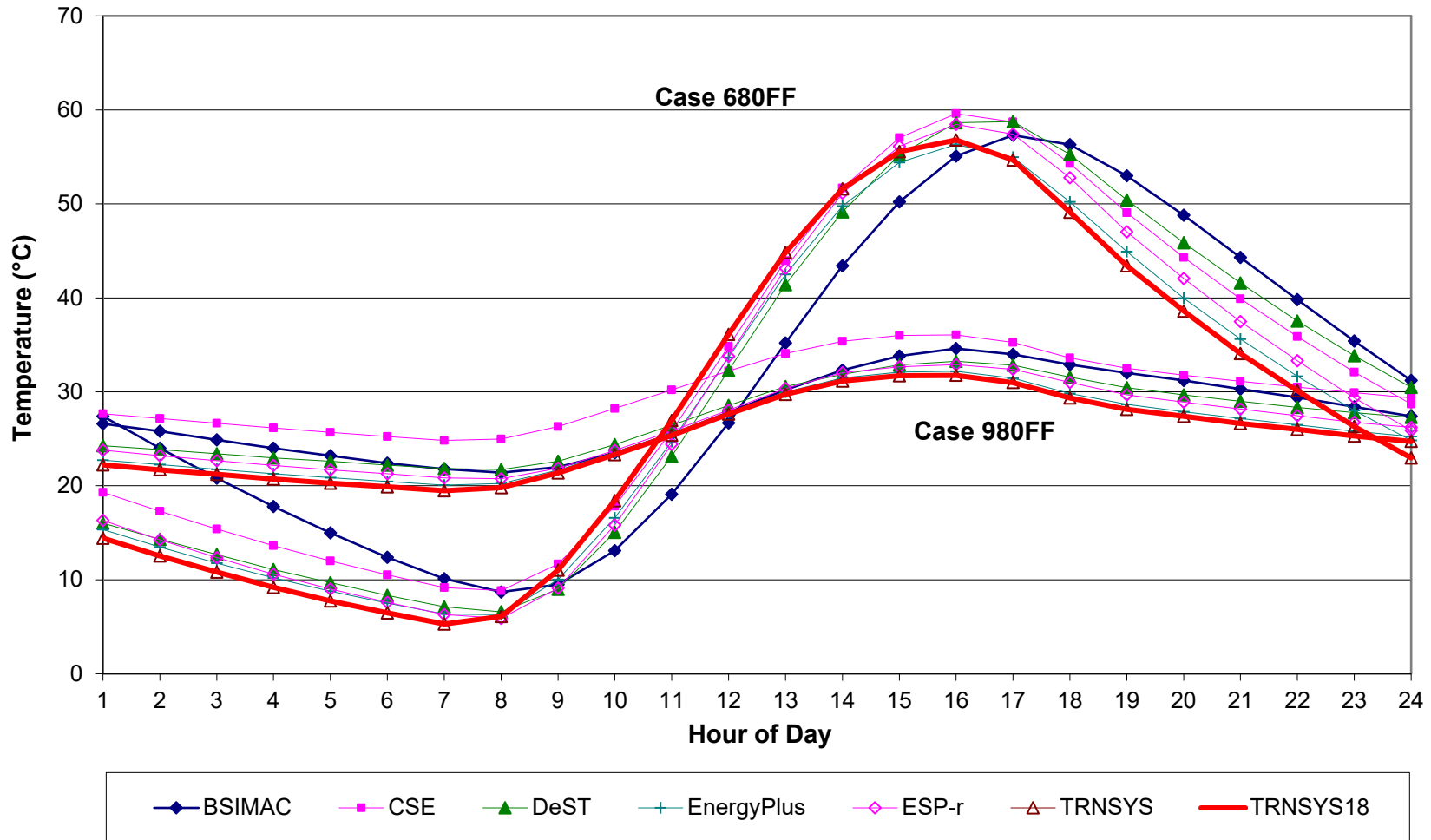
**Figure B8-H12.**  
**Hourly Free-Float Temperatures**  
**Clear Cold Day (Feb 1), Cases 600FF and 900FF**



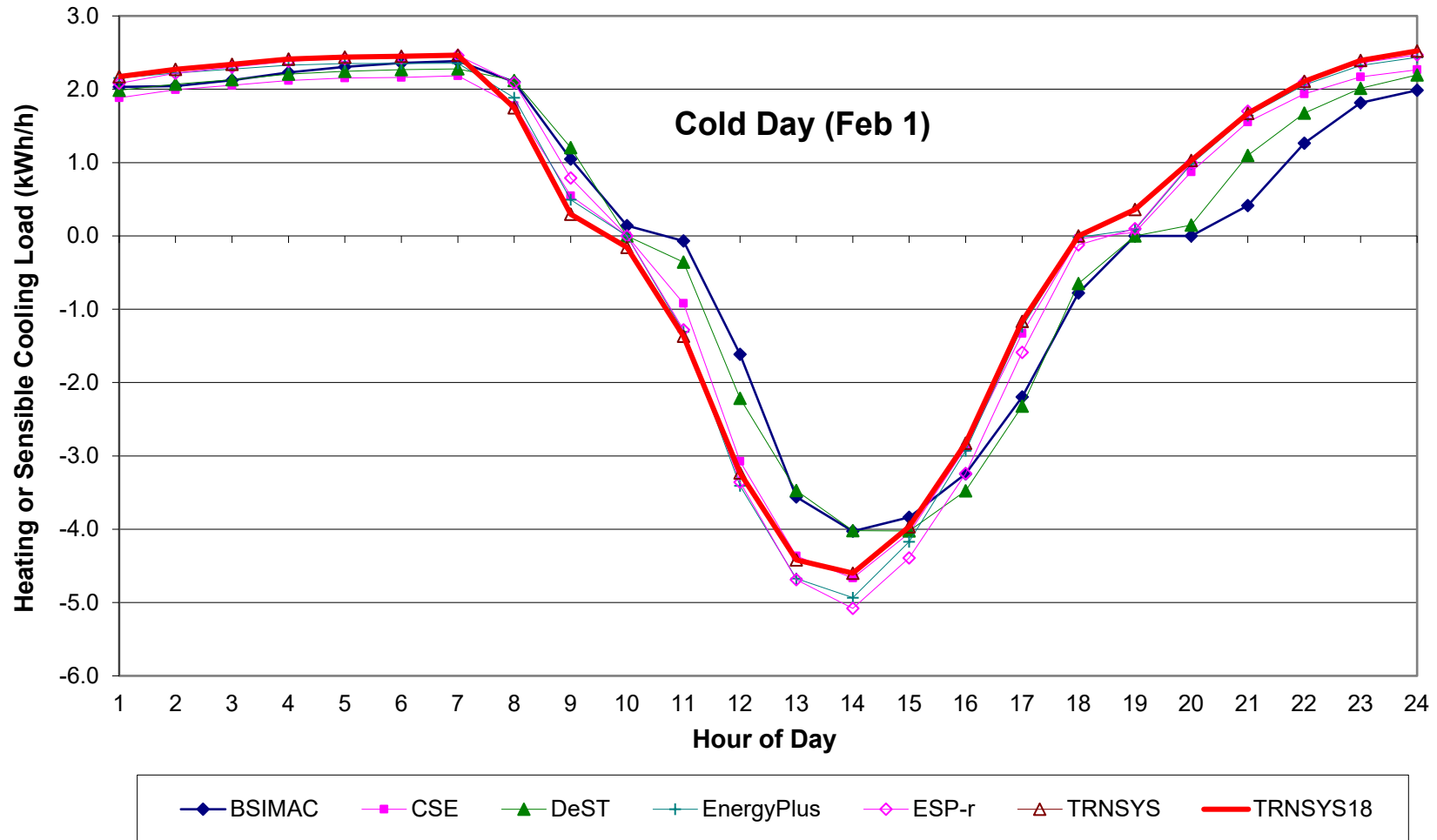
**Figure B8-H13.**  
**Hourly Free-Float Temperatures**  
**Clear Hot Day (Jul 14), Cases 650FF and 950FF**



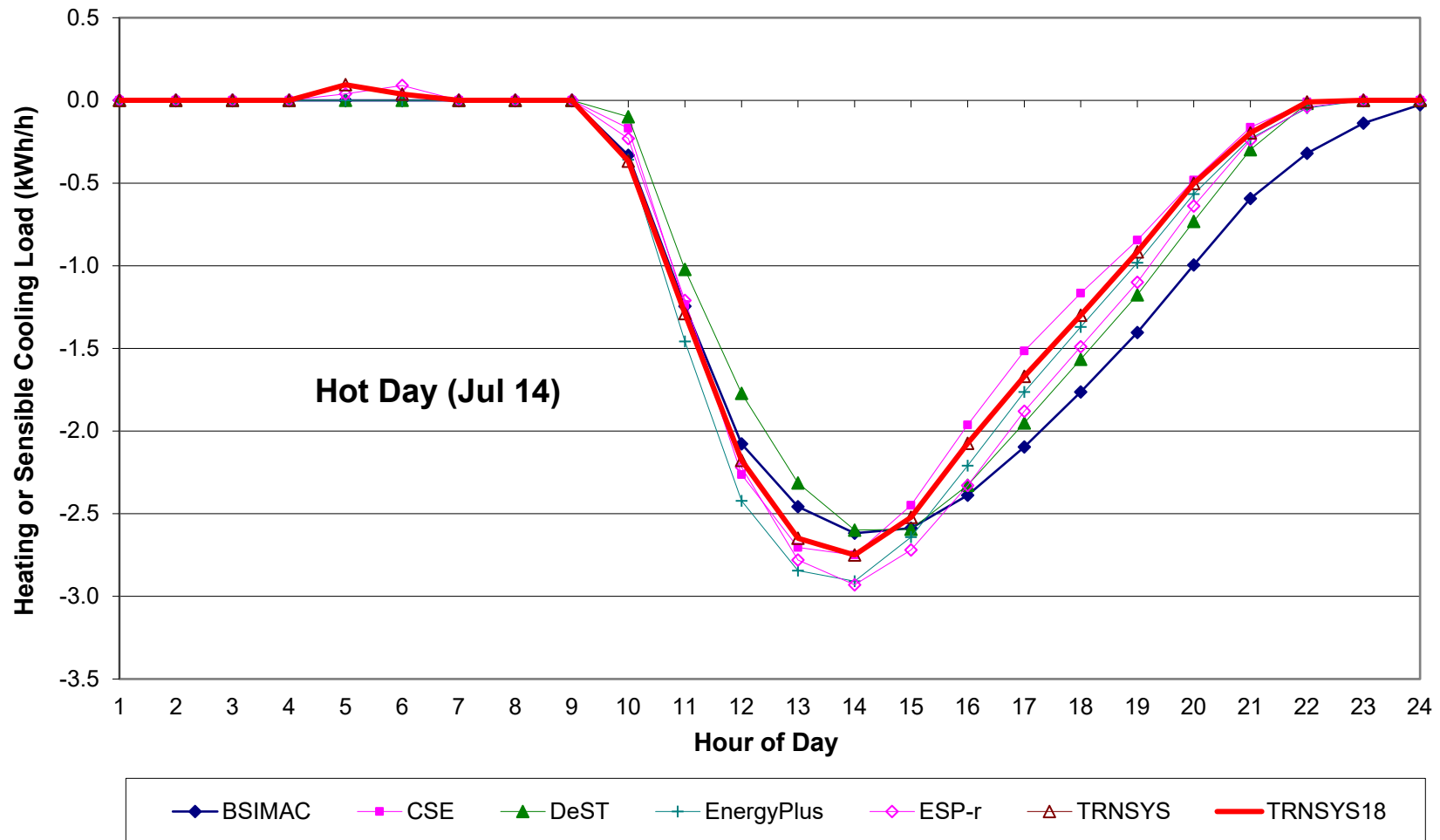
**Figure B8-H14.**  
**Hourly Free-Float Temperatures**  
**Clear Cold Day (Feb1), Cases 680FF and 980FF**



**Figure B8-H15. Hourly Loads**  
**Clear Cold Day, Case 600 (Low Mass, Double-Clear Window)**  
**Heating (+), Sensible Cooling (-)**

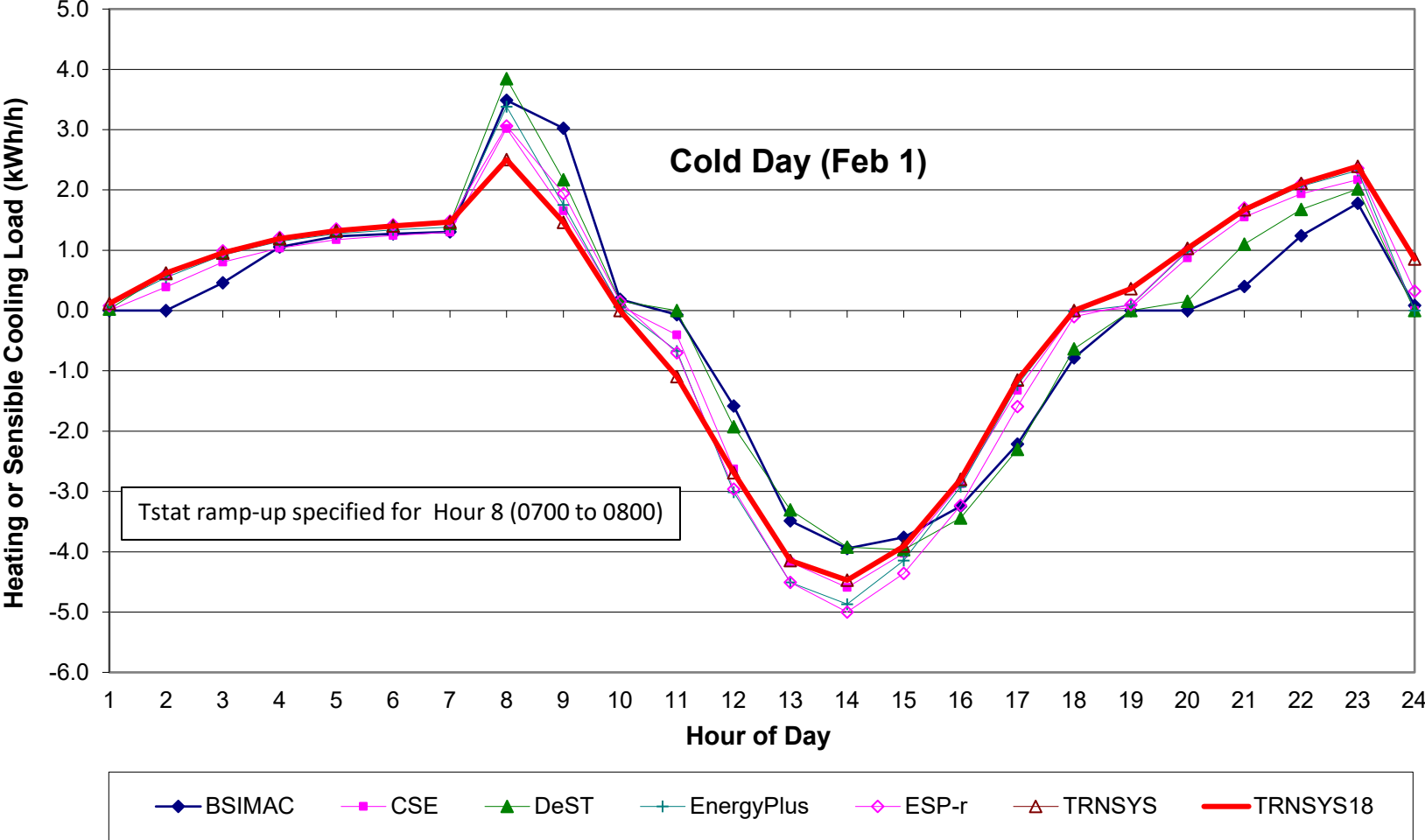


**Figure B8-H16. Hourly Loads**  
**Clear Hot Day, Case 600 (Low Mass, Double-Clear Window)**  
**Heating (+), Sensible Cooling (-)**

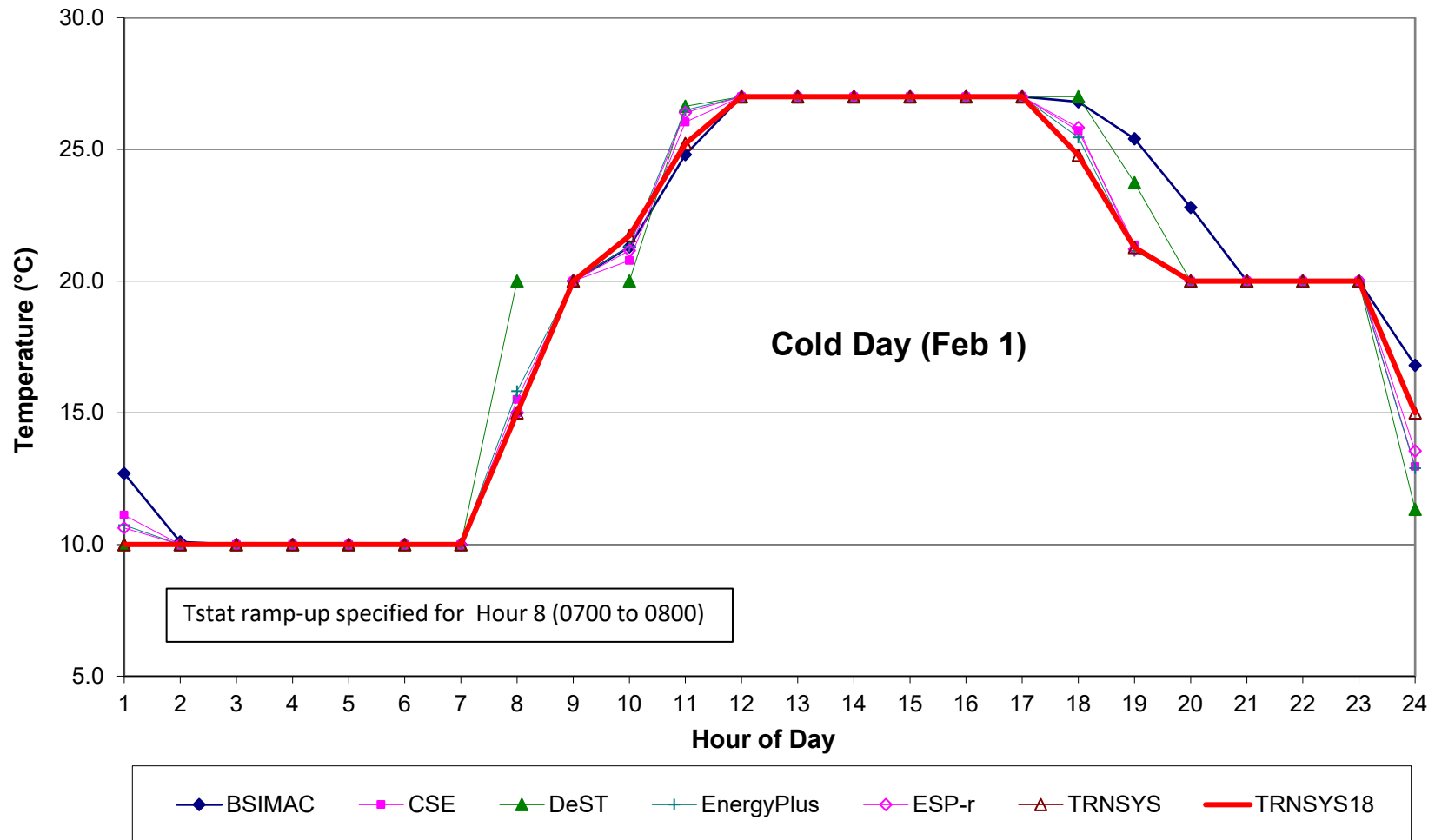




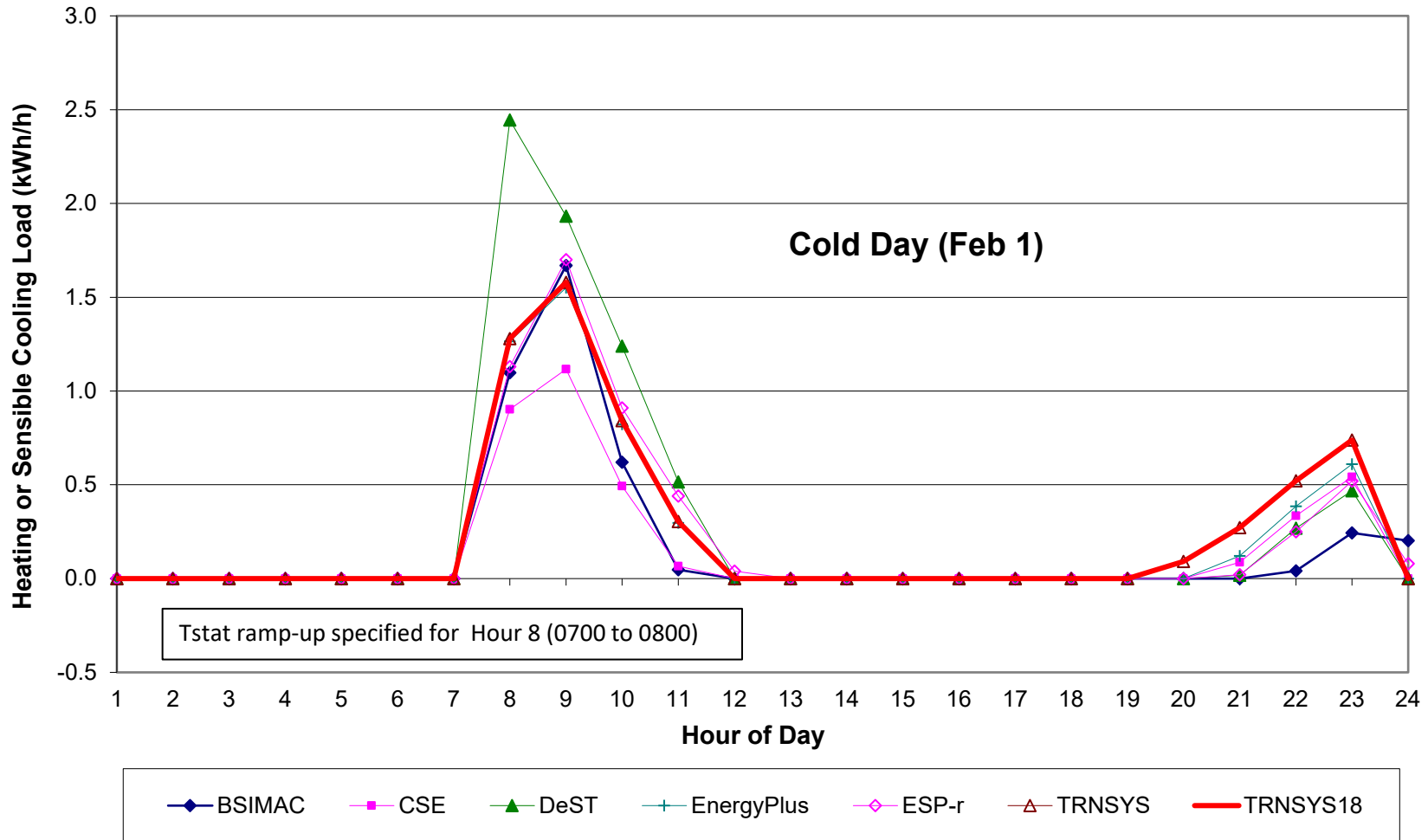
**Figure B8-H17. Hourly Loads**  
**Clear Cold Day, Case 640 (Low Mass, Night Setback)**  
**Heating (+), Sensible Cooling (-)**



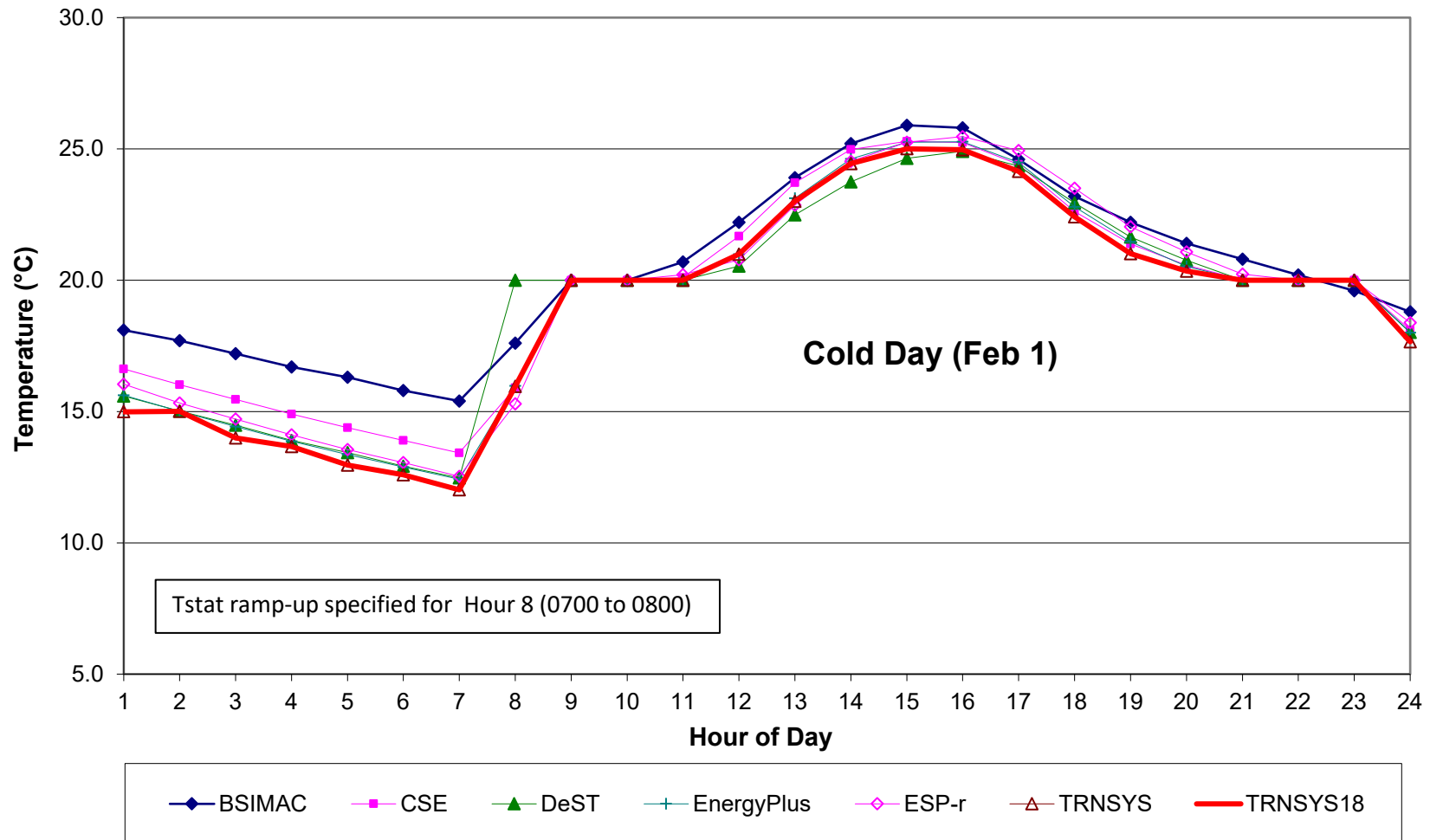
**Figure B8-H18.**  
**Hourly Conditioned Zone Temperatures**  
**Clear Cold Day, Case 640**



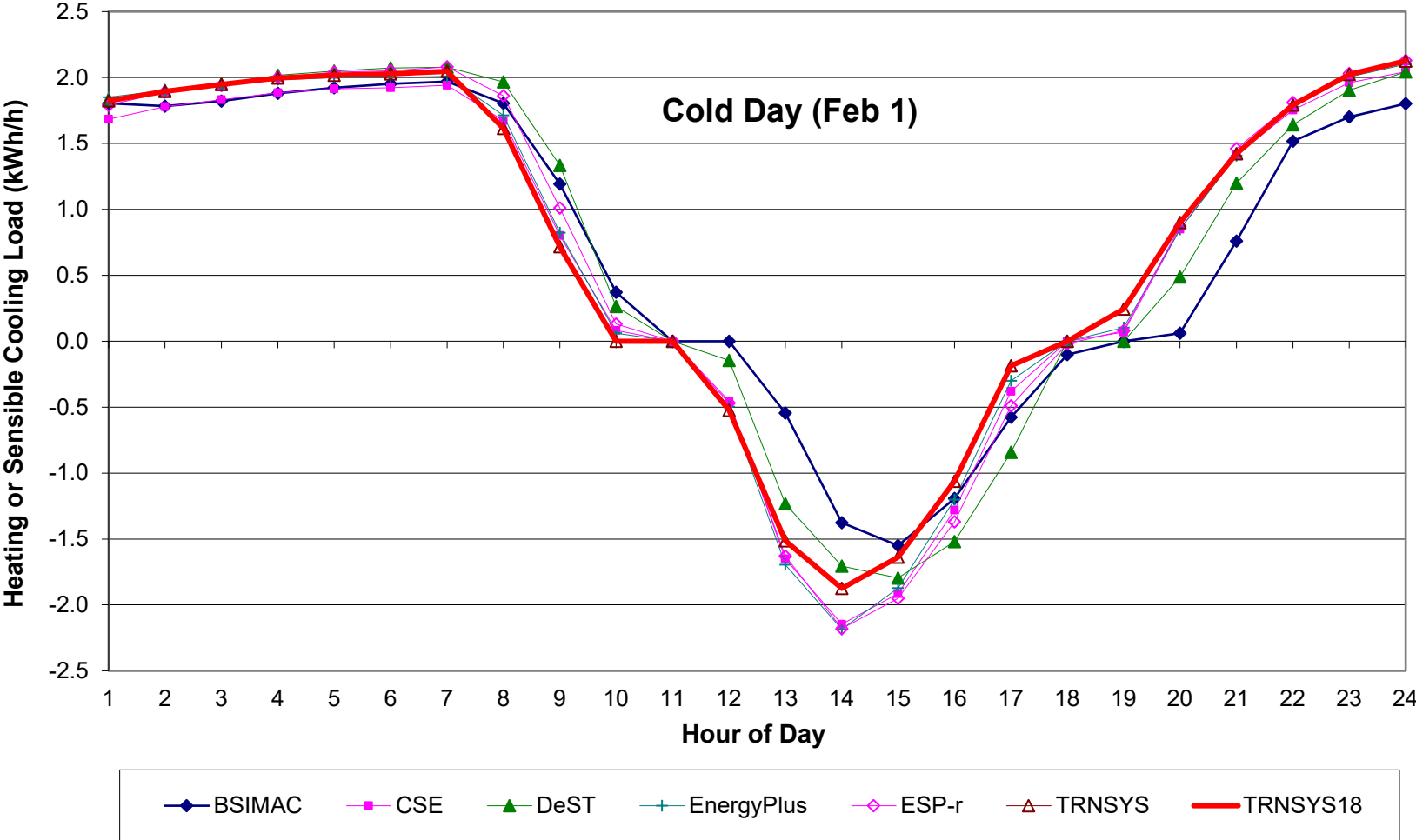
**Figure B8-H19. Hourly Loads**  
**Clear Cold Day, Case 940 (High Mass, Night Setback)**  
**Heating (+), Sensible Cooling (-)**



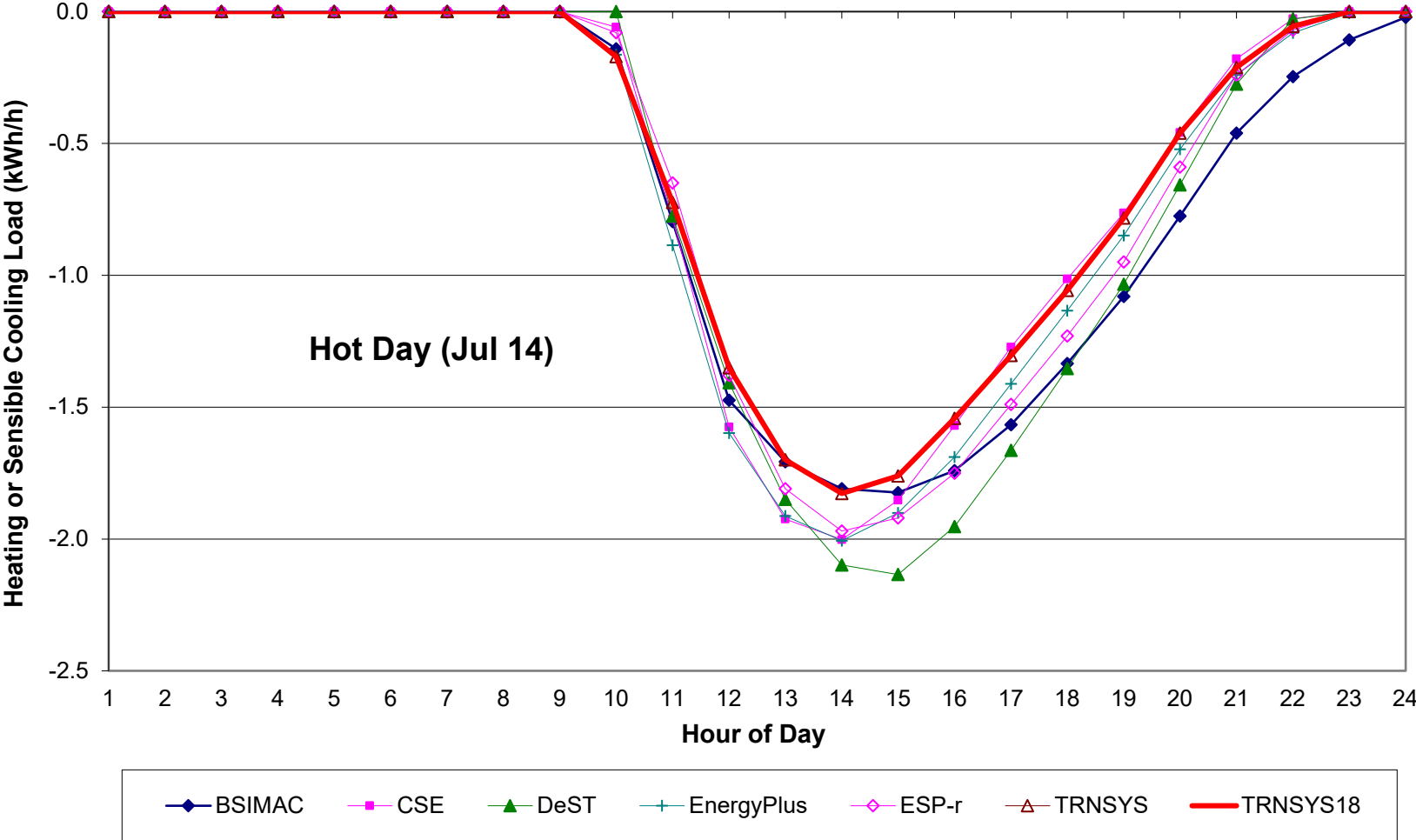
**Figure B8-H20.**  
**Hourly Conditioned Zone Temperatures**  
**Clear Cold Day, Case 940**



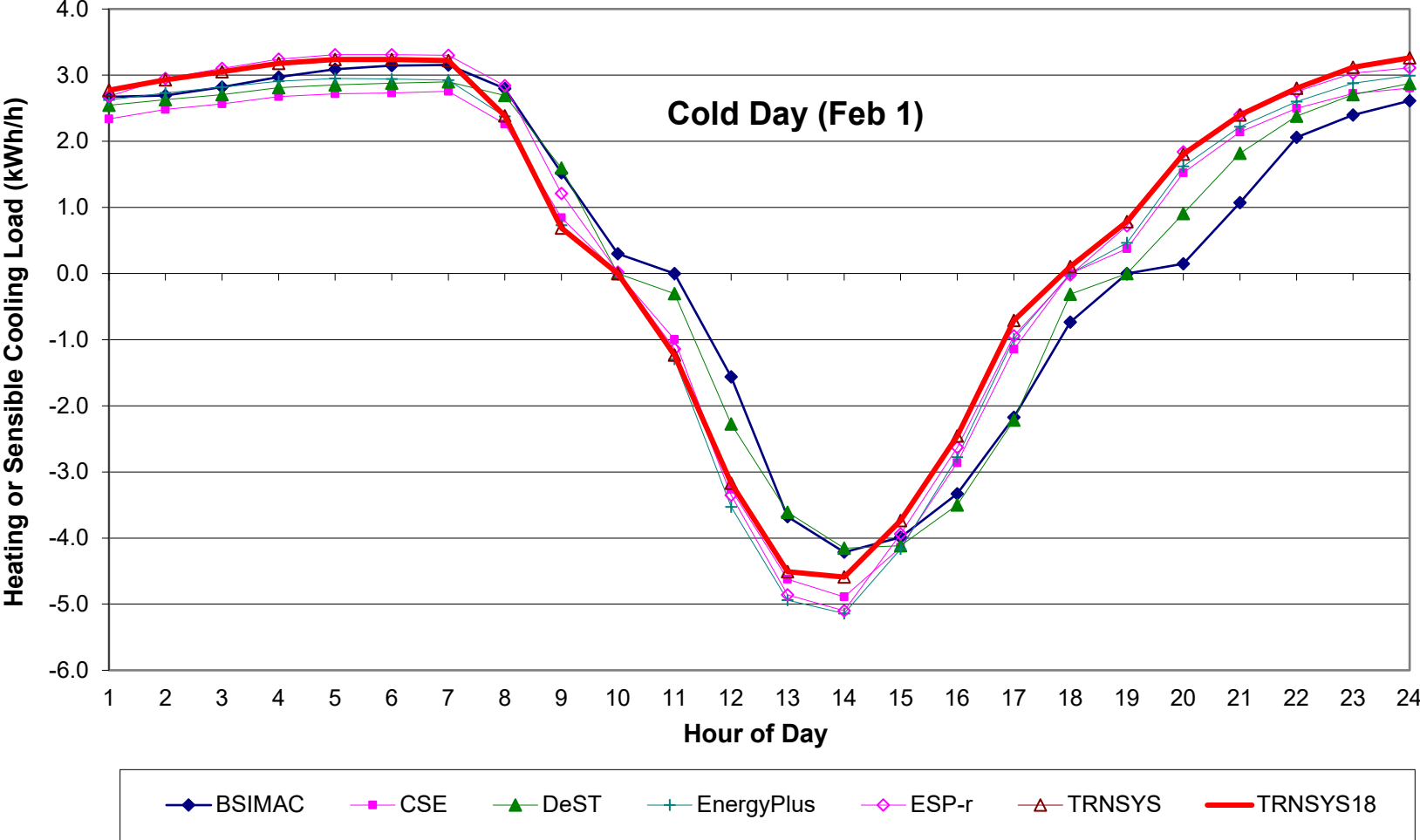
**Figure B8-H21. Hourly Loads**  
**Clear Cold Day, Case 660 (Low-E Window)**  
**Heating (+), Sensible Cooling (-)**



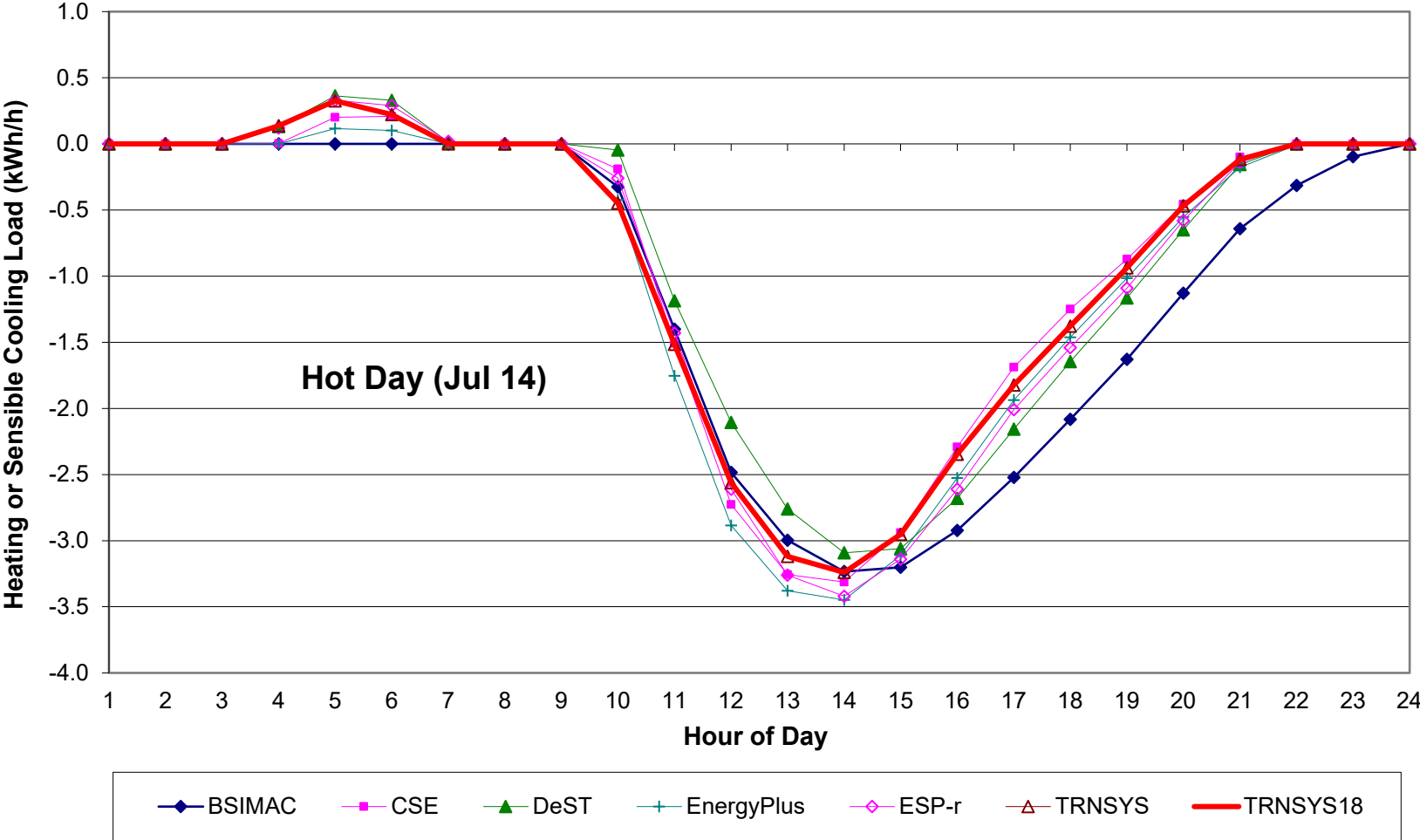
**Figure B8-H22. Hourly Loads**  
**Clear Hot Day, Case 660 (Low-E Window)**  
**Heating (+), Sensible Cooling (-)**



**Figure B8-H23. Hourly Loads**  
**Clear Cold Day, Case 670 (Single-Pane Window)**  
**Heating (+), Sensible Cooling (-)**

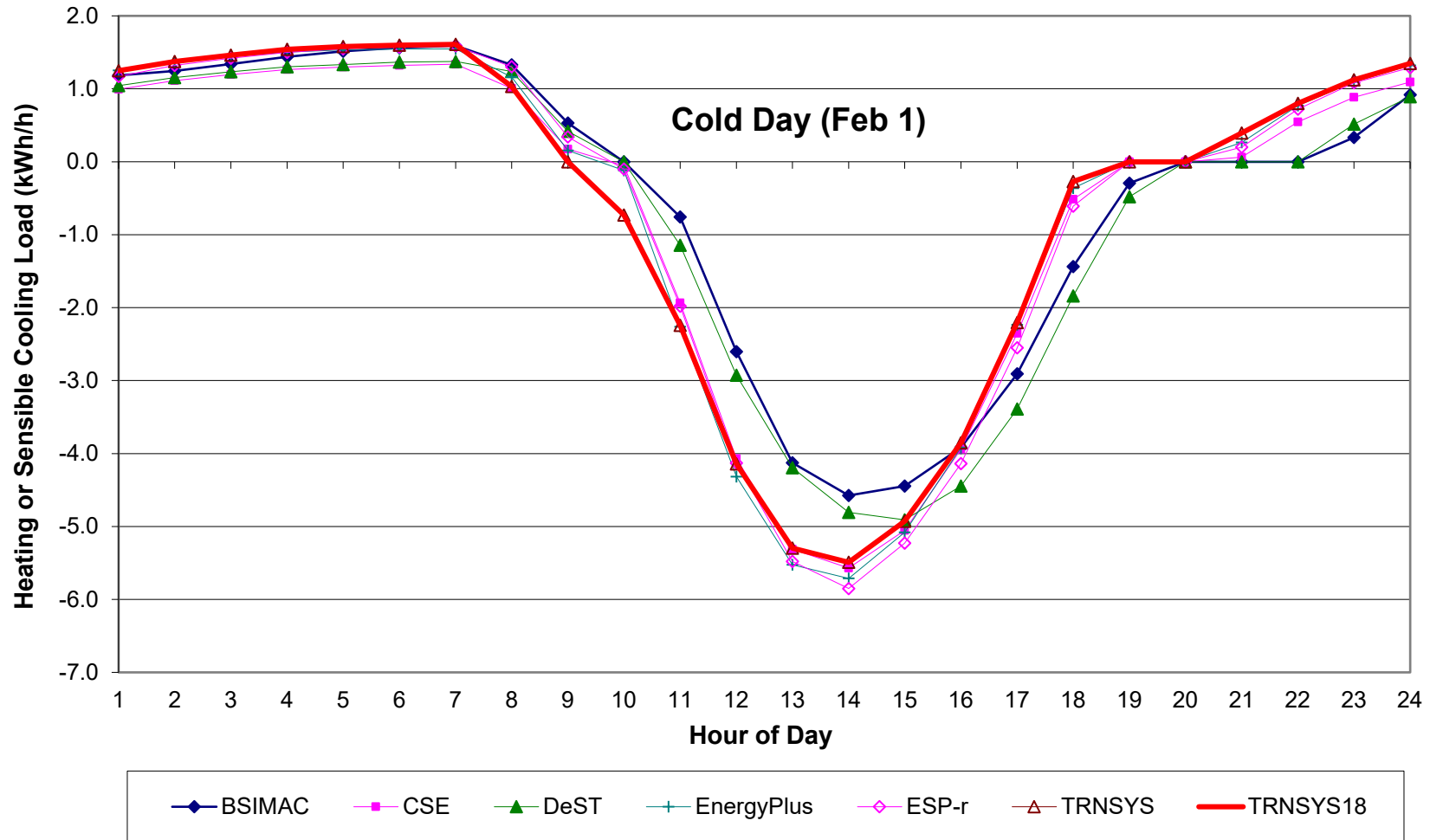


**Figure B8-H24. Hourly Loads**  
**Clear Hot Day, Case 670 (Single-Pane Window)**  
**Heating (+), Sensible Cooling (-)**

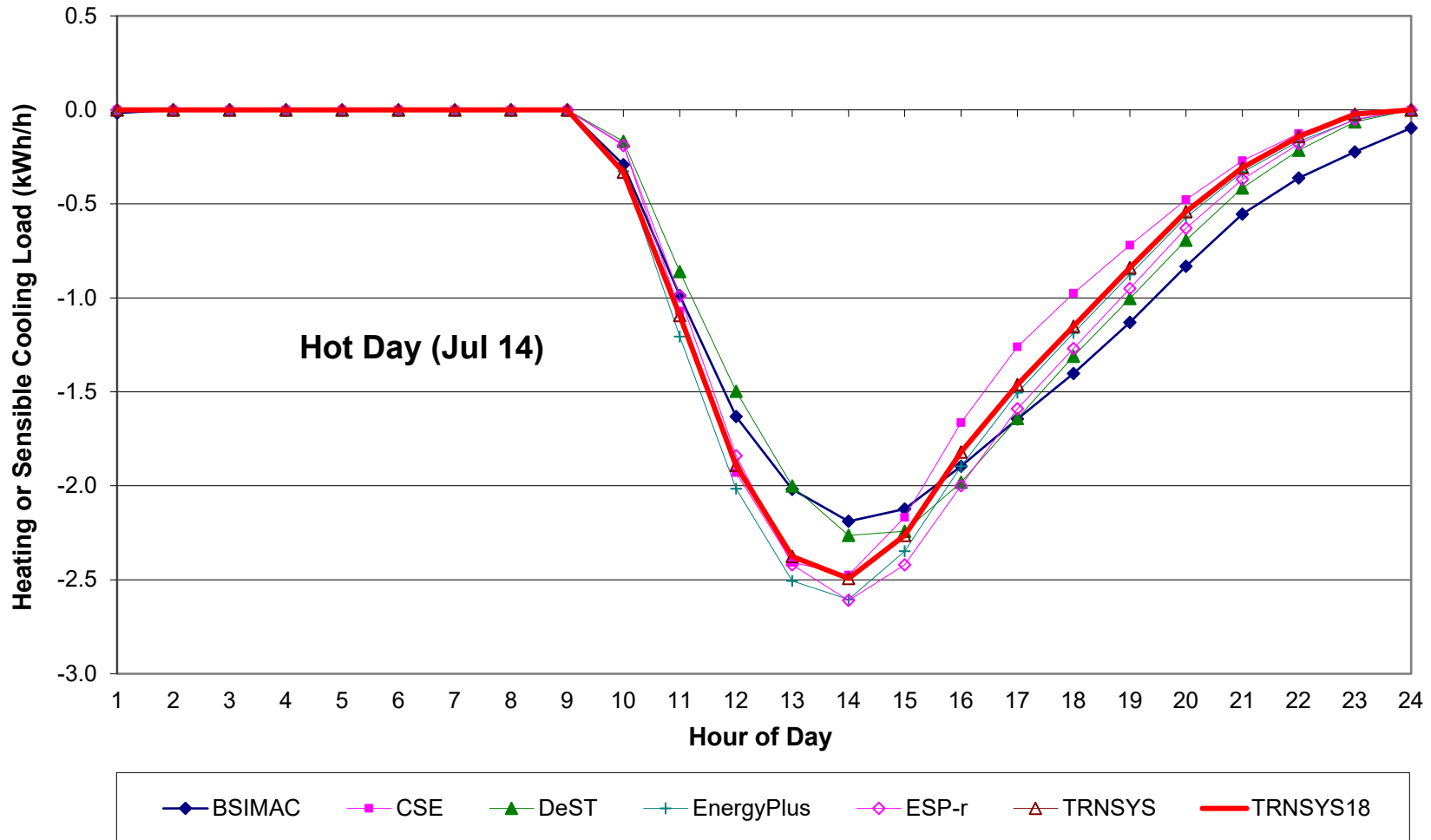




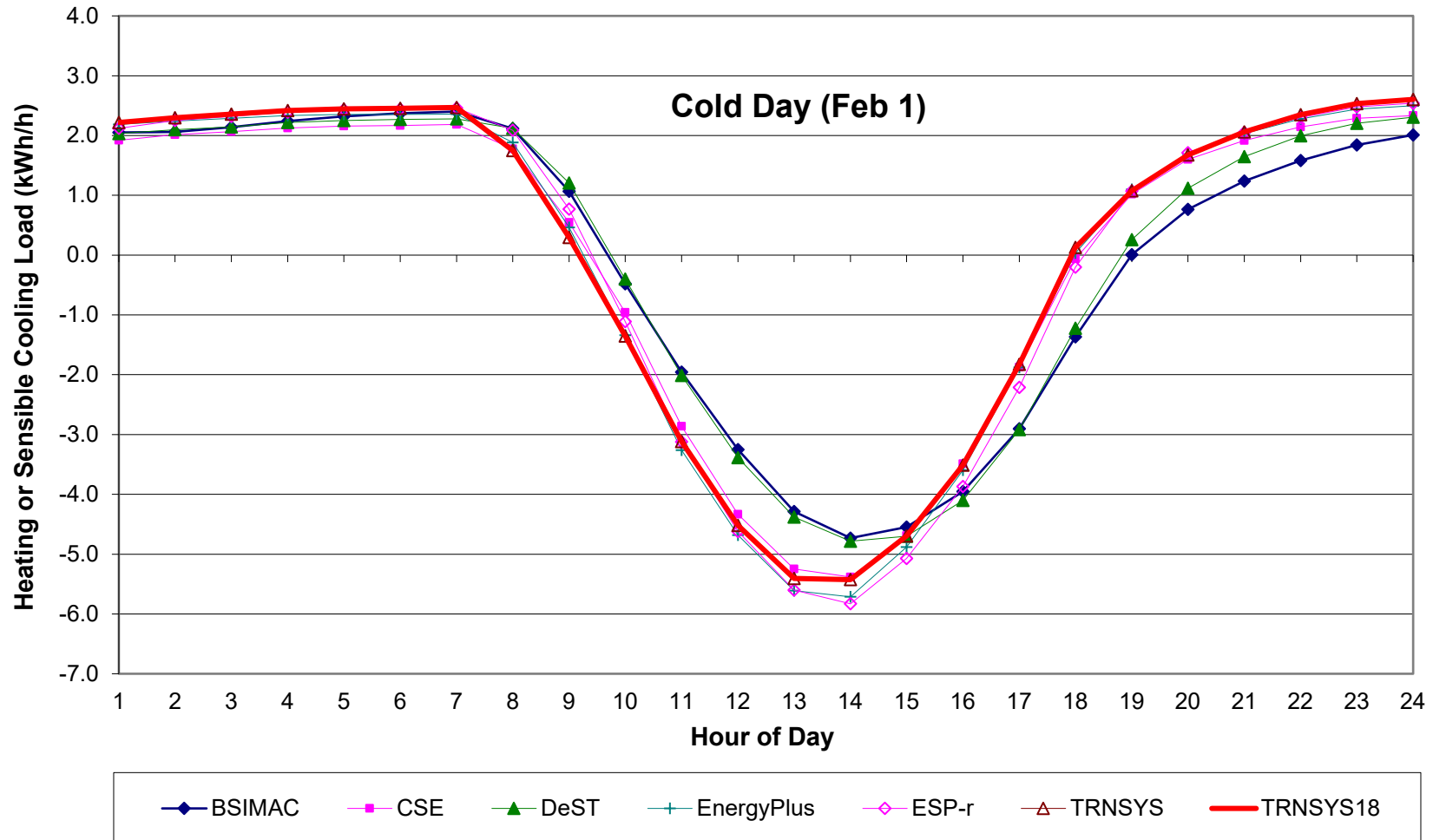
**Figure B8-H25. Hourly Loads  
Clear Cold Day, Case 680 (Insulation)  
Heating (+), Sensible Cooling (-)**



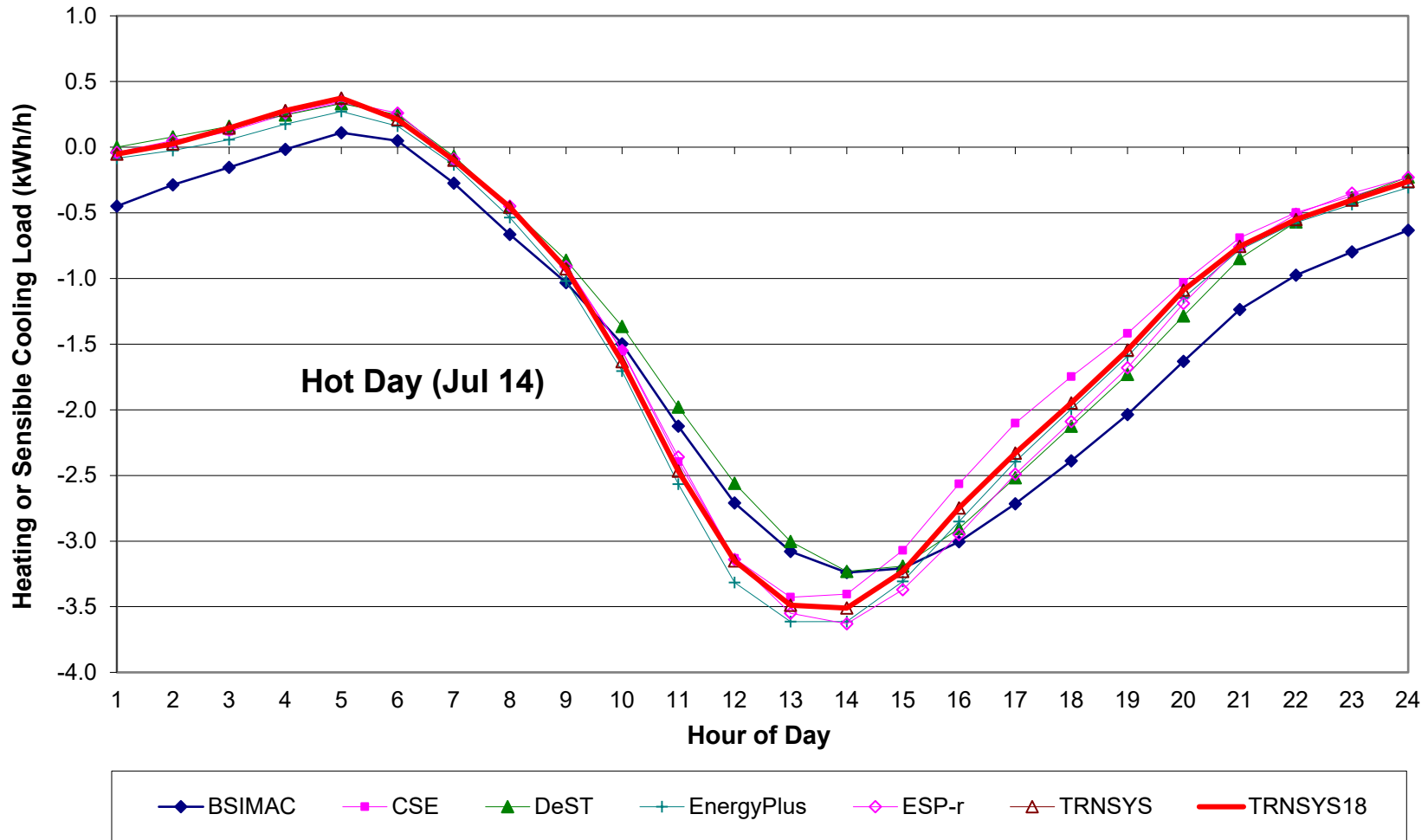
**Figure B8-H26. Hourly Loads**  
**Clear Hot Day, Case 680 (Insulation)**  
**Heating (+), Sensible Cooling (-)**



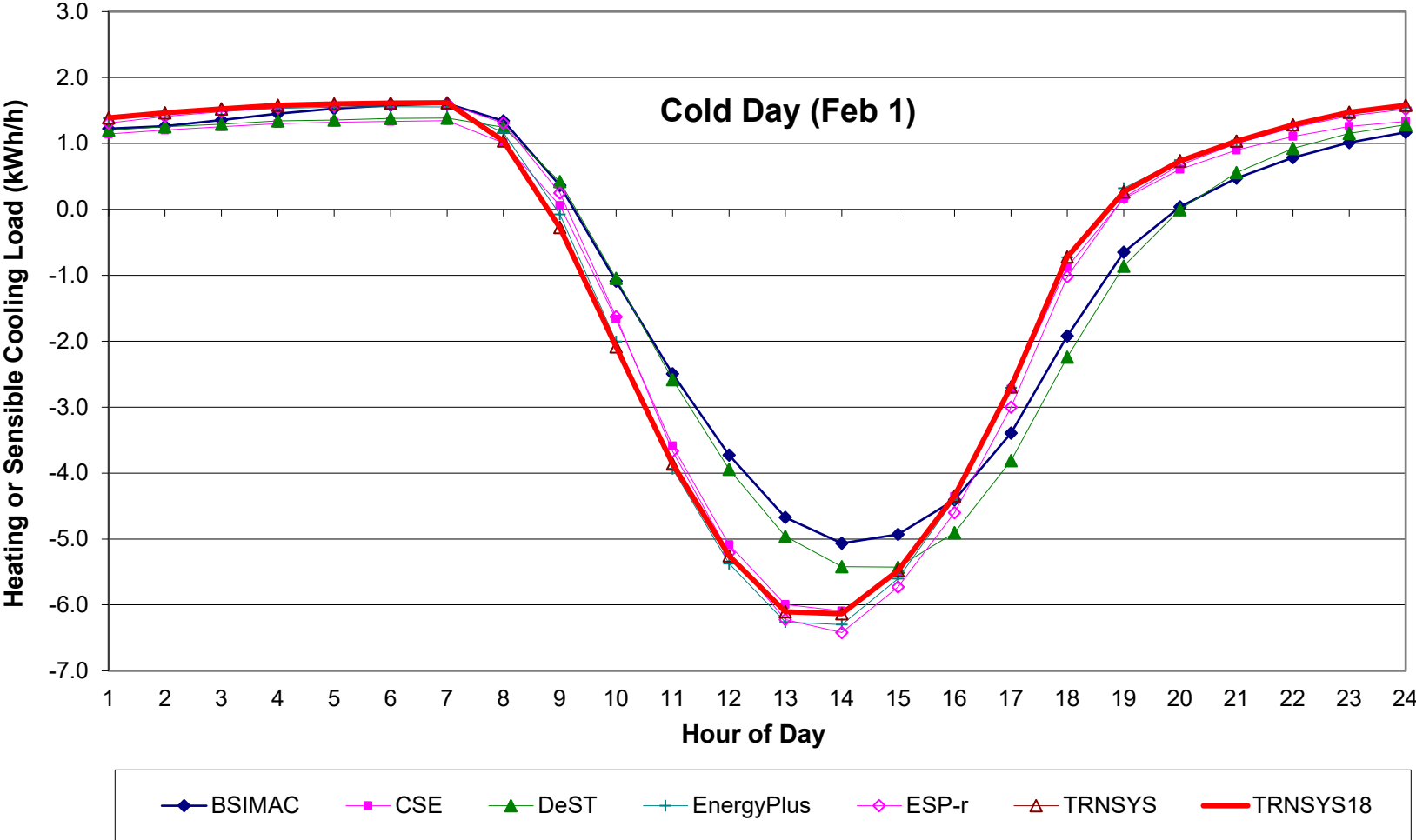
**Figure B8-H27. Hourly Loads  
Clear Cold Day, Case 685 (20/20 Tstat)  
Heating (+), Sensible Cooling (-)**



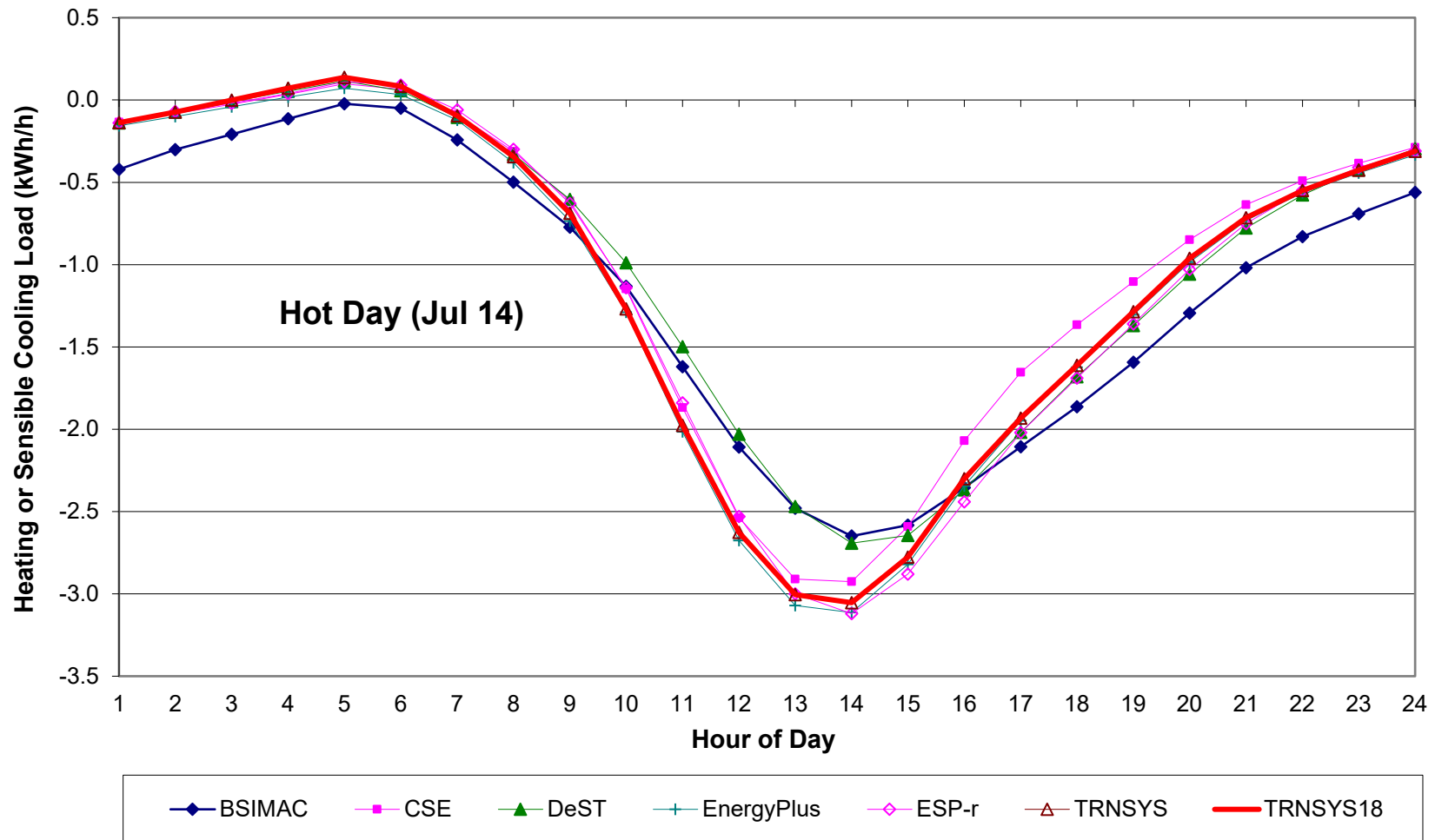
**Figure B8-H28. Hourly Loads  
Clear Hot Day, Case 685 (20/20 Tstat)  
Heating (+), Sensible Cooling (-)**



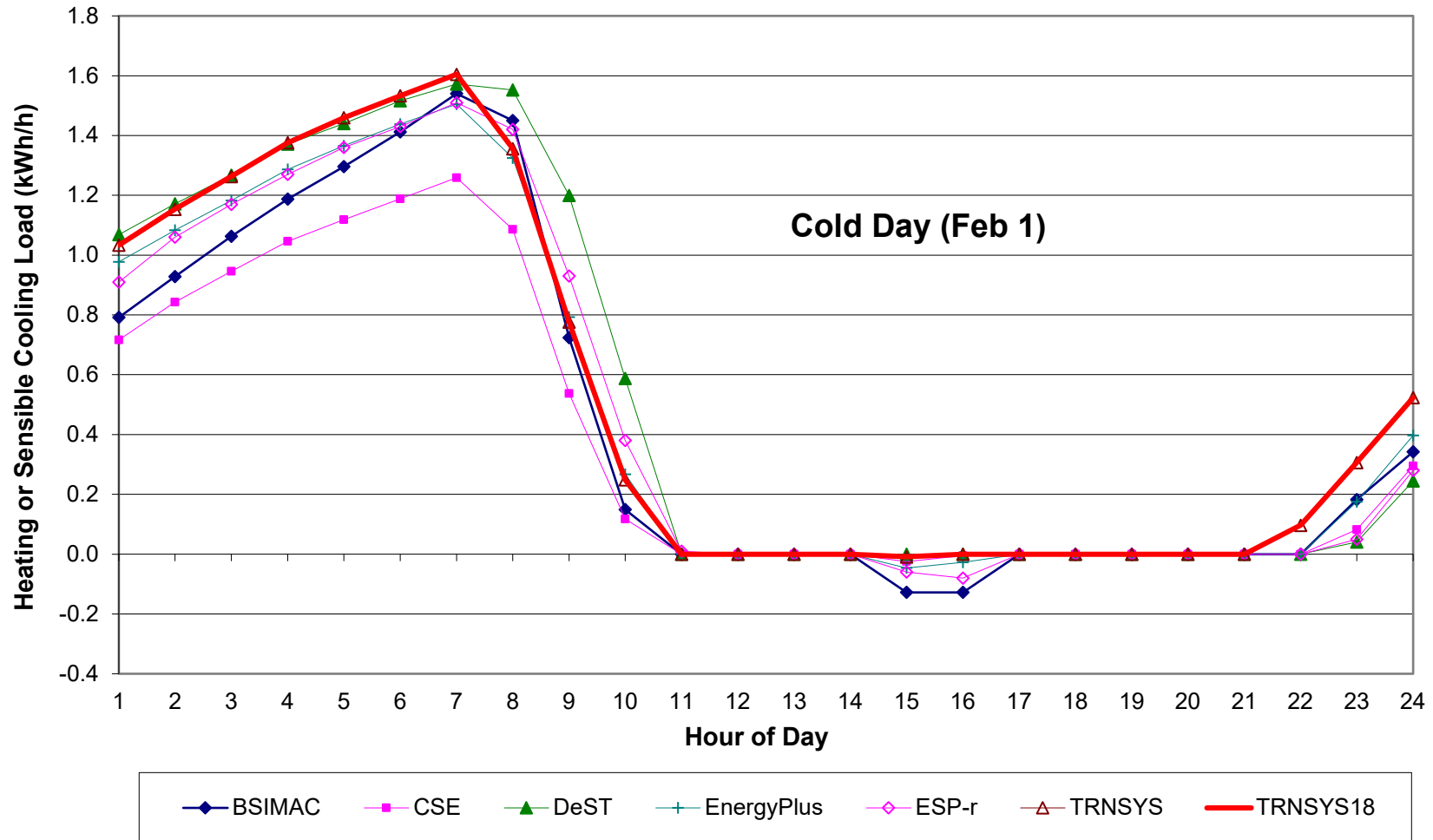
**Figure B8-H29. Hourly Loads**  
**Clear Cold Day, Case 695 (20/20, Insulation)**  
**Heating (+), Sensible Cooling (-)**



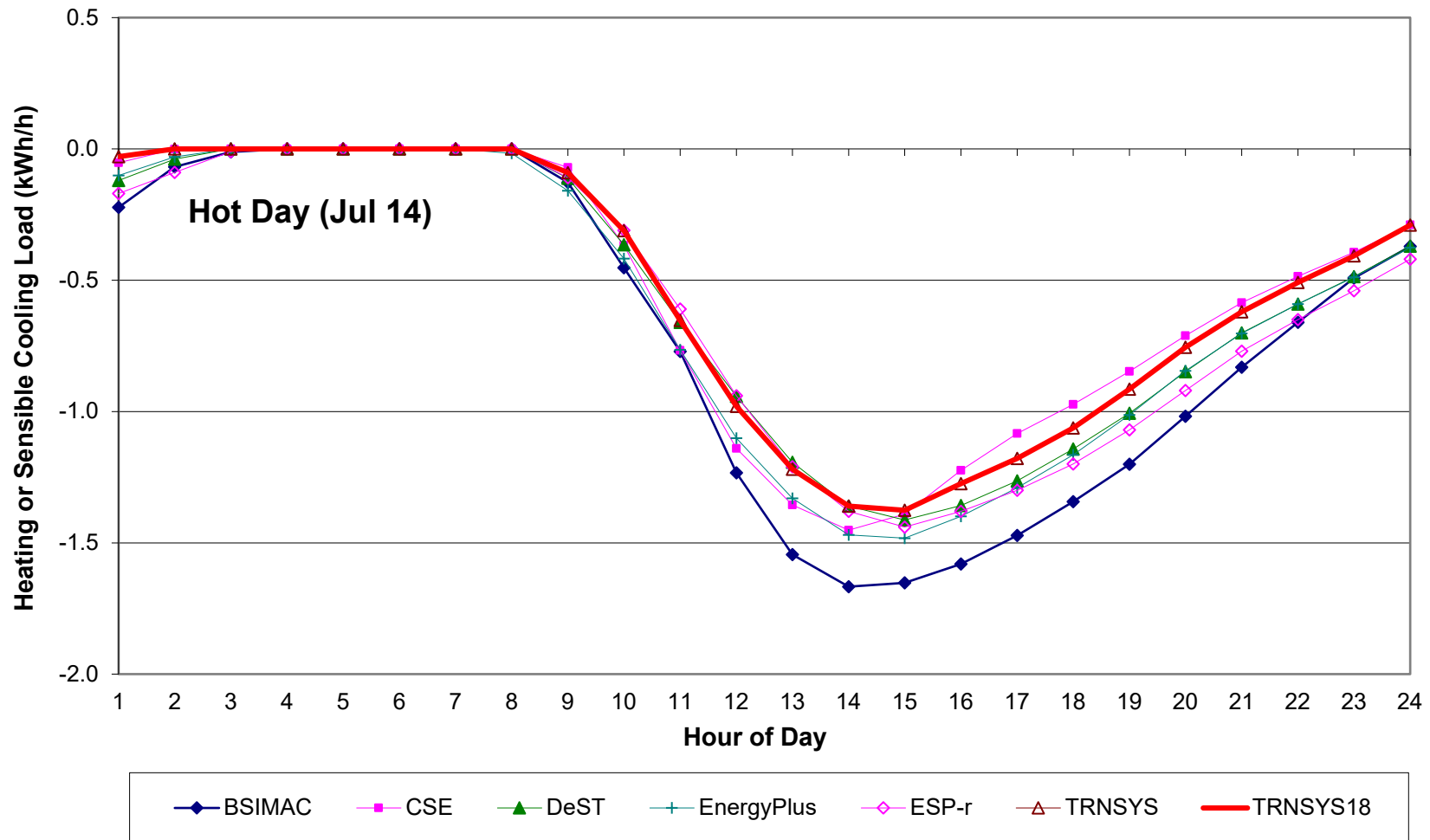
**Figure B8-H30. Hourly Loads**  
**Clear Hot Day, Case 695 (20/20, Insulation)**  
**Heating (+), Sensible Cooling (-)**



**Figure B8-H31. Hourly Loads  
Clear Cold Day, Case 900 (High Mass)  
Heating (+), Sensible Cooling (-)**



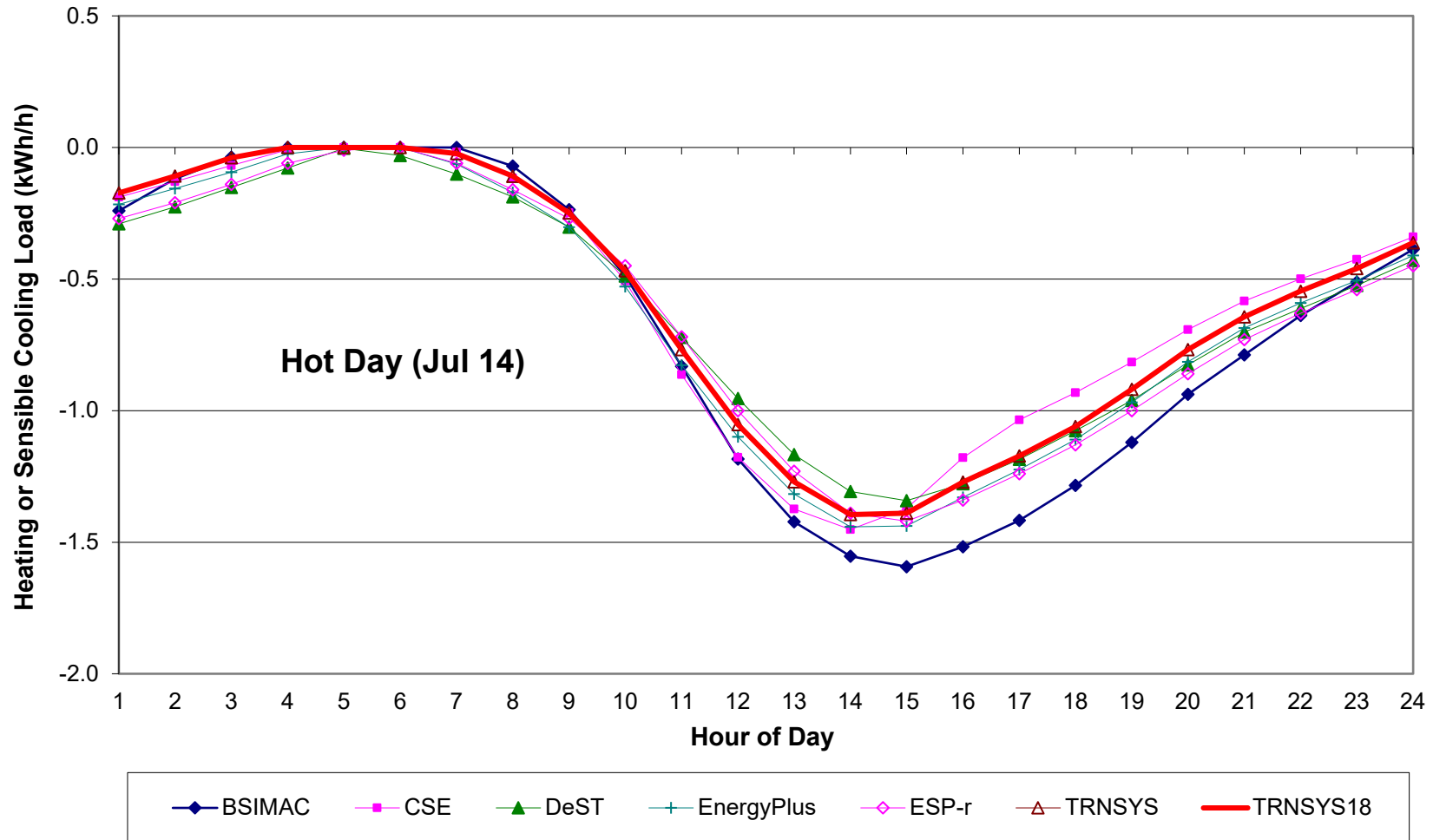
**Figure B8-H32. Hourly Loads  
Clear Hot Day, Case 900 (High Mass)  
Heating (+), Sensible Cooling (-)**



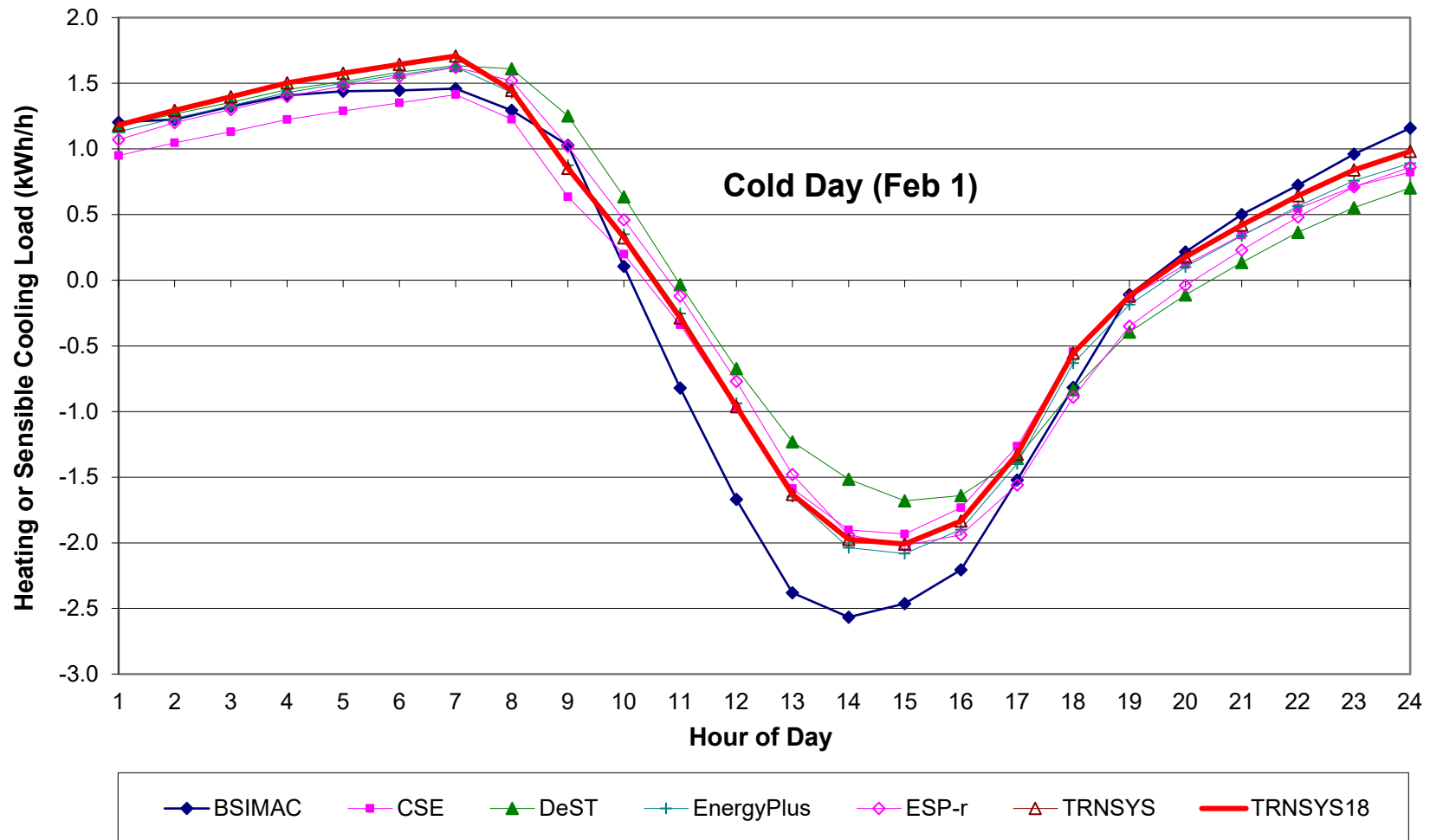




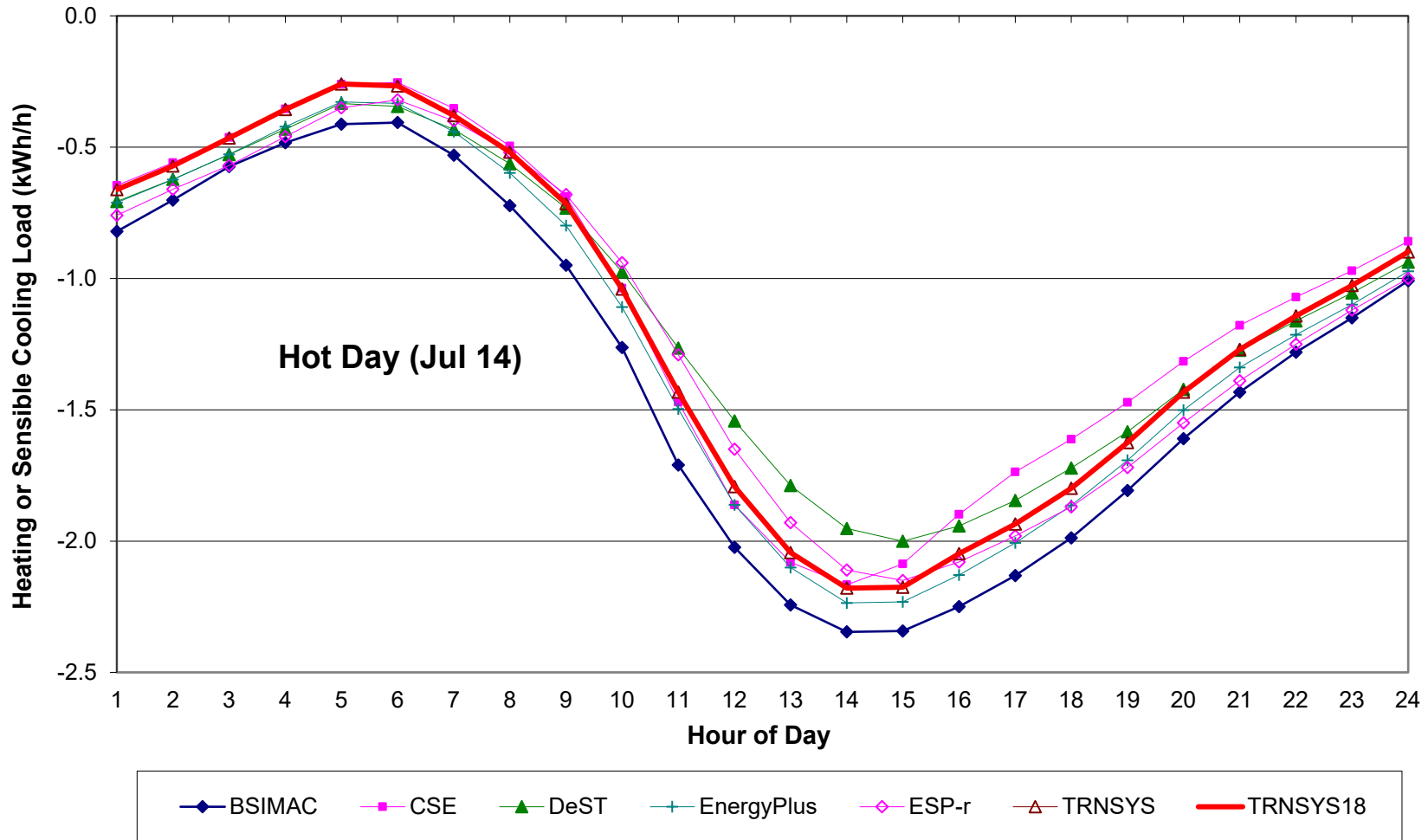
**Figure B8-H34. Hourly Loads**  
**Clear Hot Day, Case 980 (High Mass, Insulation)**  
**Heating (+), Sensible Cooling (-)**



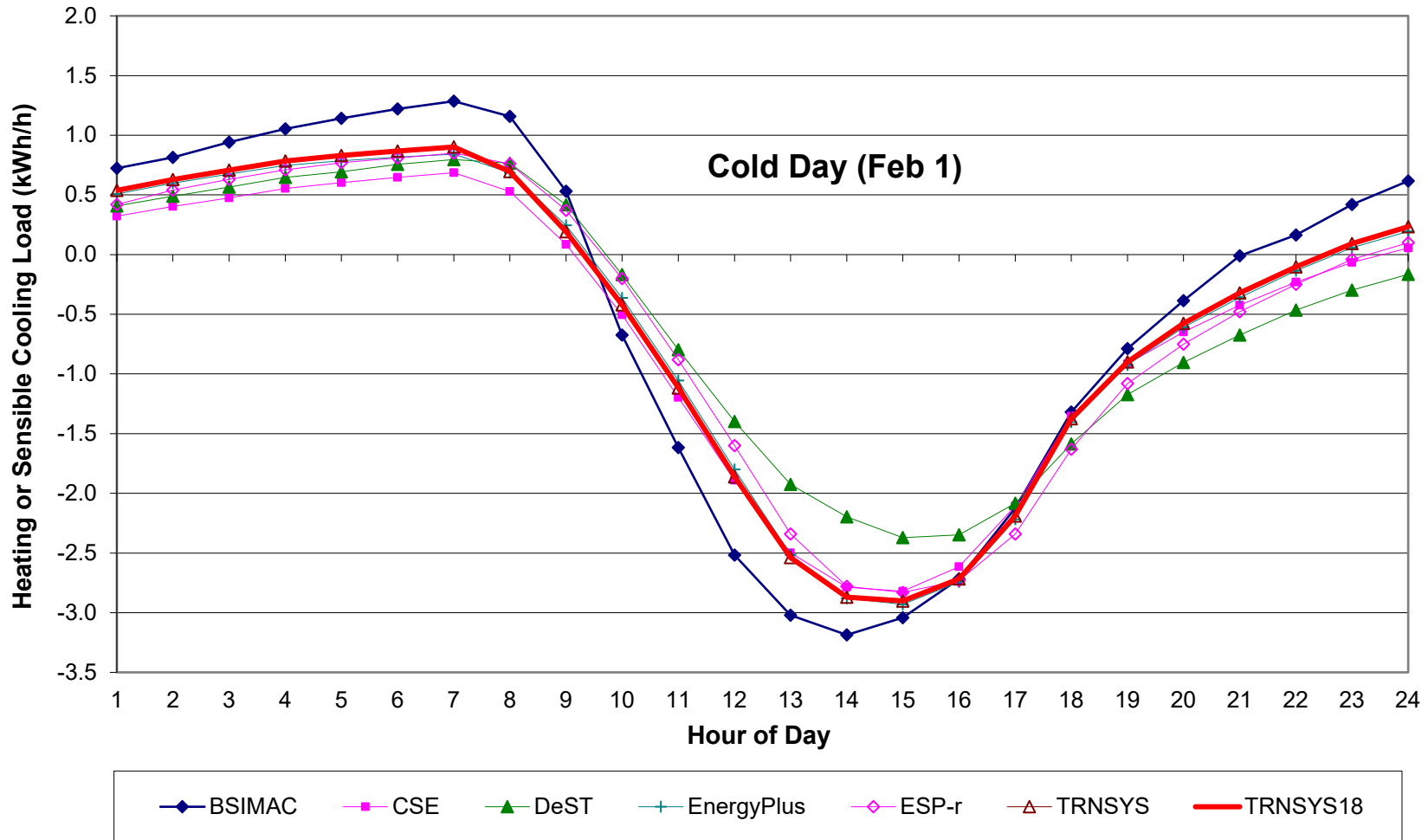
**Figure B8-H35. Hourly Loads**  
**Clear Cold Day, Case 985 (High Mass, 20/20 Tstat)**  
**Heating (+), Sensible Cooling (-)**



**Figure B8-H36. Hourly Loads**  
**Clear Hot Day, Case 985 (High Mass, 20/20 Tstat)**  
**Heating (+), Sensible Cooling (-)**



**Figure B8-H37. Hourly Loads**  
**Clear Cold Day, Case 995 (High Mass, 20/20, Insulation)**  
**Heating (+), Sensible Cooling (-)**



**Figure B8-H38. Hourly Loads**  
**Clear Hot Day, Case 995 (High Mass, 20/20, Insulation)**  
**Heating (+), Sensible Cooling (-)**

